

# MAGNETIC FORCES ON CHARGES

## Lorentz Force Law:

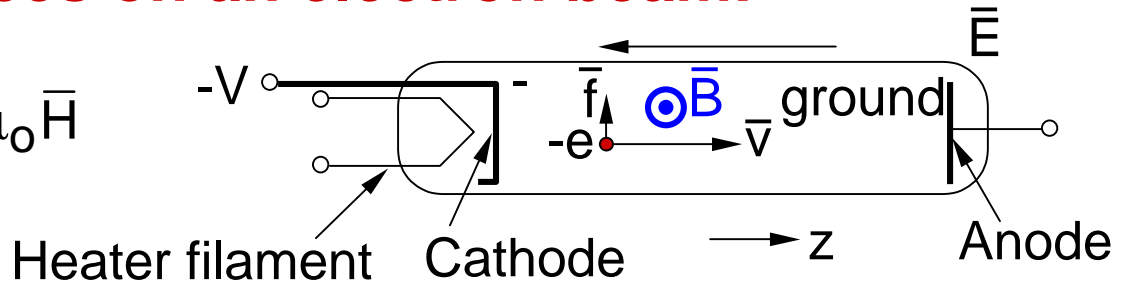
$$\vec{f} = q(\vec{E} + \vec{v} \times \mu_0 \vec{H}) \quad \text{Newtons}$$

$q$  = electric charge (Coulombs)

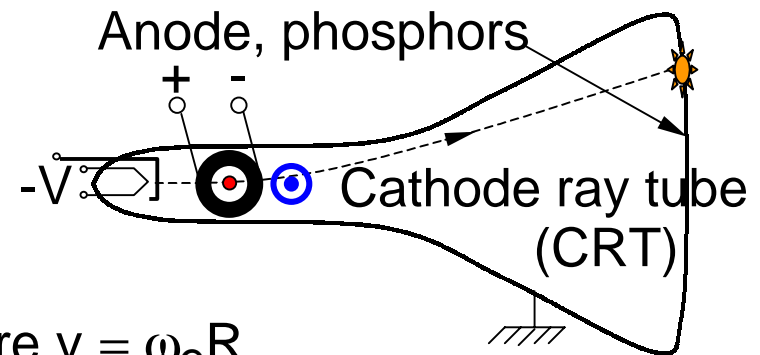
$\vec{v}$  = velocity vector ( $\text{m s}^{-1}$ )

## Example: magnetic forces on an electron beam:

Lateral forces:  $\vec{f} = q\vec{v} \times \mu_0 \vec{H}$



Electrostatic deflection best for small  $V$ ,  
magnetic deflection best for large  $V, v$ .

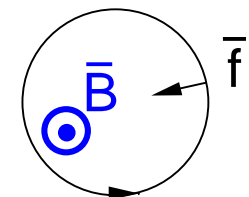


## Cyclotron motion:

$$|f| = ev\mu_0 H = ma = m_e \omega_e^2 R = m_e v \omega_e, \quad \text{where } v = \omega_e R$$

$$\omega_e = e\mu_0 H / m_e \quad \text{"Electron cyclotron frequency" } [\text{rs}^{-1}]$$

$$\text{e.g. } \omega = 1.6 \cdot 10^{-19} \times 0.1 / 9.1 \times 10^{-31} \Rightarrow 2.8 \text{ GHz } (\sim \text{MRI})$$



# MAGNETIC FORCES ON CURRENTS IN WIRES

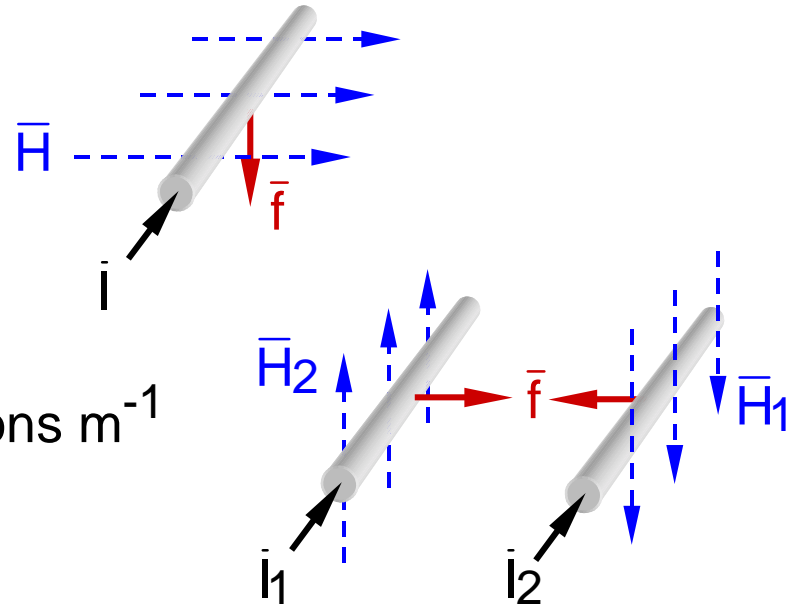
## Force equation:

$$\bar{f} = q(\bar{E} + \bar{v} \times \mu_0 \bar{H}) \text{ Newtons}$$

## Force on wire [Nm<sup>-1</sup>]:

$$\bar{f} = nq\bar{v} \times \mu_0 \bar{H} = \bar{I} \times \mu_0 \bar{H}, \text{ where}$$

$n$  is the number of conduction electrons  $m^{-1}$   
at  $\bar{v}$  and  $\bar{I}$  is the current vector =  $nq\bar{v}$



## Force attracting parallel wires:

$$|f| = I\mu_0 H = \mu_0 I^2 / 2\pi r = 2I^2 \times 10^{-7} / r \text{ [Nm}^{-1}] \quad (\mu_0 = 4\pi \times 10^{-7})$$

$$\int_C \bar{H} \cdot d\bar{s} = I = 2\pi r H \Rightarrow H = I / 2\pi r$$

Example:  $|f| = 2 \times 100^2 \times 10^{-7} / 10^{-2} = 0.2 \text{ [N]}$ , attract or repulse

## Pinch effect:

This experiment defines  $\mu_0$  and predicts “pinch effect”

The four quadrants of a wire squeeze together  $\propto I^2/r$  and can crush wire, limiting the maximum achievable current density



# VOLTAGES PRODUCED BY MOTION ACROSS $\bar{H}$

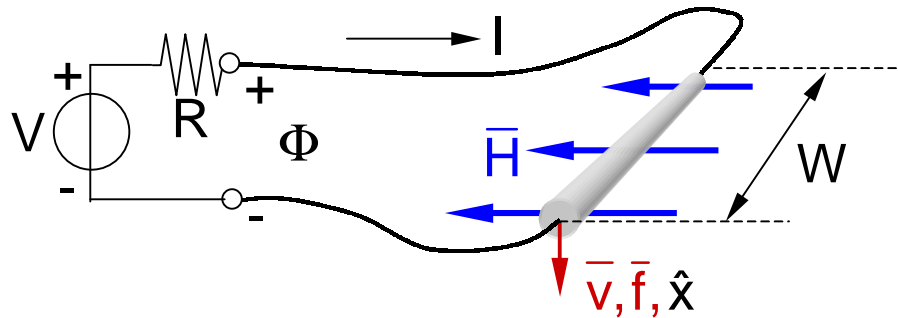
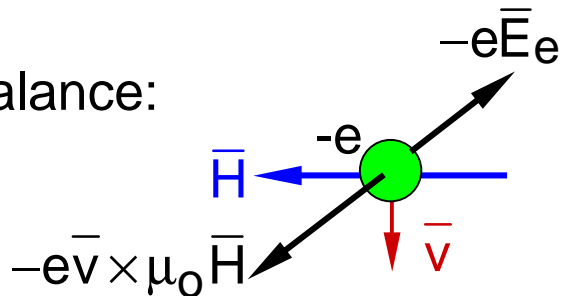
## Consider electron inside moving wire:

Force on that electron:  $\bar{f}_e = -e(\bar{E}_e + \bar{v} \times \mu_0 \bar{H})$

For open-circuit wire:  $\bar{f}_e = -e(\bar{E}_e + \bar{v} \times \mu_0 \bar{H}) = 0 \Rightarrow \bar{E}_e = -\bar{v} \times \mu_0 \bar{H}$  inside

Open-circuit voltage across wire:  $\Phi = E_e W = v \mu_0 H W [V]$ , where  $W$  = wire length

Force balance:



## Electric fields inside conductors:

Total force on free conduction electrons is produced by  $\bar{v} \times \bar{H}$  plus an opposing  $\bar{E}_e$

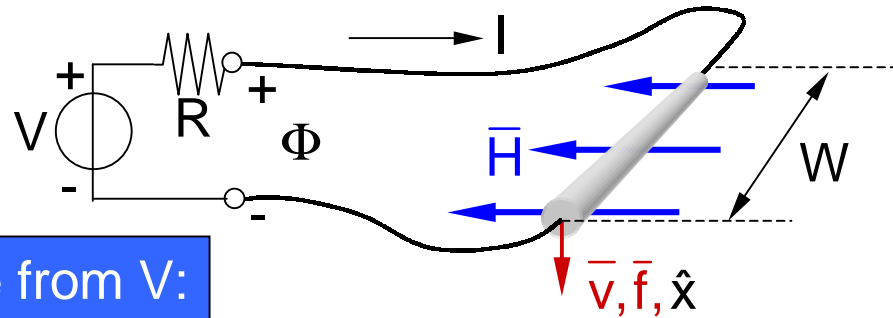
$\bar{E}_e$  is produced by charge distributions that build inside wire until all electrons see  $\bar{f} = 0$

# MAGNETIC MOTORS ARE ALSO GENERATORS

**Current  $I$ , force  $f$ , and power  $P$  produced:**

$$I = (V - \Phi)/R$$

$$\bar{f} = \hat{I} \times \mu_0 \bar{H} W = \hat{x} \mu_0 H W (V - \Phi)/R$$



Mechanical power delivered by wire from  $V$ :

$$P_m = \bar{f} \cdot \bar{v} = v \mu_0 H W (V - \Phi)/R = \Phi (V - \Phi)/R [W]$$

Electrical power delivered to wire by  $V, R$ :

$$\begin{aligned} P_e &= VI - I^2 R = V(V - \Phi)/R - (V - \Phi)^2/R \\ &= [(V - \Phi)/R] [V - (V - \Phi)] = \Phi (V - \Phi)/R [W] \end{aligned}$$

Therefore: **Electrical power  $\leftrightarrow$  Mechanical power**

**It is motor if mechanical power out  $> 0$ :** i.e. if  $V > \Phi = v \mu_0 H W$

**It is generator if electrical power out  $> 0$ :** i.e. if  $V < \Phi$ , or  $v > V/\mu_0 H W$

i.e. when the motor “back voltage”  $\Phi > V$ .

In unloaded motors  $V = \Phi$  and  $I = 0$ .

# ROTARY WIRE MOTOR

## Single wire loop spinning in uniform $\bar{H}$ :

Total force (torque) is sum of forces on wire segments

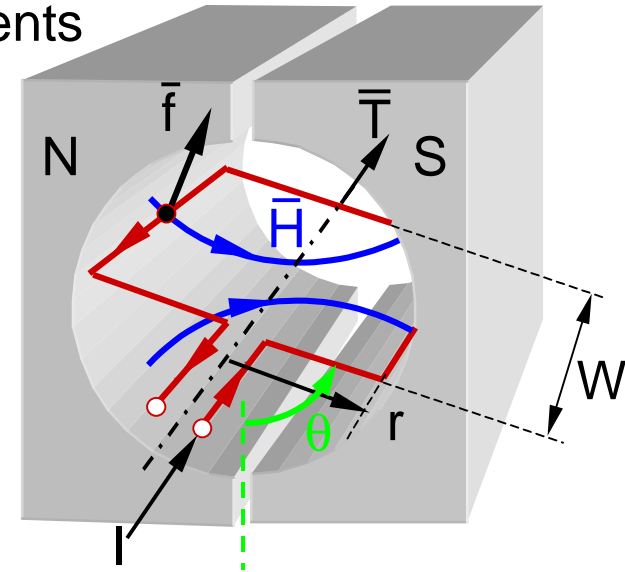
Axial forces from wires at ends cancel

Tangential forces add  $\Rightarrow$  torque =  $2f[m^{-1}]Wr$

$f = I\mu_0 H$  ( $= NI\mu_0 H$  for N-turn coil)

$T = 2I\mu_0 HWr = I\mu_0 HA$  [Nm], A is loop area

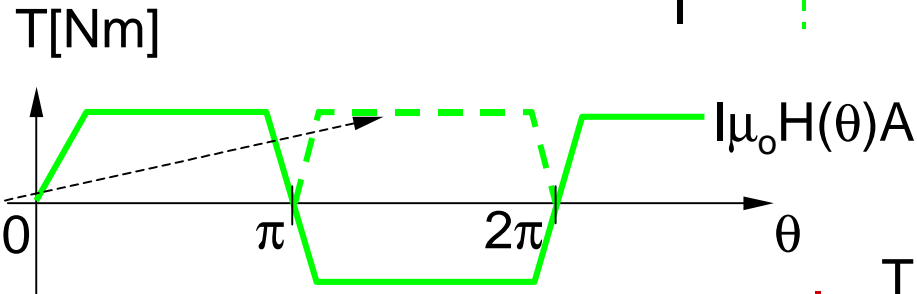
Torque is a vector  $\bar{T} = \bar{r} \times \bar{f}$



## Torque varies with $\theta$ :

If  $I = \text{constant}$ :

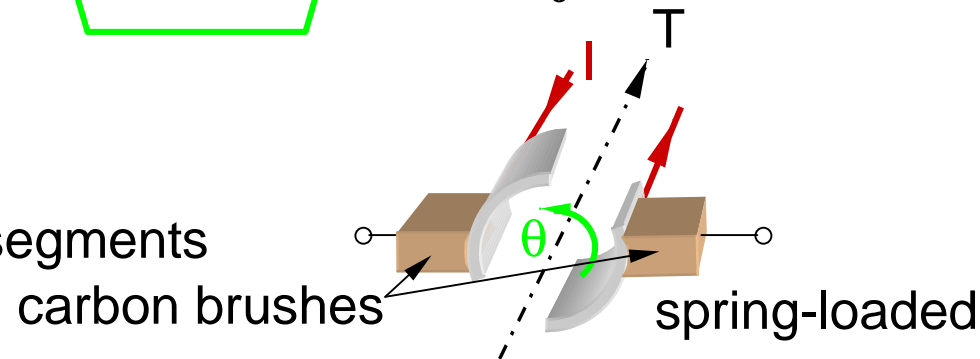
With commutator



## Commutators:

Switch currents to maximize torque

Can have N coils, 2N commutator segments



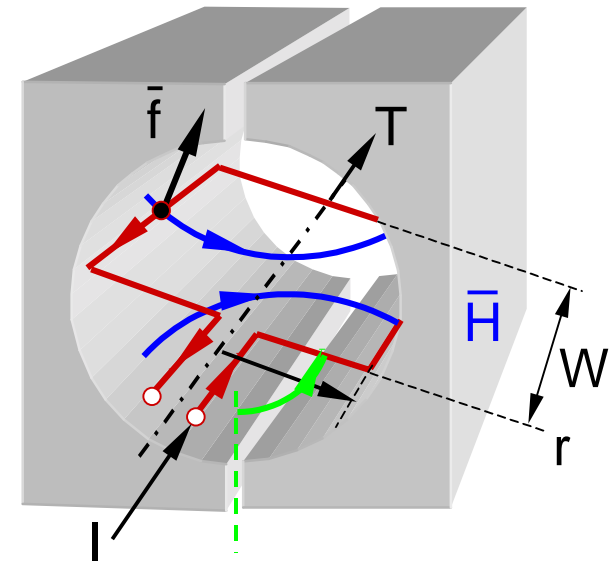
# TWO-POLE (N-S) COMMUTATED MOTOR

## Design assumptions:

$\mu_0 H \cong \text{constant} = 1 \text{ Tesla } (10^4 \text{ gauss})$

One 100-turn loop ( $N = 100$ ) of area  $A = 10^{-3} [\text{m}^2]$

$V = 24 \text{ volts, perfectly commutated}$



## Maximum $\omega$ , unloaded ( $T = 0$ ):

$\omega$  is angular frequency

Back-voltage  $\Phi = V = 24 [\text{V}]$  in equilibrium

$$\Phi = 2N E_e W = 2N v \mu_0 H W = N A \mu_0 H \omega = 24$$

$$\omega = 24 / N A \mu_0 H = 24 / (100 \times 10^{-3}) = 240 \Rightarrow 2292 \text{ rpm}$$

(More typical values for  $\bar{B}$  are 0.5  $\Rightarrow$   $\sim 4,600$  rpm max)

## Maximum torque when $\omega = 0$ :

Assume power supply is limited to  $I = 10 [\text{A}]$

$$T = N I \mu_0 H A = 100 \times 10 \times 1 \times 10^{-3} = 1 [\text{Nm}] (\rightarrow 100\text{N at } r = 1 \text{ cm})$$

# MOTOR TORQUE/POWER/SPEED RELATIONS

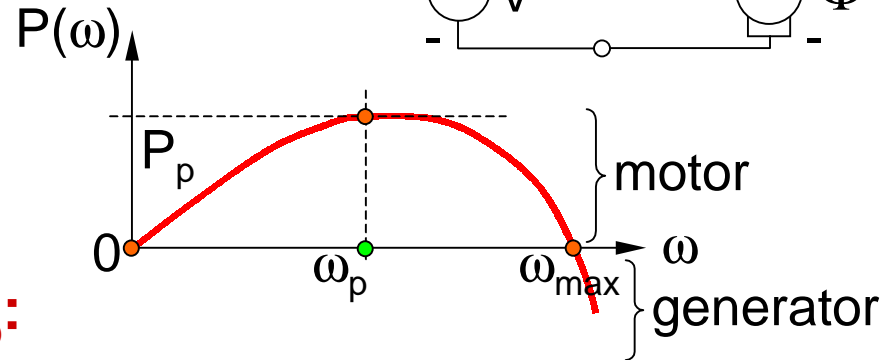
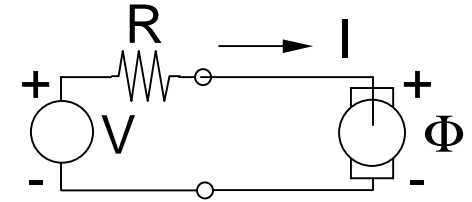
**Mechanical power output =  $\omega T$  [Nms<sup>-1</sup> = W] = f( $\omega$ ):**

$$P = \omega T = \omega NI\mu_o HA$$

$$I = (V - \Phi)/R$$

$$\Phi = NA\mu_o H\omega$$

$$P = \omega T = \omega N(V - NA\mu_o H\omega)\mu_o HA/R$$



**Maximum mechanical power out  $P_p$ :**

$$\partial P/\partial \omega = 0 \Rightarrow V = 2\omega_p NA\mu_o H \text{ [so at } \omega_p \text{ we have } \Phi = V/2] \Rightarrow$$

$$\omega_p = V/2NA\mu_o H = \omega_{\max}/2 \text{ [} V = NA\mu_o H\omega_{\max}\text{]}$$

$$P_p = \omega_p T = (V/2NA\mu_o H)N(V - [NA\mu_o H V/2NA\mu_o H])\mu_o HA /R = V^2/4R$$

At maximum power, motor is matched load of impedance R!

( $\Phi = V/2$  is across motor,  $V/2$  is across R)

Assume  $I_{\max} = V/R = 192\text{A}$  and  $V = 24$  volts. Then  $R = 0.125$  ohms, and

$$P_p = 24^2/4 \times 0.125 = 1.152 \text{ Kw}$$

**Motor design strategy:**

To minimize motor weight (cost), boost  $\omega NIH$

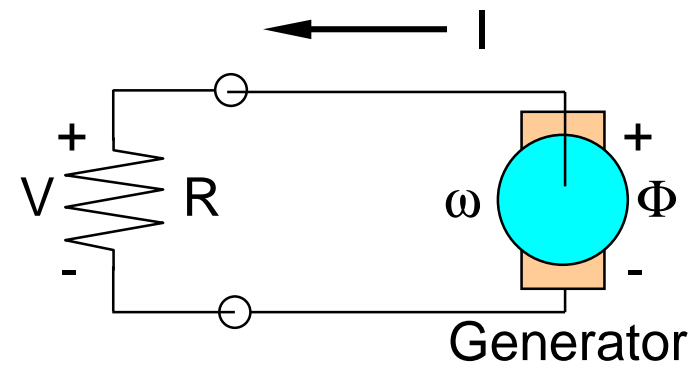
# GENERATOR POWER/FREQUENCY RELATIONS

**Electrical power out  $P = \omega T = \Phi I$ :**

$$\Phi = NA\mu_0 H\omega$$

$$I = \Phi/R$$

$$P = \Phi I = \Phi^2/R = \omega^2(NA\mu_0 H)^2/R$$

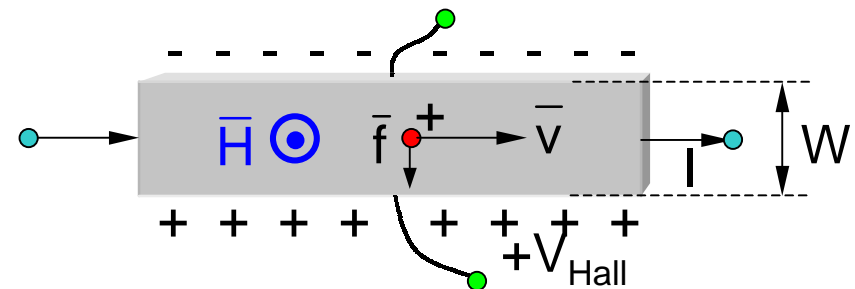


**To maximize power out  $\Rightarrow P_p$ :**

$\omega$  is limited by vibration, lubricant, rotor fragmentation, and air viscosity (drag); smooth balanced rotors with  $\omega r < c_s$  ( $\sim 300 \text{ ms}^{-1}$ ) are best.  $\Phi < \text{breakdown voltage}$ .  $I$  limited by magnet survival ( $\sim 200 \text{ C}$ ), insulation melting, and cooling; heat capacity allows transient peaks.

**Hall effect sensors:**

$$\bar{E}_e = -\bar{v} \times \mu_0 \bar{H} \Rightarrow V_{\text{Hall}} = v\mu_0 HW$$



$V_{\text{Hall}} \Rightarrow H$  if  $v$  is known,  $\Rightarrow v = I/nq$  if  $H$  is known (study carriers)