

3.044 Recitation 5

March 3-4, 2005

Topics

- * PSET 2, 3
- * Casting: Solid-Liquid Process
- * Preparation for Test 1

Dimensional Analysis

Given the Gaussian Temperature function as

$$T - T_{int} = \frac{\beta}{\rho C_p \sqrt{\pi \alpha t}} \exp\left(-\frac{x^2}{4\alpha t}\right)$$

- 1) All variables: $T - T_{int}$, x , t , α , $(\beta/\rho C_p)$: $n=5$
- 2) Base units: K , m , s , $\frac{m^2}{s}$, mK : K , m , $s \Rightarrow T, L, t$: $r=3$
- 3) Number of dimensionless group: $m=n-r=2$
- 4) Keep: ΔT , x : Eliminate: t , α , $(\beta/\rho C_p)$
- 5) Form 2 π groups

$$\pi_{\Delta T} = [T - T_{int}]^a [t]^b [\alpha]^c [\beta/\rho C_p]^d$$

$$\pi_{\Delta T} = [T]^a [t]^b [\frac{L^2}{t}]^c [LT]^d = [T]^{a+b} [t]^{b-c} [L]^{2c+d} = T^0 t^0 L^0 \Rightarrow c = -1, b = \frac{1}{2}, a = \frac{1}{2}$$

$$\pi_{\Delta T} = \frac{(T - T_{int}) \rho C_p \sqrt{\alpha t}}{\beta}$$

$$\pi_x = [x]^a [t]^b [\alpha]^c [\beta/\rho C_p]^d$$

$$\pi_x = [L]^a [t]^b [\frac{L^2}{t}]^c [LT]^d = [T]^c [t]^{b-c} [L]^{a+2c+d} = [T]^0 [t]^0 [L]^0 \Rightarrow c = 0, b = -\frac{1}{2}, a = -\frac{1}{2}$$

$$\pi_x = \frac{x}{\sqrt{\alpha t}}$$

$$\pi_{\Delta T} = \frac{1}{\sqrt{\pi}} \exp\left(-\frac{\pi x^2}{4}\right)$$

Casting: Solid-Liquid Processes

In solidification process, the solid liquid interface moves with time ($X(t)$). $Bi_s = hX(t)/k$, so Bi_s changes with time. The solidification rate depends on the type of mold, metals being cast, and mold geometry. The net heat fluxes through the solid/liquid interface is the latent heat released during solidification.

$$\vec{q}_s \cdot \hat{n} - \vec{q}_l \cdot \hat{n} = -\rho \Delta H_M \frac{dX}{dt}$$

$\vec{q} \cdot \hat{n}$ is negative if the heat transfer direction is opposite to the normal vector of the interface. Therefore, if more heat is removed from solid than heat from liquid put into the interface, dX/dt is positive. Using this equation, we can derive the thickness of solidified metal (X) and solidification rate (dX/dt) for different casting processes.

There are several types of molds used for metal casting. Two most common molds are metal mold and sand mold. Metal is a better heat conductor than sand. Therefore heat is transferred at faster rate in the metal mold than in the sand mold. Simplified case studies for each type of mold will be discussed.

Metal Mold (example in class)

- Good conductor
- Internal water cooling: surface conduction is dominant. $T_{mold} = T_{env}$
- Assume linear T profile through solid phase

Energy balance equation

Heat transferred at the mold surface = Heat conducted thru the solid phase = Latent heat during solidification

$$|q| = h(T_s - T_{env}) = \frac{k_s(T_m - T_{env})}{X}|_{S/L} = \rho \Delta H_M \frac{dX}{dt}|_{x=0}$$

At short time ($T_s = T_m$)

$$|q| = h(T_s - T_{env}) = \rho \Delta H_M \frac{dX}{dt}$$

$$X = \frac{h(T_m - T_{env})}{\rho \Delta H_M} t \quad \text{Linear growth (constant growth rate)}$$

At long time ($T_s = T_{env}$)

$$|q| = \frac{k_s(T_m - T_s)}{X} = \frac{k_s(T_m - T_{env})}{X} = \rho \Delta H_M \frac{dX}{dt}$$

$$\int_0^t \frac{k_s(T_m - T_{env})}{\rho \Delta H_M} dt = \int_0^X X dX$$

$$\frac{k_s(T_m - T_{env})}{\rho \Delta H_M} t \Big|_0^t = \frac{X^2}{2} \Big|_{X=0}$$

$$\frac{k_s(T_m - T_{env})}{\rho \Delta H_M} t = \frac{X^2}{2}$$

$$X = \sqrt{\frac{2k_s(T_m - T_{env})}{\rho \Delta H_M}} \sqrt{t}$$

Sand Mold

- Poor conductor
- Assume uniform T profile in solid $T_s = T_m$
- erf like T profile in the mold $T - T_m = (T_{env} - T_m) \text{erf}\left(\frac{X}{2\sqrt{\alpha t}}\right)$

Energy balance equation

Heat transferred at the mold surface = Latent heat during solidification

$$|q| = k_{mold} \frac{dT}{dX} \Big|_{x=0} = \frac{k_{mold}(T_m - T_{env})}{\sqrt{\pi \alpha_{mold} t}} = \rho \Delta H_M \frac{dX}{dt}$$

$$\int_0^t \frac{k_{mold}(T_m - T_{env})}{\rho \Delta H_M \sqrt{\pi \alpha_{mold} t}} dt = \int_0^X dX$$

$$\frac{k_{mold}(T_m - T_{env})}{\rho \Delta H_M \sqrt{\pi \alpha_{mold}}} 2t^{1/2} \Big|_0^t = X \Big|_{X=0}$$

$$X = \frac{2}{\sqrt{\pi}} \frac{k_{mold}(T_m - T_{env})}{\sqrt{\alpha_{mold}} \rho \Delta H_M} \sqrt{t}$$

Preparation for Test 1

Math

- Vectors: Dot, Cross, Gradient, Divergence, Curl
- erf and erfc function: graph, derivatives

Steady State: 1D Heat conduction ($0 = \alpha \nabla^2 T + \frac{\dot{q}}{\rho C_p}$)

- Single layer: slab, cylinder, sphere
- Multilayered wall: flat, cylinder, sphere
- Heat flow $Q=qA$ is constant in any shape
- Approximate time to steady state for a thin body

Unsteady State: 1D Heat conduction ($\frac{\partial T}{\partial t} = \alpha \nabla^2 T + \frac{\dot{q}}{\rho C_p}$)

- Unlimited heat source: erf
- Limited heat source: Gaussian
- Welding $\delta(T_0 - T_i) = H / (\rho C_p)$: H =total heat for thermal boundary layer. 2δ for infinite domain

Biot Number and Fourier Number

- Small Bi: Uniform temperature in the body
- Large Bi: Large temperature gradient in the body
- How to apply Fo and Bi in practice

Finite Difference

- Explicit timestepping method
- Mesh Fourier number
- Maximum Δt

Dimensional Analysis

- Represent some physical features
- Dimensionless form of equation
- Buckingham Pi Theorem

Radiation

- Black body is a perfect emitter.
- Emissivity of any body will be a fraction of black body emissivity
- Unsteady state heat transfer by radiation

Economic Models in Engineering

- Present value, Future value, Equal payment
- NPV and Annual payment
- Product volume and Effective Production Volume
- Dedicated equipment cost
- Non-Dedicated equipment cost
- Material cost