

3.2 March 2, 2005: Moving Body, Stability

Recall: vacuum arc remelting. Setup, geometry, frame of reference, relative z -velocity $u_z < 0$. Convective flux $\vec{q} = "H\vec{u}"$ or $\rho c_p \vec{u}$, Back up a couple of steps:

$$\rho c_p \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial z^2} - \rho c_p u_z \frac{\partial T}{\partial z} + \dot{q} \quad (3.9)$$

Cancel ρc_p :

$$\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial z^2} - u_z \frac{\partial T}{\partial z} + \frac{\dot{q}}{\rho c_p} \quad (3.10)$$

Go through terms: regular accumulation, regular second derivative with thermal diffusivity. Next the convective term, discuss in terms of units and derivatives. Rewrite again in terms of substantial derivative:

$$\frac{DT}{Dt} = \alpha \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{\rho c_p} \quad (3.11)$$

Steady-state, no generation: temperature depends only on z , not t :

$$\alpha \frac{d^2 T}{dz^2} - u_z \frac{dT}{dz} = 0 \quad (3.12)$$

Simple solution using the characteristic polynomial, $R = 0$, u_z/α . Result:

$$T = A + B \exp\left(\frac{u_z z}{\alpha}\right) \quad (3.13)$$

Fit to boundary conditions: $z = 0 \Rightarrow T = T_M$, $z = \infty \Rightarrow T = T_i$ so use erf-style:

$$\frac{T - T_i}{T_M - T_i} = \exp\left(\frac{u_z z}{\alpha}\right) \quad (3.14)$$

Lengthscale = α/u_z . Graph, noting that u_z is negative. Titanium $\alpha = 0.1 \frac{\text{cm}^2}{\text{s}}$, $u_z \sim 5 \frac{\text{cm}}{\text{min}} = \frac{1}{12} \frac{\text{cm}}{\text{s}}$, so $\alpha/u_z = 1.2 \text{cm}$, about 1/2 inch. So only the bottom few centimeters are heated at all, even at this low velocity!

Heat flux into the bottom:

$$q_z = -k \frac{\partial T}{\partial z} = -k(T_m - T_i) \frac{u_z}{\alpha} \exp\left(\frac{u_z z}{\alpha}\right) = -\rho c_p u_z (T_m - T_i) \quad (3.15)$$

Note $\rho c_p (T_m - T_i)$ is the enthalpy per unit volume to heat metal to its melting point. Mult by u_z for enthalpy per unit area to heat metal coming at a rate of u_z , which is a cool result.

This is heat flux into the solid. What about into the liquid? Remember last time:

$$\vec{q}_s \cdot \hat{n} - \vec{q}_l \cdot \hat{n} = -\rho \Delta H_M \frac{dX}{dt} \quad (3.16)$$

Replace dX/dt with u_z and we're done, need to supply the heat of melting and of getting to this temperature. Here larger \vec{q}_l than \vec{q}_s , both positive, so dX/dt positive.

Stability Is the VAR melt front stable? What if we have a bump, or groove?

Solidification: is the growing solid shell stable?

What about a solid particle growing into an undercooled liquid?

What about alloy solidification?