

1. From Lecture A, pg 4, solubility of mixture is:

$$C_w = X_t C_w^o$$

where  $C_w$  = solubility of compound in contact with mixture  
 $C_w^o$  = solubility in contact with pure product  
 $X_t$  = mole fraction of compound in mixture

Calculation of mole fraction - assume 1 Kg of mixture

	M.W.	mass	moles	mole fraction
TCE	131.5	.4	3.04	0.40
TCA	133.4	.6	4.50	0.60
total		1	7.54	
	gm/mole	Kg	mol	

Calculation of  $C_w$

	$C_w^o$	$X_t$	$C_w$
TCE	1100	0.4	440 mg/L
TCA	1500	0.6	900 mg/L

2. Problem statement indicates generally north to south flow. This plus elevations used to draw map (attached)

$$i = \frac{\Delta h}{\Delta L} = \frac{97.7 - 86.7}{2000 \text{ m}} \quad (\text{MW-2 to lake})$$

$$= 0.0055$$

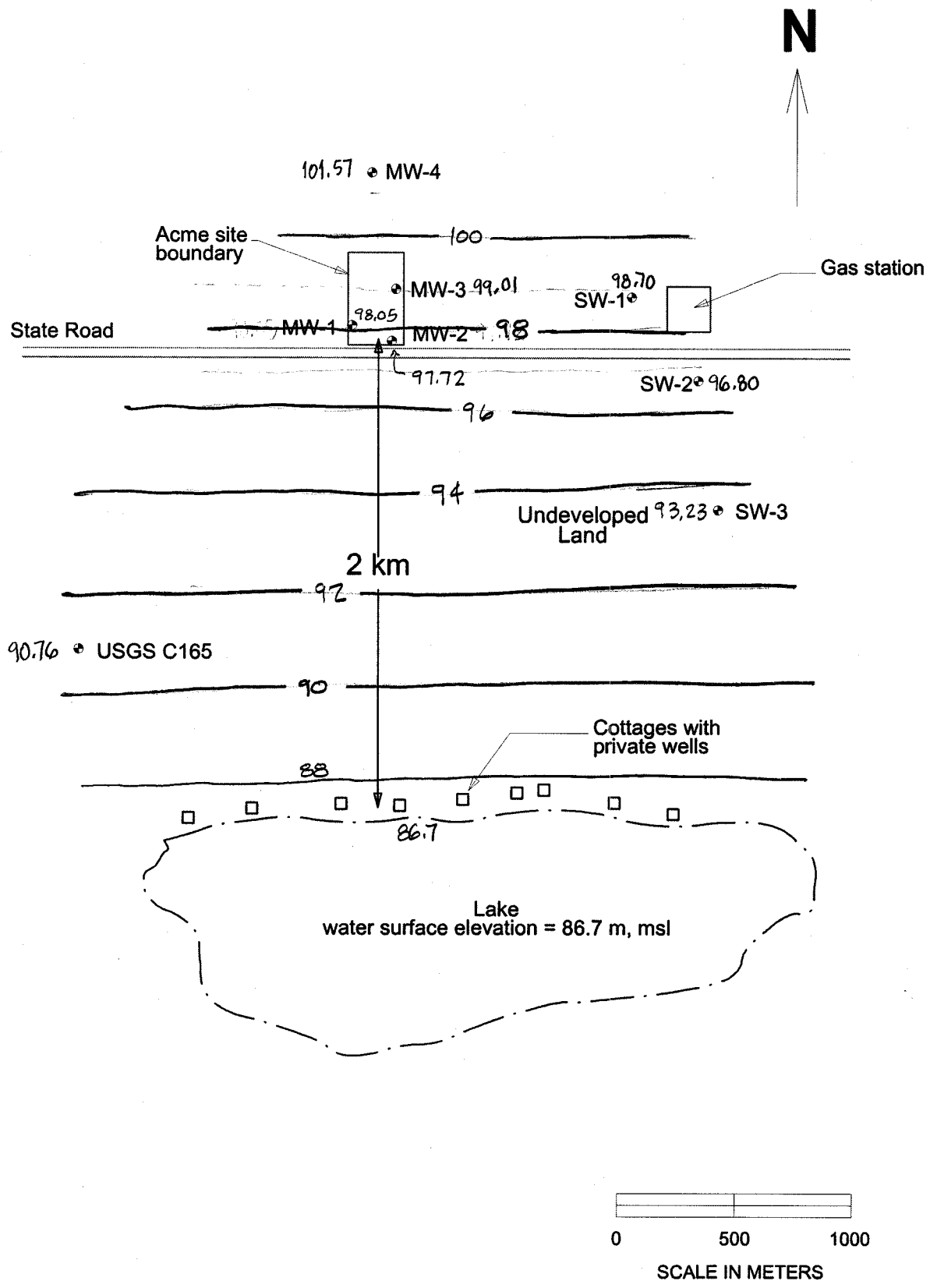


Figure 1  
Acme site vicinity map

3. From Lecture 8 =  $W = \frac{Q_w}{T_i}$

$$T = KB$$

$$K = 1.6 \times 10^{-2} \text{ cm/s} = 14 \text{ m/d}$$

(average of slug tests)

B = aquifer thickness  
= 3 meters

(based on 2 meters to  
water table (top of aquifer)  
and 5 meters to clay  
(bottom of aquifer))

$$T = 14 \frac{\text{m}}{\text{d}} \cdot 3 \text{ m} = 42 \frac{\text{m}^2}{\text{d}}$$

Desired  $W = 200 \text{ m}$  (width of site)

$$200 \text{ m} = \frac{Q_w}{42 \frac{\text{m}^2}{\text{d}} \cdot 0.0055}$$

$$\rightarrow Q_w = 46 \text{ m}^3/\text{d}$$

4. See spreadsheet solution for capture zone

$$X_s = \frac{Q_w}{2\pi T_i} = 31 \text{ m}$$

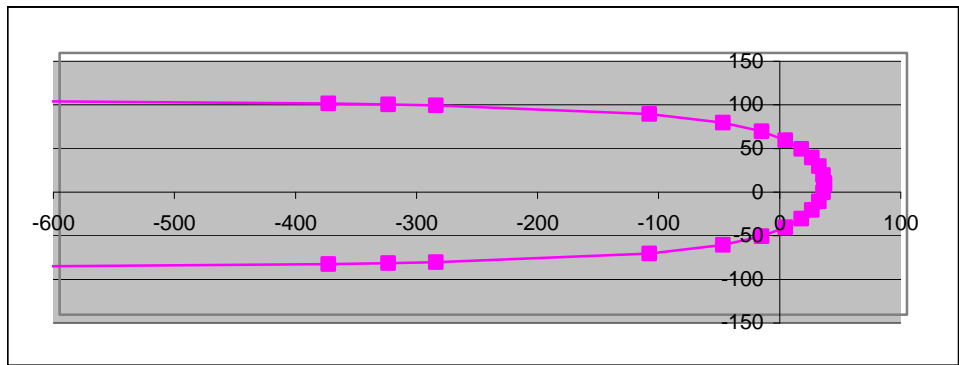
Solve for x given y

$$x = y / \tan (2*\pi*T*i*y/Q_w)$$

Hydraulic gradient, i      0.0055  
 Transmissivity, T          42 m<sup>2</sup>/d  
 Pumping rate, Q<sub>w</sub>          46 m<sup>3</sup>/d

Stagnation point, x<sub>s</sub>      31.69319

x	y
-5532.17	-99
-1980.35	-98
-654.679	-95
-377.973	-92
-328.406	-91
-289.034	-90
-112.68	-80
-51.8878	-70
-20.0403	-60
-0.34148	-50
12.7556	-40
21.60901	-30
27.37009	-20
30.63439	-10
31.68267	-1
31.69319	-0.001
31.69319	0.001
31.68267	1
30.63439	10
27.37009	20
21.60901	30
12.7556	40
-0.34148	50
-20.0403	60
-51.8878	70
-112.68	80
-289.034	90
-328.406	91
-377.973	92
-654.679	95
-1980.35	98
-5532.17	99



$$5. \quad \frac{s}{Q} = \frac{1500}{T}$$

$$T = 42 \frac{\text{m}^2}{\text{d}} = 452 \frac{\text{ft}^2}{\text{d}} \times 7.5 \frac{\text{gal}}{\text{ft}^3} = 3,400 \frac{\text{gpd}}{\text{ft}}$$

$$Q = 46 \frac{\text{m}^3}{\text{d}} = 1600 \frac{\text{ft}^3}{\text{d}} = 12,100 \frac{\text{gal}}{\text{d}} = 8.4 \text{ gpm}$$

$$s = \frac{1500 Q}{T} = 3.7 \text{ ft} = 1.1 \text{ m}$$

3 meters are available for drawdown so one well should be OK. It is a bit marginal and field tests will be needed to confirm the rough estimate.

6. Don't drill through DNAPL!

If you must, double-case wells and be extraordinarily careful