

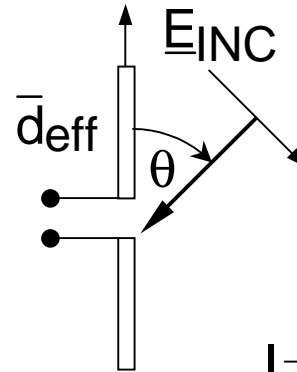
RECEIVING ANTENNAS

Recall: $A_e(\theta, \phi) = \left(\lambda^2/4\pi\right) G(\theta, \phi)$

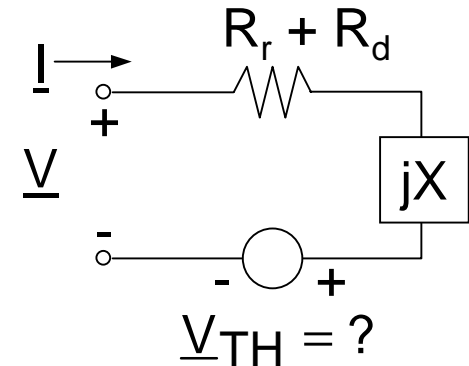
We never proved it; sometimes untrue (when?)

Proof for Short Dipole Antenna:

If $d \ll \lambda/2\pi$, quasistatics applies



We seek V_{Th} in equivalent circuit:



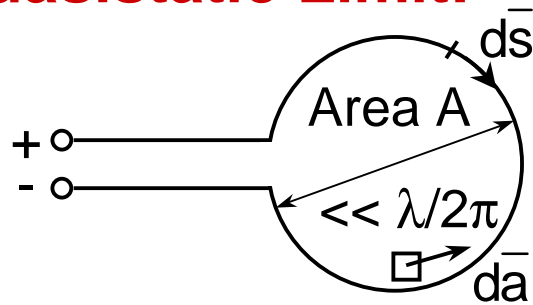
Assume Normally Incident Uniform Plane Wave:

Case 1: small loop antenna ($D \ll \lambda/2\pi$)

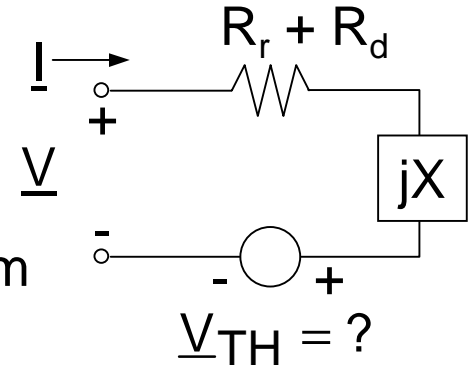
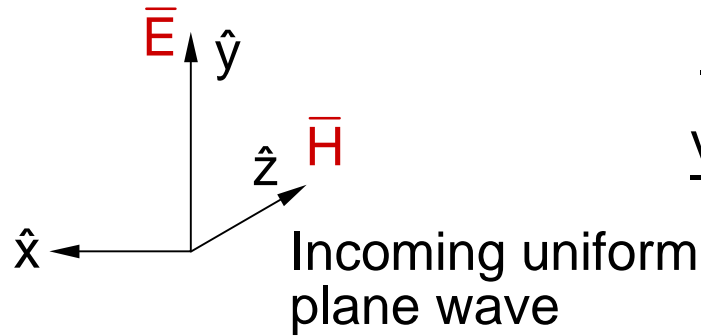
Case 2: short dipole antenna ($d \ll \lambda/2\pi$)

SMALL LOOP ANTENNA: OPEN CIRCUIT VOLTAGE

Quasistatic Limit:



Faraday's Law:



$$\nabla \times \bar{E} = -\partial \bar{B} / \partial t \Rightarrow -\frac{d}{dt} \int_A \bar{B} \cdot d\bar{a} = \int_C \bar{E} \cdot d\bar{s} = V_{TH}$$

Open Circuit Voltage:

$$V_{TH} = -A\mu_0 \left(\partial [\bar{H} \cdot \hat{z}] / \partial t \right)$$

UPW: Power $P [W/m^2] = \eta_0 |\bar{H}_0|^2 / 2$

Where: $\bar{H} = \hat{z} H_0 \cos \omega t$ at $z = 0$, and

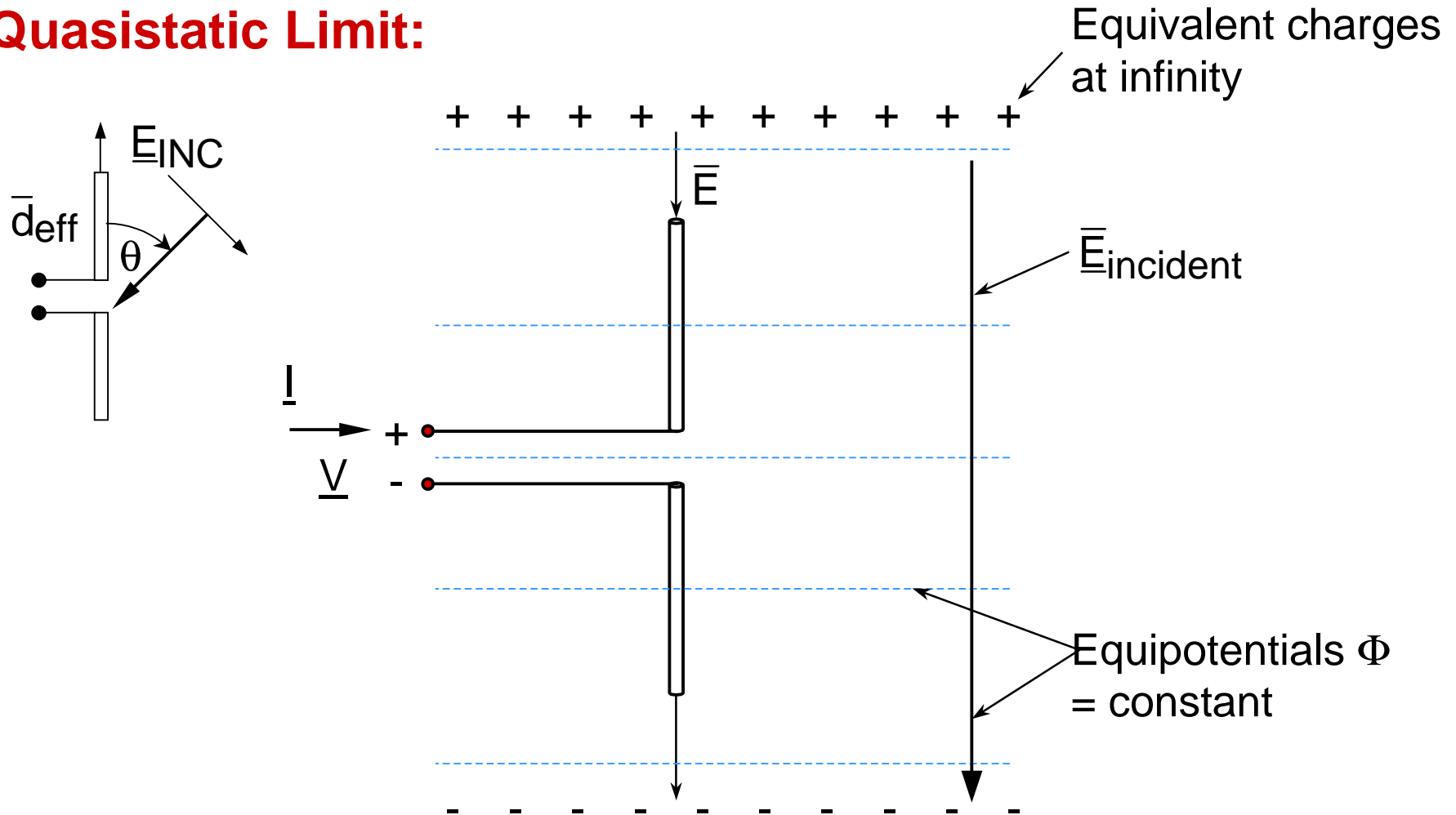
$$\left(\partial [\bar{H} \cdot \hat{z}] / \partial t \right) = -\omega H_0 \sin \omega t$$

Therefore: $\left(\partial [\bar{H} \cdot \hat{z}] / \partial t \right) = -\omega (2P/\eta_0)^{0.5} \sin \omega t$ and

$$V_{TH} = A\mu_0 \omega (2P/\eta_0)^{0.5} \sin \omega t$$

SHORT DIPOLE ANTENNA: OPEN CIRCUIT VOLTAGE

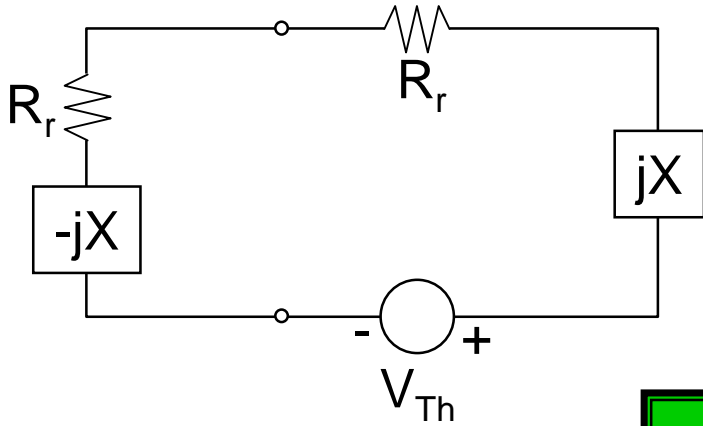
Quasistatic Limit:



$$\underline{V}_{\text{Th}} = -\vec{E}_{\text{INC}} \cdot \vec{d}_{\text{eff}} = -\vec{E}_{\text{INC}} d_{\text{eff}} \sin \theta$$

MAXIMUM POWER EXTRACTABLE FROM A SHORT DIPOLE ANTENNA

Antenna Equivalent Circuit plus Matched Load:



$$P_{\text{rec.max}} = \frac{1}{2} |V_{\text{Th}}/2|^2 / R_r$$

$$= |\bar{E}_{\text{INC}}|^2 \frac{d_{\text{eff}}^2}{8R_r} \sin^2 \theta$$

where $R_r = \eta_0 (kd_{\text{eff}})^2 / 6\pi$

Define $A_{\text{eff}}(\theta, \phi) \triangleq \frac{P_{\text{rec}}}{|\bar{E}_{\text{inc}}|^2 / 2\eta_0}$ "Effective Area"

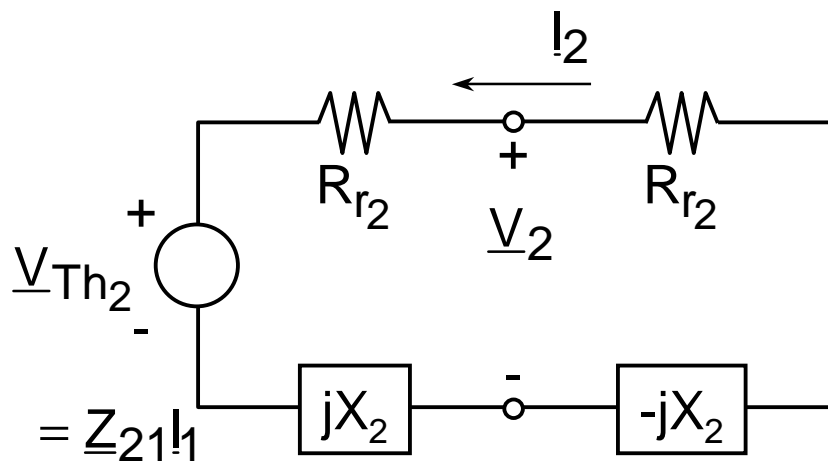
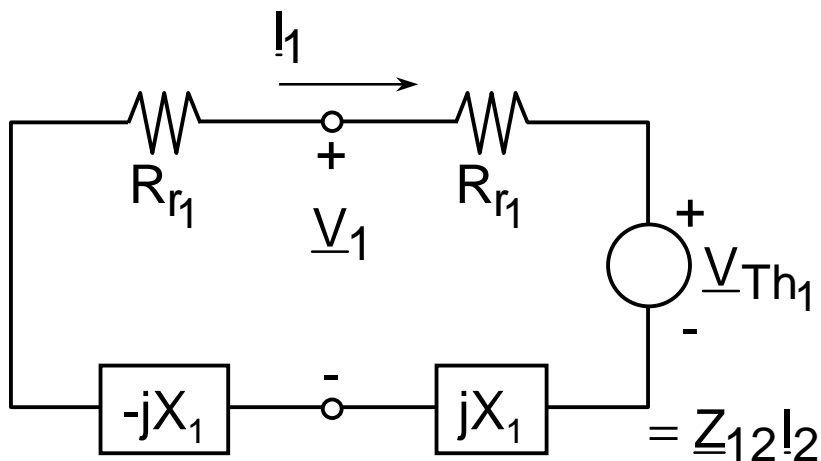
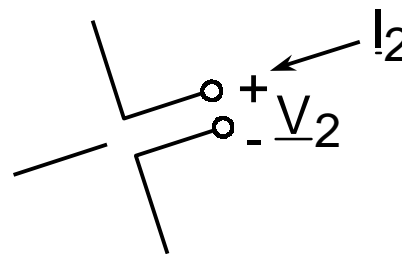
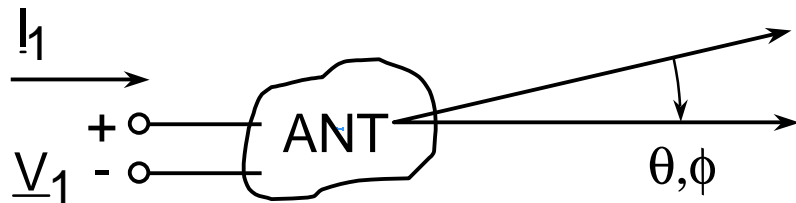
For short dipole: $A_{\text{eff}}(\theta) = \frac{2\eta_0 P_{\text{rec}}}{|\bar{E}_{\text{inc}}|^2} = \frac{\eta_0 d_{\text{eff}}^2 \sin^2 \theta}{4R_r} = \frac{\lambda^2 3}{8\pi} \sin^2 \theta$

Therefore: $A_e(\theta, \phi) = \frac{\lambda^2}{4\pi} G(\theta, \phi) (\text{m}^2)$ [true for almost all antennas]

Recall, for short dipole: $G(\theta) = 1.5 \sin^2 \theta$ [$\neq f(\omega)$]

PROOF THAT $A = G\lambda^2/4\pi$ FOR MOST ANTENNAS

Test Range = Unknown plus Short Dipole Antenna:



$$P_{\text{rec}_1} = \frac{|Z_{12}I_2|^2}{8R_{r1}} = P_{t2} \frac{G_2}{4\pi r^2} A_1$$

$$P_{\text{rec}_2} = \frac{|Z_{21}I_1|^2}{8R_{r2}} = P_{t1} \frac{G_1}{4\pi r^2} A_2$$

(Power transmitted by antenna #1)

Wm^{-2}
at antenna 2

PROOF THAT $A = G\lambda^2/4\pi$ FOR MOST ANTENNAS (2)

$$P_{\text{rec}1} = \frac{|Z_{12}I_2|^2}{8R_{r1}} = P_{t2} \frac{G_2}{4\pi r^2} A_1 \quad P_{\text{rec}2} = \frac{|Z_{21}I_1|^2}{8R_{r2}} = P_{t1} \frac{G_1}{4\pi r^2} A_2$$

$$\therefore \frac{P_{\text{rec}2}}{P_{\text{rec}1}} = \frac{G_1 A_2 P_{t1}}{G_2 A_1 P_{t2}} \Rightarrow \frac{A_1}{G_1} = \frac{A_2}{G_2} \left[\frac{P_{t1}}{P_{t2}} \cdot \frac{P_{\text{rec}1}}{P_{\text{rec}2}} \right]$$

$$\text{But } \frac{P_{\text{rec}1}}{P_{\text{rec}2}} = \frac{|Z_{12}I_2|^2}{|Z_{21}I_1|^2} \cdot \frac{R_{r2}}{R_{r1}} = \frac{|Z_{12}|^2}{|Z_{21}|^2} \cdot \frac{P_{t2}}{P_{t1}}$$

Therefore, if $|Z_{12}|^2 = |Z_{21}|^2$, then

$$\frac{A_1}{G_1} = \frac{A_2}{G_2} = \frac{\lambda^2}{4\pi} \text{ Q.E.D.}$$

RECIPROCITY AND NON-RECIPROCAL DEVICES

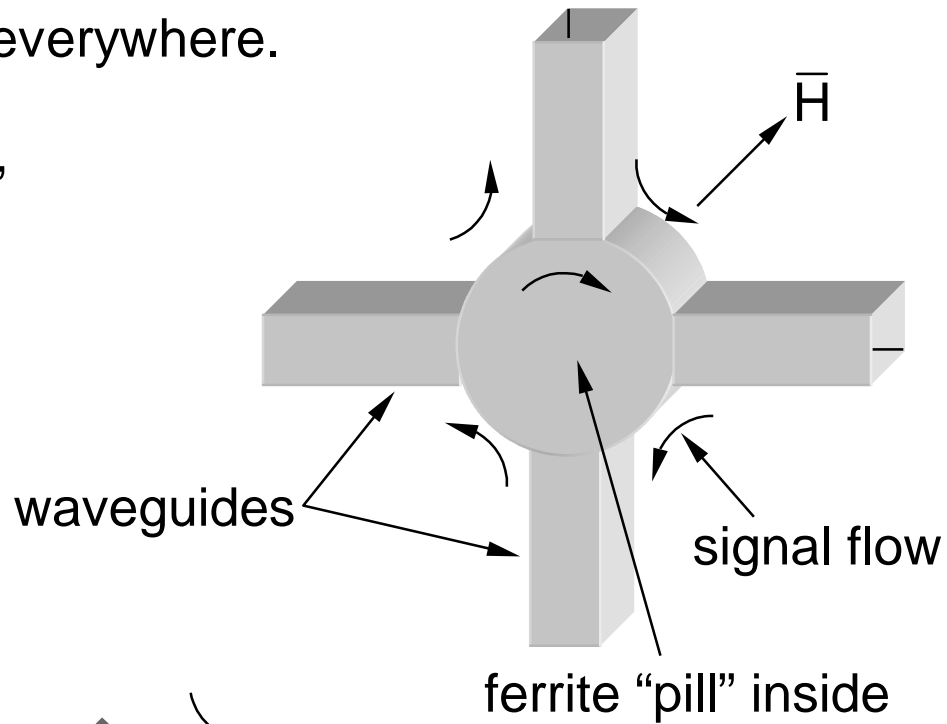
Reciprocity:

$$|Z_{12}|^2 = |Z_{21}|^2 \text{ if } \bar{\epsilon} = \bar{\epsilon}_t, \bar{\mu} = \bar{\mu}_t \text{ everywhere.}$$

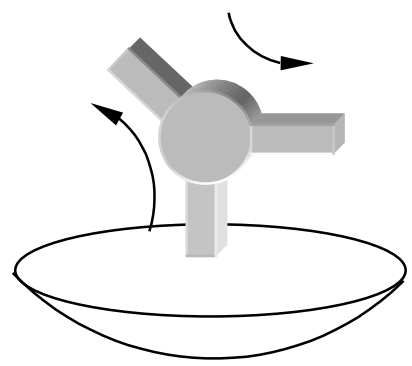
Exceptions: magnetized plasmas,
magnetized ferrites

Non-reciprocal Devices:

4-Port Circulators



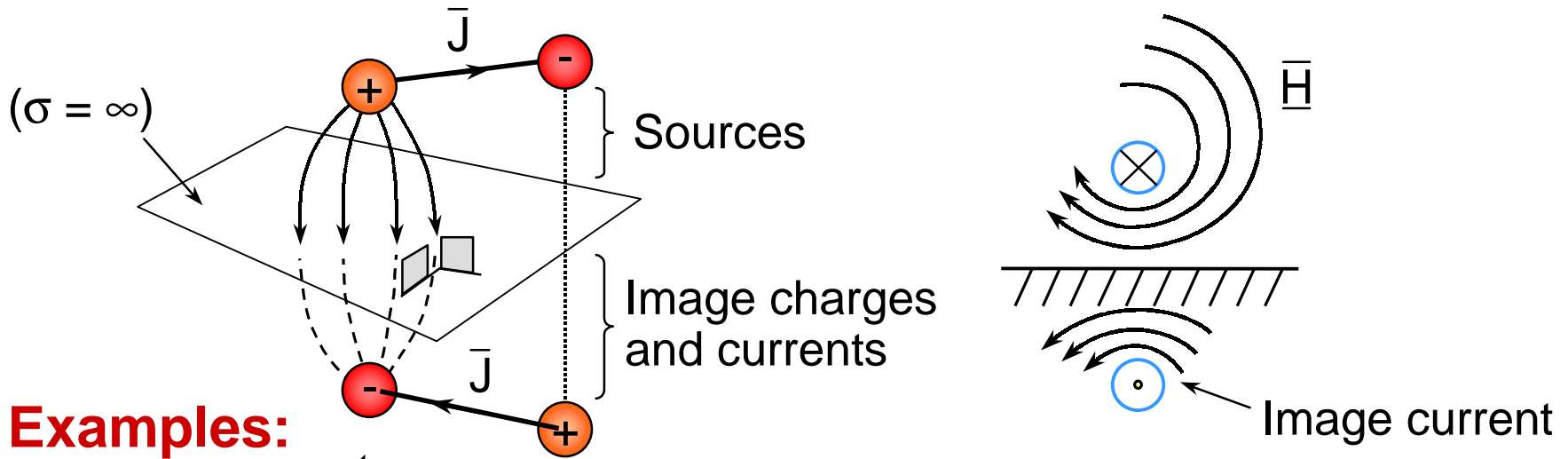
Non-reciprocal Antennas:



MIRROR IMAGES

Mirror Images: Infinite flat conducting surfaces are “mirrors”

Consider the charges and currents shown, and how \bar{E} must everywhere be perpendicular to the mirror, and \bar{H} must be parallel



Examples:

