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2.094 Finite Element Analysis of Solids and Fluids
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2.094

FINITE ELEMENT ANALYSIS OF SOLIDS AND FLUIDS

SPRING 2008

Homework 7 - Solution

Instructor: Prof. K. J. Bathe

Assigned: 04/03/2008
Due: 04/10/2008

Problem 1 (20 points):

(a)

$${}^0X = {}^0R {}^0U = \begin{bmatrix} \cos 45^\circ & -\sin 45^\circ \\ \sin 45^\circ & \cos 45^\circ \end{bmatrix} \begin{bmatrix} \frac{1}{2} & 0 \\ 0 & \frac{3}{4} \end{bmatrix} = \frac{1}{\sqrt{2}} \begin{bmatrix} \frac{1}{2} & -\frac{3}{4} \\ \frac{1}{2} & \frac{3}{4} \end{bmatrix}$$

$${}^tX = ({}^0X)^{-1} = \begin{bmatrix} \sqrt{2} & \sqrt{2} \\ -\frac{2\sqrt{2}}{3} & \frac{2\sqrt{2}}{3} \end{bmatrix}$$

(b)

$${}^t\varepsilon = \frac{1}{2} ({}^tX^T {}^tX - I) = \begin{bmatrix} \frac{17}{18} & \frac{5}{9} \\ \frac{5}{9} & \frac{17}{18} \end{bmatrix}$$

$${}^tS = \begin{bmatrix} 11 & 7 & 0 \\ 7 & 11 & 0 \\ 0 & 0 & 9 \end{bmatrix} \begin{bmatrix} \frac{17}{18} \\ \frac{17}{18} \\ \frac{5}{9} \end{bmatrix} = \begin{bmatrix} 17 \\ 17 \\ 5 \end{bmatrix}$$

$$\frac{{}^t\rho}{{}^0\rho} = \frac{{}^0V}{{}^tV} = \frac{(1.5)(1)(thickness)}{(2)(2)(thickness)} = \frac{3}{8}$$

Therefore,

$${}^t \underline{\tau} = \frac{{}^t \rho}{\rho} {}^t \underline{X} {}^t \underline{S} {}^t \underline{X}^T = \begin{bmatrix} 33 & 0 \\ 0 & 8 \end{bmatrix}$$

$${}^t \tau_{11} = 33, \quad {}^t \tau_{22} = 8, \quad {}^t \tau_{12} = 0$$

Hence the Cauchy stress ${}^t \underline{\tau}$ given by the program is not correct.

We can identify the program error by noting that $\frac{33+8}{2} = 20.5$, $20.5 + 12.5 = 33$ and $20.5 - 12.5 = 8$. Hence a rotation of 45° was wrongly applied. Therefore,

$${}^t \underline{\tau} \Big|_{program} = \underline{R} {}^t \underline{\tau} \Big|_{above} \underline{R}^T \quad \text{where } \underline{R} = \begin{bmatrix} \cos 45^\circ & -\sin 45^\circ \\ \sin 45^\circ & \cos 45^\circ \end{bmatrix}$$

Problem 2 (10 points):

Since $H, h \ll b$, we only consider the displacement u_r in the x_1 -direction with the plane stress assumption.

Total Lagrangian formulation

$${}^t f^B = {}^t \rho {}^t r \omega^2$$

$${}^0 t = H \left(\frac{r-b}{a-b} \right) + h \left(\frac{r-a}{b-a} \right), \quad {}^t t = H \left(\frac{r-{}^t b}{{}^t a-{}^t b} \right) + h \left(\frac{r-{}^t a}{{}^t b-{}^t a} \right) \quad (\text{Thickness})$$

$${}^0 e_{rr} = \frac{\partial u_r}{\partial {}^0 r} + \frac{\partial {}^t u_r}{\partial {}^0 r} \frac{\partial u_r}{\partial {}^0 r}, \quad {}^0 \eta_{rr} = \frac{1}{2} \left(\frac{\partial u_r}{\partial {}^0 r} \right)^2$$

$${}^0 e_{\theta\theta} = \frac{u_r}{r} + \frac{{}^t u_r u_r}{r^2}, \quad {}^0 \eta_{\theta\theta} = \frac{1}{2} \left(\frac{u_r}{r} \right)^2$$

Therefore,

$$\begin{aligned} & \int_a^b {}_0 C_{ijrs} e_{rs} \delta_0 e_{ij}^0 r^0 t dr + \int_a^b {}_0^t S_{ij} \delta_0 \eta_{ij}^0 r^0 t dr \\ &= \int_{t+\Delta t}^{t+\Delta t} \rho^{t+\Delta t} r \omega^{2t+\Delta t} r^{t+\Delta t} t \delta u_r dr - \int_a^b {}_0^t S_{ij} \delta_0 e_{ij}^0 r^0 t dr \end{aligned}$$