

**6.012 Electronic Devices and Circuits**  
Formula Sheet for Final Exam, Fall 2003

Parameter Values:

$$q = 1.6 \times 10^{19} \text{ Coul}$$

$$\epsilon_0 = 8.854 \times 10^{-14} \text{ F/cm}, \quad \epsilon_{\text{Si}} = 11.7, \quad \epsilon_{\text{SiO}_2} = 3.9$$

$$\epsilon_{\text{Si}} = 10^{-12} \text{ F/cm}, \quad \epsilon_{\text{SiO}_2} = 3.5 \times 10^{-13} \text{ F/cm}$$

$$n_i[\text{Si@RT}] = 10^{10} \text{ cm}^{-3}$$

$$kT/q = 0.025 \text{ V}; \quad (kT/q) \ln 10 = 0.06 \text{ V}$$

$$m = 1 \times 10^{-4} \text{ cm}$$

Periodic Table:

III	IV	V
B	C	N
Al	Si	P
Ga	Ge	As
In	Sn	Sb

Drift/Diffusion:

Drift velocity :  $\bar{v}_x = \pm \mu E_x$

Conductivity :  $\sigma = q(e n + h p)$

Diffusion flux :  $F_m = D_m \frac{\partial C_m}{\partial x}$

Einstein relation :  $\frac{D_m}{\mu} = \frac{kT}{q}$

Electrostatics:

$$\frac{dE(x)}{dx} = \rho(x) \quad E(x) = \frac{1}{\epsilon} \int \rho(x) dx$$

$$\frac{dV(x)}{dx} = -E(x) \quad V(x) = -\int E(x) dx$$

$$\frac{d^2 V(x)}{dx^2} = -\frac{\rho(x)}{\epsilon} \quad V(x) = \frac{1}{2\epsilon} \int \rho(x) dx$$

The Five Basic Equations:

Electron concentration :  $\frac{\partial n(x,t)}{\partial t} + \frac{1}{q} \frac{\partial J_e(x,t)}{\partial x} = g_L(x,t) - [n(x,t) \cdot p(x,t) - n_i^2] r(T)$

Hole concentration :  $\frac{\partial p(x,t)}{\partial t} + \frac{1}{q} \frac{\partial J_h(x,t)}{\partial x} = g_L(x,t) - [n(x,t) \cdot p(x,t) - n_i^2] r(T)$

Electron current density :  $J_e(x,t) = q e n(x,t) E(x,t) + q D_e \frac{\partial n(x,t)}{\partial x}$

Hole current density :  $J_h(x,t) = q h p(x,t) E(x,t) - q D_h \frac{\partial p(x,t)}{\partial x}$

Poisson's equation :  $\frac{\partial E(x,t)}{\partial x} = \frac{q}{\epsilon} [p(x,t) - n(x,t) + N_d^+(x) - N_a^-(x)]$

Uniform doping, full ionization, TE

n - type,  $N_d \gg N_a$

$$n_o \approx N_d, \quad N_a \approx 0, \quad p_o = n_i^2 / n_o, \quad n_i = \frac{kT}{q} \ln \frac{N_D}{n_i}$$

p - type,  $N_a \gg N_d$

$$p_o \approx N_a, \quad N_d \approx 0, \quad n_o = n_i^2 / p_o, \quad p_i = \frac{kT}{q} \ln \frac{N_A}{n_i}$$

Uniform optical excitation, uniform doping

$$n = n_o + n', \quad p = p_o + p', \quad n' = p' \quad \frac{dn'}{dt} = g_l(t) - (p_o + n_o + n') n' r$$

Low level injection,  $n', p' \ll p_o + n_o$  :  $\frac{dn'}{dt} + \frac{n'}{\tau_{\min}} = g_l(t)$  with  $\tau_{\min} = (p_o r)^{-1}$

Flow problems (uniformly doped quasineutral regions with quasi-static excitation and low level injection; p-type example):

$$\begin{aligned}
 \text{Minority carrier excess:} \quad & \frac{d^2 n'(x)}{dx^2} = \frac{n'(x)}{L_e^2} = \frac{1}{D_e} g_L(x) & L_e \equiv \sqrt{D_e \tau_e} \\
 \text{Minority carrier current density:} \quad & J_e(x) = q D_e \frac{dn'(x)}{dx} \\
 \text{Majority carrier current density:} \quad & J_h(x) = J_{Tot} - J_e(x) \\
 \text{Electric field:} \quad & E_x(x) = -\frac{1}{q} \frac{dJ_h(x)}{dx} = \frac{D_h}{D_e} J_e(x) \\
 \text{Majority carrier excess:} \quad & p'(x) = n'(x) + \frac{dE_x(x)}{q dx}
 \end{aligned}$$

Non-uniformly doped semiconductor sample in thermal equilibrium

$$\begin{aligned}
 \frac{d^2 n(x)}{dx^2} &= \frac{q}{D_n} \left\{ n_i \left[ e^{q(x)/kT} - e^{-q(x)/kT} \right] \left[ N_d(x) - N_a(x) \right] \right\} \\
 n_o(x) &= n_i e^{q(x)/kT}, \quad p_o(x) = n_i e^{-q(x)/kT}, \quad p_o(x)n_o(x) = n_i^2
 \end{aligned}$$

Depletion approximation for abrupt p-n junction:

$$\begin{aligned}
 n(x) &= \begin{cases} 0 & \text{for } x < x_p \\ qN_{Ap} & \text{for } x_p < x < 0 \\ qN_{Dn} & \text{for } 0 < x < x_n \\ 0 & \text{for } x_n < x \end{cases} & N_{Ap}x_p = N_{Dn}x_n \\
 & & x_p \equiv -x_n = \frac{kT}{q} \ln \frac{N_{Dn}N_{Ap}}{n_i^2}
 \end{aligned}$$

$$\begin{aligned}
 w(v_{AB}) &= \sqrt{\frac{2 \epsilon_s \epsilon_0 (v_{AB})}{q} \frac{(N_{Ap} + N_{Dn})}{N_{Ap}N_{Dn}}} & |E_{pk}| &= \sqrt{\frac{2q \epsilon_s \epsilon_0 (v_{AB})}{\epsilon_s} \frac{N_{Ap}N_{Dn}}{(N_{Ap} + N_{Dn})}}
 \end{aligned}$$

$$q_{DP}(v_{AB}) = AqN_{Ap}x_p(v_{AB}) = A \sqrt{2q \epsilon_s \epsilon_0 (v_{AB})} \frac{N_{Ap}N_{Dn}}{(N_{Ap} + N_{Dn})}$$

Ideal p-n junction diode i-v relation:

$$n(-x_p) = \frac{n_i^2}{N_{Ap}} e^{qV_{AB}/kT}, \quad n'(-x_p) = \frac{n_i^2}{N_{Ap}} \left( e^{qV_{AB}/kT} - 1 \right); \quad p(x_n) = \frac{n_i^2}{N_{Dn}} e^{-qV_{AB}/kT}, \quad p'(x_n) = \frac{n_i^2}{N_{Dn}} \left( e^{-qV_{AB}/kT} - 1 \right)$$

$$i_D = Aq n_i^2 \left[ \frac{D_h}{N_{Dn} w_{n,eff}} + \frac{D_e}{N_{Ap} w_{p,eff}} \right] \left[ e^{qV_{AB}/kT} - 1 \right] \quad w_{m,eff} = \begin{cases} w_m & \text{if } L_m \gg w_m \\ L_m \tanh[(w_m - x_m)/L_m] & \text{if } L_m \sim w_m \\ L_m & \text{if } L_m \ll w_m \end{cases}$$

$$q_{QNR,p-side} = Aq \int_{-w_p}^{-x_p} n'(x) dx, \quad q_{QNR,n-side} = Aq \int_{x_n}^{w_n} p'(x) dx, \quad \text{Note: } p'(x) \text{ } n'(x) \text{ in QNRs}$$

Ebers-Moll Model for Bipolar Junction Transistor (BJT) characteristics (npn example; no base width modulation):

$$i_E = i_{hE} + i_{eE} = Aqn_i^2 \frac{D_h}{N_{DE}w_{E,eff}} + \frac{D_e}{N_{AB}w_{B,eff}} \left[ e^{qV_{BE}/kT} - 1 \right]$$

$$i_C = i_{eE}(1 - \beta) = Aqn_i^2 \frac{D_e}{N_{AB}w_{B,eff}} \left[ e^{qV_{BE}/kT} - 1 \right] (1 - \beta) \quad \text{with} \quad \beta = \frac{w_{B,eff}^2}{2D_e \tau_e} = \frac{w_{B,eff}^2}{2L_e^2}$$

$$i_B = i_{hE} + \beta i_{eE} = i_{eE}(\beta + 1) = Aqn_i^2 \frac{D_e}{N_{AB}w_{B,eff}} \left[ e^{qV_{BE}/kT} - 1 \right] (\beta + 1) \quad \beta = \frac{i_C}{i_B} = \frac{(1 - \beta)}{(\beta + 1)}$$

Large Signal BJT Model in Forward Active Region (FAR) (npn; with base width mod):

$$i_B(v_{BE}, v_{CE}) = I_{BS} \left[ e^{qV_{BE}/kT} - 1 \right] \quad \text{with} \quad I_{BS} \equiv \frac{1}{(\beta + 1)} I_{ES} = \frac{1}{(\beta + 1)} Aqn_i^2 \frac{D_{eB}}{w_{B,eff} N_{AB}} + \frac{D_{hE}}{w_{E,eff} N_{DE}}$$

$$i_C(v_{BE}, v_{CE}) = \beta [1 + v_{CE}] i_B(v_{BE}, v_{CE}) = \beta I_{BS} \left[ e^{qV_{BE}/kT} - 1 \right] [1 + v_{CE}]$$

Break - point model:  $v_{BE,on} = 0.6V$ ,  $v_{CE,sat} = 0.2V$

MOS Capacitor:

Flat - band voltage:  $V_{FB} \equiv v_{GB}$  at which  $\phi_s = 0$

$$V_{FB} = \phi_{p, Si} - \phi_m$$

Threshold voltage:  $V_T \equiv v_{GC}$  at which  $\phi_s = \phi_{p, Si} + v_{BC}$

$$V_T(v_{BC}) = V_{FB} - \phi_{p, Si} + \frac{1}{C_{ox}^*} \left\{ 2 \phi_{p, Si} q N_A \left[ \left| 2 \phi_{p, Si} + v_{BC} \right| \right]^{1/2} \right\} \quad x_{DT}(v_{BC}) = \sqrt{\frac{2 \phi_{p, Si} \left[ \left| 2 \phi_{p, Si} + v_{BC} \right| \right]}{q N_A}}$$

Inversion layer sheet charge density:  $q_N^* = C_{ox}^* [v_{GC} - V_T(v_{BC})]$

Accumulation layer sheet charge density:  $q_P^* = C_{ox}^* [v_{GB} - V_{FB}(v_{BC})]$

Gradual Channel Approx. for MOSFET characteristics (n-channel; no channel length mod.):

Valid for  $v_{BS} = 0$ , and  $v_{DS} \geq 0$ :

$$i_G(v_{GS}, v_{DS}, v_{BS}) = 0 \quad \text{and} \quad i_B(v_{GS}, v_{DS}, v_{BS}) = 0$$

$$0 \quad \text{for} \quad \frac{1}{L} [v_{GS} - V_T(v_{BS})] < 0 < v_{DS}$$

$$i_D(v_{GS}, v_{DS}, v_{BS}) = \frac{1}{2} \frac{W}{L} q N_A \mu_n C_{ox}^* [v_{GS} - V_T(v_{BS})]^2 \quad \text{for} \quad 0 < \frac{1}{L} [v_{GS} - V_T(v_{BS})] < v_{DS}$$

$$\frac{W}{L} q N_A \mu_n C_{ox}^* v_{GS} - V_T(v_{BS}) \frac{v_{DS}}{2} \quad \text{for} \quad 0 < v_{DS} < \frac{1}{L} [v_{GS} - V_T(v_{BS})]$$

$$\text{with} \quad V_T(v_{BS}) \equiv V_{FB} - \phi_{p, Si} + \frac{1}{C_{ox}^*} \left\{ 2 \phi_{p, Si} q N_A \left[ \left| 2 \phi_{p, Si} + v_{BS} \right| \right]^{1/2} \right\}$$

$$\equiv 1 + \frac{1}{C_{ox}^*} \frac{q N_A}{2 \left[ \left| 2 \phi_{p, Si} + v_{BS} \right| \right]^{1/2}} \quad C_{ox}^* \equiv \frac{q \epsilon_{ox}}{t_{ox}}$$

Large Signal MOSFET Model in Saturation (FAR) (n-channel; with base width mod.):

$$i_G(v_{GS}, v_{DS}, v_{BS}) = 0 \quad i_B(v_{GS}, v_{DS}, v_{BS}) = 0$$

$$i_D(v_{GS}, v_{DS}, v_{BS}) = \frac{K}{2} [v_{GS} - V_T(v_{BS})]^2 [1 + \lambda v_{DS}]$$

with  $K \equiv \frac{W}{L} \mu_n C_{ox}^*$  and  $V_T = V_{FB} - 2 \lambda_p \lambda_{Si} + \frac{1}{C_{ox}^*} \left\{ 2 \lambda_{Si} q N_A \left[ 2 \lambda_p \lambda_{Si} |v_{BS}| \right] \right\}^{1/2}$

Small signal linear equivalent circuits:

p-n Diode

$$g_d = \frac{q}{kT} I_{BS} e^{qV_{AB}/kT} \quad \frac{qI_D}{kT}$$

$$C_d = C_{dp} + C_{df}, \text{ where } C_{dp}(V_{AB}) = A \sqrt{\frac{q \lambda_{Si} N_{Ap}}{2(\lambda_p V_{AB})}} \quad \text{and}$$

$$C_{df}(V_{AB}) = \frac{qI_D}{kT} \frac{[w_p \lambda_p]^2}{2D_e} = g_d \lambda_p \quad \text{with } \lambda_p \equiv \frac{[w_p \lambda_p]^2}{2D_e}$$

BJT (in FAR)

$$g_m = \frac{q|I_C|}{kT} \quad g_o = \frac{g_m}{\beta} \quad g_o = |I_C| \quad \text{or} \quad \left| \frac{I_C}{V_A} \right|$$

$$C_{be} = g_m \lambda_b + \text{B-E depletion capacitance, where } \lambda_b = \frac{w_B^2}{2D_{minority \text{ in base}}}$$

$$C_{bc} = \text{B-C depletion capacitance}$$

MOSFET (in saturation)

$$g_m = \sqrt{2K |I_D|} = K |V_{GS} - V_T| = \frac{2I_D}{(V_{GS} - V_T)} \quad g_o = |I_D| \quad \text{or} \quad \left| \frac{I_D}{V_A} \right|$$

$$g_{mb} = g_m = \sqrt{2K |I_D|} \quad \text{with } \lambda_p = \frac{1}{C_{ox}^*} \sqrt{\frac{\lambda_{Si} q N_A}{|q \lambda_p| V_{BS}}}$$

$$C_{gs} = \frac{2}{3} W L C_{ox}^* \quad C_{sb}, C_{gb}, C_{db} : \text{ depletion region capacitances}$$

$$C_{gd} = W C_{gd}^* \quad \text{where } C_{gd}^* \text{ is the gate-to-drain fringing and overlap capacitance per unit gate width}$$

## Single transistor analog circuit building block stages

### Bipolar:-based stages

	Voltage gain, $A_v$	Current gain, $A_i$	Input resistance, $R_i$	Output resistance, $R_o$
Common emitter	$\frac{g_m}{[g_o + g_l]} (= g_m r_l')$	$\frac{g_l}{[g_o + g_l]}$	$r$	$r_o = \frac{1}{g_o}$
Common base	$\frac{g_m}{[g_o + g_l]} (= g_m r_l')$	1	$\frac{r}{[+1]}$	$[+1]r_o$
Emitter follower	$\frac{[g_m + g_l]}{[g_m + g_l + g_o + g_l]} = 1$	$\frac{g_l}{[g_o + g_l]}$	$r + [+1]r_l'$	$\frac{r_l + r}{[+1]}$
Emitter degeneration (series feedback)	$-\frac{r_l}{R_F}$		$r + [+1]R_F$	$r_o$
Shunt feedback	$\frac{[g_m - G_F]}{[g_o + G_F]} = g_m R_F$	$\frac{g_l}{G_F}$	$\frac{1}{g + G_F[1 - A_v]}$	$r_o \parallel R_F = \frac{1}{[g_o + G_F]}$

### MOSFET-based stages

	Voltage gain, $A_v$	Current gain, $A_i$	Input resistance, $R_i$	Output resistance, $R_o$
Common source	$g_m r_l'$	•	•	$r_o = \frac{1}{g_o}$
Common gate	$[g_m + g_{mb}]r_l'$	1	$\frac{1}{[g_m + g_{mb}]}$	$r_o \left( 1 + \frac{[g_m + g_{mb} + g_o]}{g_t} \right)$
Source follower	$\frac{g_m}{[g_m + g_o + g_l]} = 1$	•	•	$\frac{1}{[g_m + g_o + g_l]} = \frac{1}{g_m}$
Source degeneration (series feedback)	$-\frac{r_l}{R_F}$	•	•	$r_o$
Shunt feedback	$\frac{[g_m - G_F]}{[g_o + G_F]} = g_m R_F$	$\frac{g_l}{G_F}$	$\frac{R_F}{G_F[1 - A_v]}$	$r_o \parallel R_F = \frac{1}{[g_o + G_F]}$

### OCTC/SCTC

$$\text{OCTC estimation of } H_{HI} : H_{HI} \left[ \frac{1}{i} \right]^1 = \frac{1}{i} R_i C_i$$

with  $R_i$  defined as the equivalent resistance in parallel with  $C_i$ , with all other parasitic device C's ( $C_s$ 's,  $C_{gs}$ 's,  $C_{gd}$ 's, etc.) open circuited.

$$\text{SCTC estimation of } L_{LO} : L_{LO} \geq \frac{1}{j} = \left[ \frac{1}{j} R_j C_j \right]^1$$

with  $R_j$  defined as the equivalent resistance in parallel with  $C_j$ , with all other biasing and coupling C's ( $C_I$ 's,  $C_O$ 's,  $C_E$ 's,  $C_S$ 's, etc.) short circuited.

## Difference- and Common-mode signals

Given two signals,  $v_1$  and  $v_2$ , we can decompose them into two new signals, one ( $v_C$ ) that is common to both  $v_1$  and  $v_2$ , and one ( $v_D$ ) that makes an equal, but opposite polarity, contribution to  $v_1$  and  $v_2$ :

$$v_D \equiv v_1 - v_2 \quad \text{and} \quad v_C \equiv \frac{v_1 + v_2}{2} \quad v_1 = v_C + \frac{v_D}{2} \quad \text{and} \quad v_2 = v_C - \frac{v_D}{2}$$

## CMOS performance

### Transfer characteristic

$$\text{In general: } V_{LO} = 0, \quad V_{HI} = V_{DD}, \quad I_{ON} = 0, \quad I_{OFF} = 0$$

$$\text{Symmetry: } V_M = \frac{V_{DD}}{2} \quad \text{and} \quad N_{ML} = N_{MH} \quad K_n = K_p \quad \text{and} \quad |V_{Tp}| = V_{Tn}$$

$$\text{Minimum size gate: } L_n = L_p = L_{\min}, \quad W_p = \left( \frac{n}{p} \right) W_n, \quad W_n = W_{\min}$$

### Switching times and Gate delay

$$\begin{aligned} \tau_{charge} &= \tau_{discharge} = \frac{2V_{DD}C_L}{K_n [V_{DD} - V_{Tn}]^2} \\ C_L &= n(W_n L_n + W_p L_p) C_{ox}^* = 3nW_{\min} L_{\min} C_{ox}^* \quad \text{assumes } t_{ox} = 2 \mu m \\ \tau_{Min.Cycle} &= \tau_{charge} + \tau_{discharge} = \frac{12nL_{\min}^2 V_{DD}}{e [V_{DD} - V_{Tn}]^2} \end{aligned}$$

### Power dissipation

$$\begin{aligned} P_{ave@Max.f} &= C_L V_{DD}^2 f_{\max} \mu \frac{C_L V_{DD}^2}{\tau_{Min.Cycle}} = \frac{e W_{\min} C_{ox}^* V_{DD} [V_{DD} - V_{Tn}]^2}{L_{\min}} \\ PD_{ave@Max.f} &= \frac{P_{ave@Max.f}}{\text{Inverter area}} \mu \frac{P_{ave@Max.f}}{W_{\min} L_{\min}} = \frac{e_{ox} V_{DD} [V_{DD} - V_{Tn}]^2}{t_{ox} L_{\min}^2} \end{aligned}$$