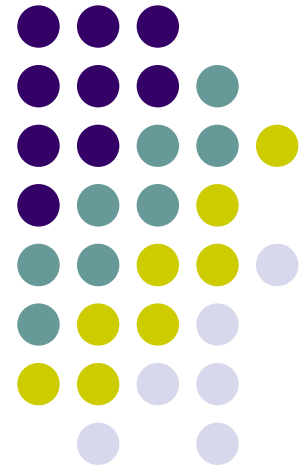
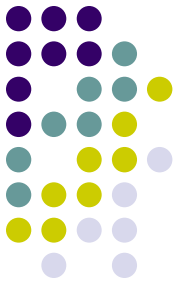


Diffusion Creep

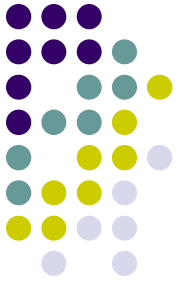
Poirier, Chapter 2 and 7, 1985.
Gordon, 1985.



Fick's First Law: Driving Force



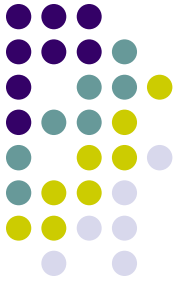
$$J = -D \cdot \nabla \mu \quad \left\{ \begin{array}{l} \nabla c \quad \bullet \text{ Chemical Diffusion} \\ \nabla T \quad \bullet \text{ Thermal diffusion} \\ \nabla V \quad \bullet \text{ Electrical conduction} \\ \sigma \quad \bullet \text{ Diffusion creep} \end{array} \right.$$



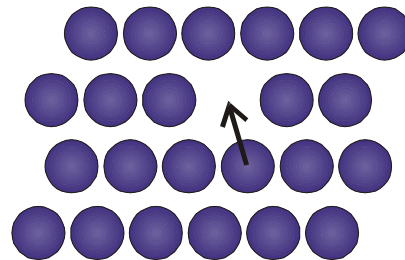
Types of Diffusion

Mechanism	Path	Process
Isotope	Lattice	Interdiffusion
Self-diffusion	Pipe	Creep
Vacancy	Grain Boundary	Ambipolar
Interstitial	Surface	
Ring	Pore fluid	

Diffusion mechanisms

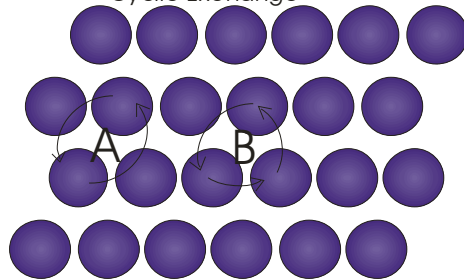


Vacancy Diffusion



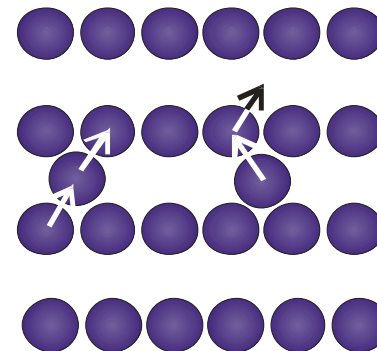
Ring Diffusion

Direct Exchange
Cyclic Exchange



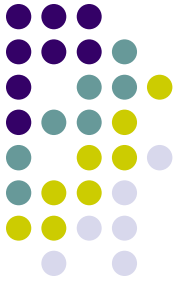
Interstitial

Collinear
Non-collinear



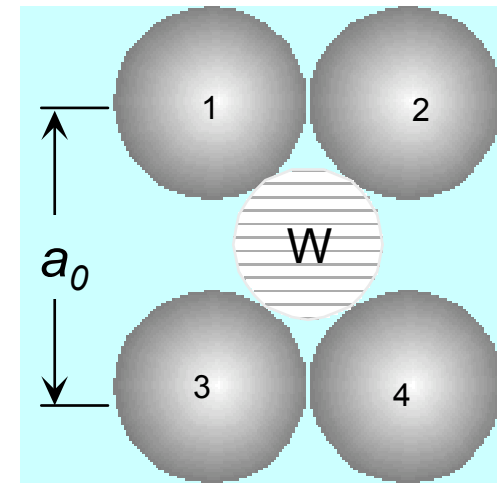
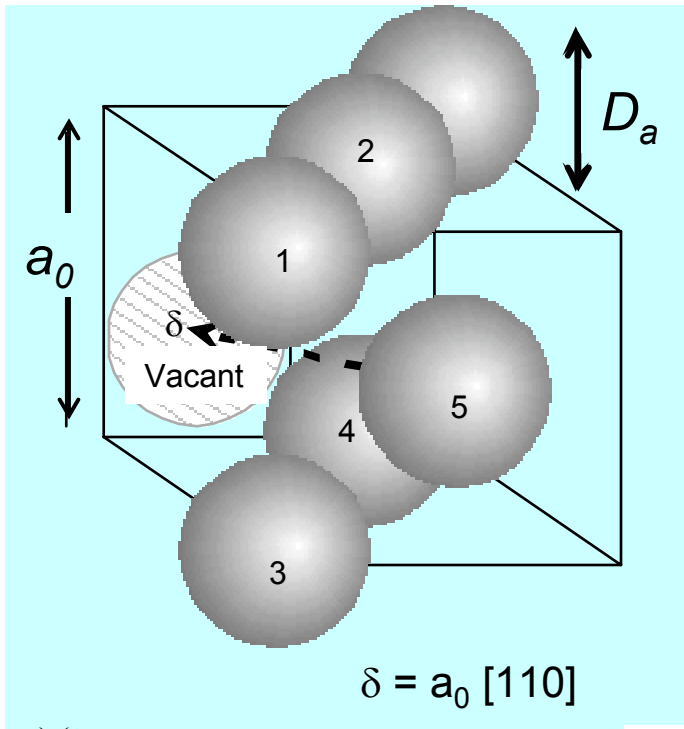
Vacancy-Assisted Diffusion

From Site by Glicksman and Lupulescu, RPI, 2003



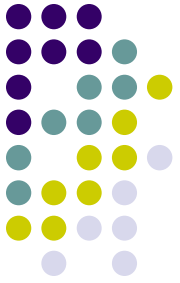
The FCC lattice geometry requires

$$W = (\sqrt{3} - 1)D_a = 0.73D_a$$



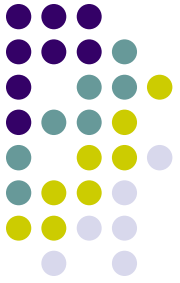
plan view

Kinetics Equation for Vacancy Diffusion

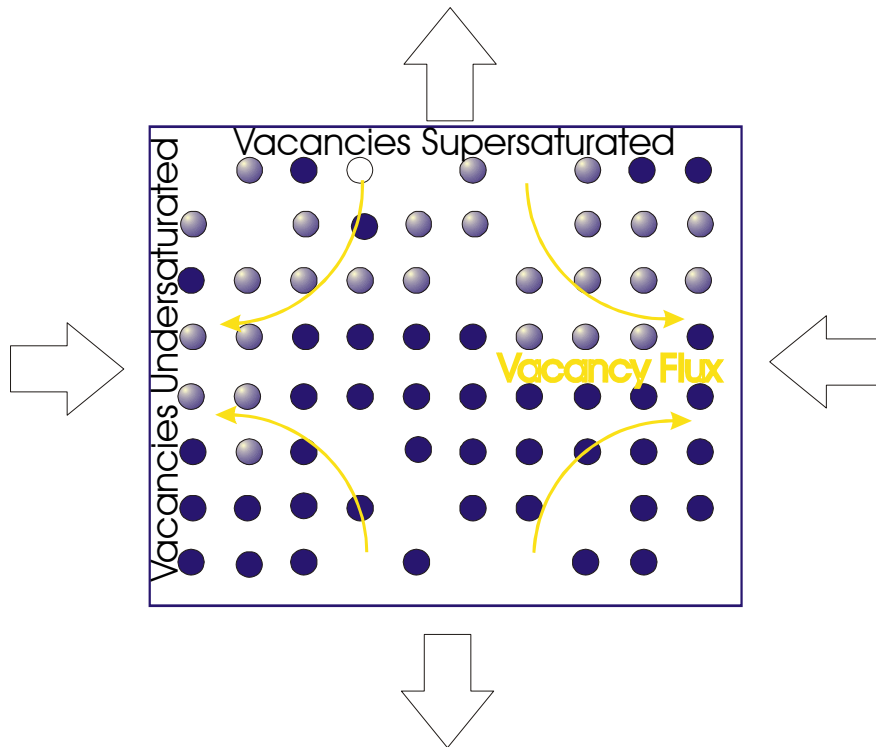


- Coefficient of Diffusivity for Self-diffusion not the same as Coefficient for Vacancy Diffusion

$$\begin{aligned} D_{sd} &= N_v \cdot D_{v \text{ migration}} \\ &= N_{v_o} \exp\left(-\frac{\Delta G_{vf}}{kT}\right) \cdot D_{v_o} \exp\left(-\frac{\Delta G_{vm}}{kT}\right) \\ &= D_{sd_o} \exp\left(-\frac{\Delta G_{vf} + \Delta G_{vm}}{kT}\right) \end{aligned}$$

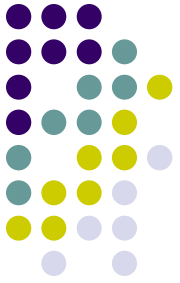


Diffusion Creep in Monatomic Solid



- Basic Ideas

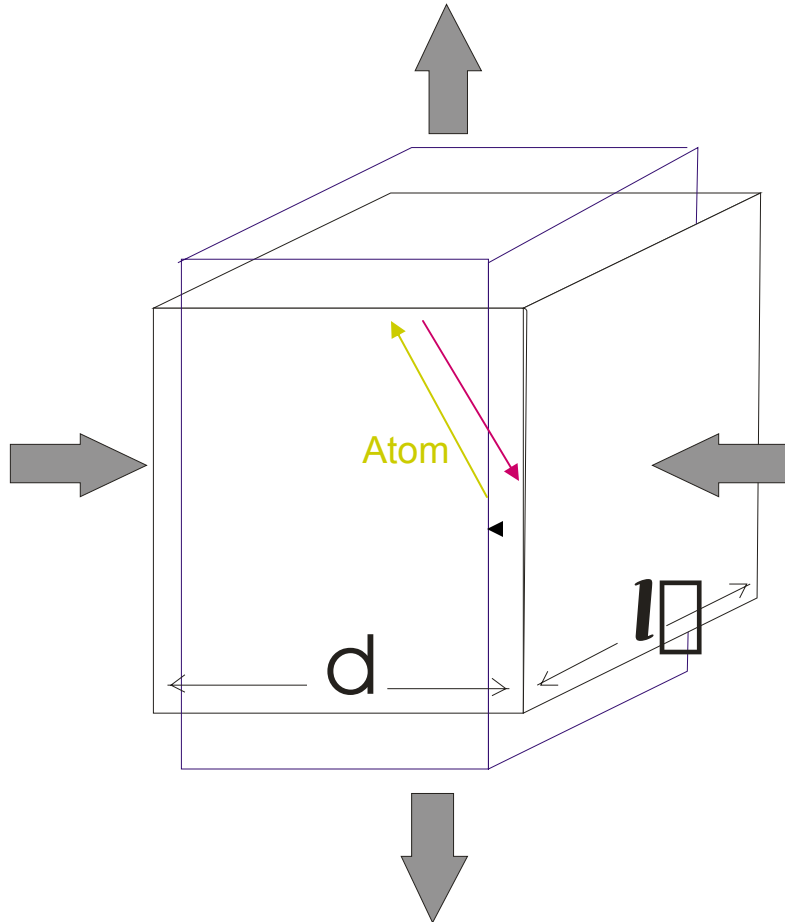
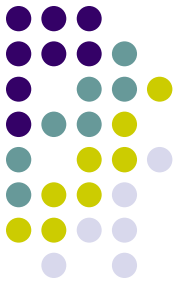
- Supersaturation of vacancies owing to stress
- Diffusion results
- Work done on mat'l by tractions
- Energy dissipated in heat, entropy, and surface area



Diffusion Creep

- Nabarro-Herring Creep
Lattice
- Coble Creep
Grain Boundary
- Monatomic
- Quasi static
- Vacancy
- Increasing length;
Poisoning

Critical Idea: Tension makes vacancy formation easier.

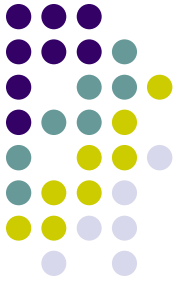


- Tension=supersaturation

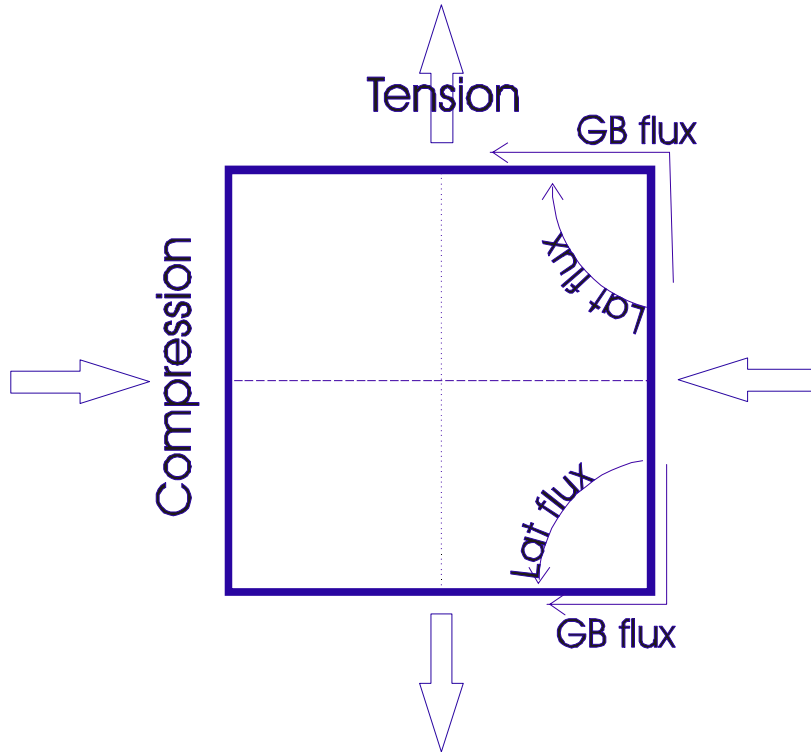
$$\Delta G_{f_{v\Box}}(\sigma) = \Delta G_{f_{v\Box}}(0) - \sigma\Omega$$

$$C_{v0\Box} = C \cdot \exp\left(-\frac{\Delta G_{f_{v\Box}}(0)}{kT\Box}\right)$$

$$C_{v\Box}(\sigma) = C \exp\left[-\frac{\Delta G_{f_{v\Box}}(0) - \sigma\Omega}{kT\Box}\right]$$



Gradient in Composition



- Path Length:
 - Boundary: $2xd/4$
 - Lattice: $(\pi/2)x(d/4)$
- Concentration Difference

$$C_o \exp\left(-\frac{\Delta G_{fv} - \sigma\Omega}{kT}\right)$$

$$-C_o \exp\left(-\frac{\Delta G_{fv} + \sigma\Omega}{kT}\right)$$

$$C_o \exp\left(-\frac{\Delta G_{fv}}{kT}\right) \left(\exp\left(\frac{\sigma\Omega}{kT}\right) - \exp\left(-\frac{\sigma\Omega}{kT}\right) \right)$$

$$\Delta C = 2C_o \exp\left(-\frac{\Delta G_{fv}}{kT}\right) \cdot \frac{\sigma\Omega}{kT}$$

- Quasi-static Approx.

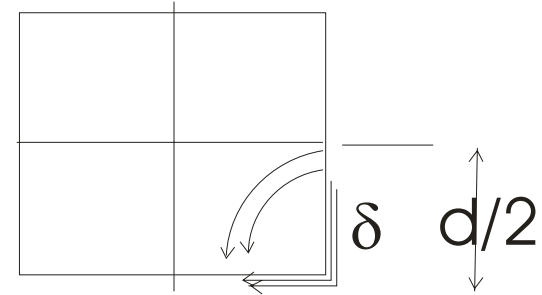
Fick's 1st Law



$$J_{path} = -D_{path} \frac{\Delta C}{\Delta L_{path}} \quad i.)$$

Total flux = Σ Flux on each Path:

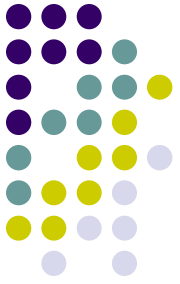
$$\Phi_{vac\ flux} = J_L \cdot \frac{d}{2} \cdot l + J_B \cdot \delta \cdot l$$



$$J_{total} \triangleq total\ ave.\ flux = \frac{\Phi_{vac\ flux}}{d/2 \cdot l} = J_L + \frac{2\delta}{d} J_B \quad ii.)$$

Plugging ΔC and ΔL into i.) and inserting fluxes in ii.):

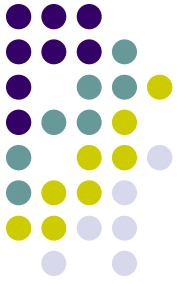
$$J_{total} = -D_L 2C_o \exp\left(-\frac{\Delta G_{fv}}{kT}\right) \cdot \frac{\sigma\Omega}{kT} \frac{1}{\pi d/8} + \frac{2\delta}{d} (-D_b) \frac{2C_o \exp\left(-\frac{\Delta G_{fv}}{kT}\right) \cdot \frac{\sigma\Omega}{kT}}{d/2}$$



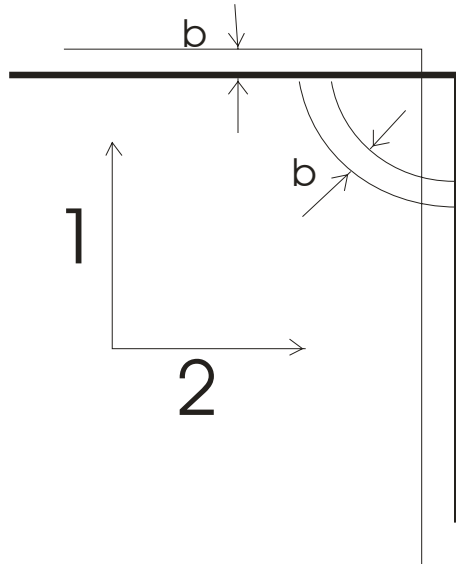
Total Flux on Both Paths



$$\begin{aligned}
 J_{Total} &= \frac{8}{\pi d} D_L C_{vo} \exp\left[-\frac{\Delta G_{vf}}{kt}\right] \left\{ \frac{\sigma \Omega}{kT} \right\} + \frac{2\delta}{d} \frac{2D_B C_{vo}}{d} \left(\exp\left[-\frac{\Delta G_{vf}}{kt}\right] \right)^2 \left\{ \frac{\sigma \Omega}{kT} \right\} \\
 &= \frac{16}{\pi d} \left[D_L C_{vo} \exp\left[-\frac{\Delta G_{vf}}{kt}\right] \right] \left\{ \frac{\sigma \Omega}{kT} \right\} \left\{ 1 + \frac{\pi \delta D_B}{2d D_L} \right\}
 \end{aligned}$$

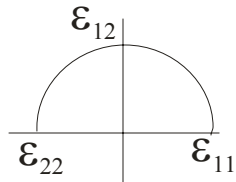


Converting flux to strain

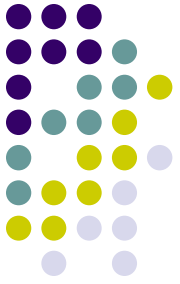


- Each vacancy that travels through the channel adds layer of depth b

$$\frac{\Delta l}{l \cdot t} = \frac{\# \text{ vacs } b}{s d} = 2 \cdot J_{\text{total}} \cdot b^2 \cdot \frac{b}{d} = \frac{2 J_{\text{total}} \Omega}{d}$$



- $$\dot{\epsilon} = \frac{32}{\pi d^2} \frac{\sigma \Omega}{kT} D_{L\Box} \left(1 + \frac{\pi \delta D_{B\Box}}{2d D_{V\Box}} \right)$$



Summary: N-H and Coble Creep

- Diffusion Creep Constitutive Law:

$$\dot{\epsilon} = \frac{32}{\pi d^2} \frac{\sigma \Omega}{kT} D_{L\Box} \left(1 + \frac{\pi \delta}{2d} \frac{D_{B\Box}}{D_{V\Box}} \right)$$

- $D_{L\Box} = D_{VM} C_{V\Box}$
- Strain rate linear in stress
- $\dot{\epsilon} \propto \frac{1}{d^{2,3}}$
- Other geometries change initial constant