## 10.569 Synthesis of Polymers Prof. Paula Hammond Lecture 3: Step Growth Polymerization, Types of Monomers, Kinetics and Equilibrium Considerations, Closed vs. Open Systems

## Kinetics of Step Growth Polymerization (Chapter 2)

 $A + B \rightarrow polymer + byproduct$ 

$$Rp = \text{rate of polymerization}$$
$$Rp = \frac{-d[M]}{dt} = \frac{-d[a]}{dt} = \frac{-d[b]}{dt} = k[a][b]$$

Assume r = 1, where r is the stoichiometric ratio.  $r = \frac{a}{b}$ 

$$[a] = [b]$$

Terminology  $\overline{p_n}$  varies with  $t \to \overline{p_n} = \frac{[a]_p}{[a]}$ 

$$(X_{n}) \text{ p. 50}$$

$$\frac{-d[a]}{dt} = k[a]^{2}$$

$$\frac{-d[a]}{[a]^{2}} = kt$$

$$\frac{1}{[a]} - \frac{1}{[a]_{o}} = kt$$

$$\frac{[a]_{o}}{[a]} - 1 = [a]_{o} kt$$

$$\pi = 1 - \frac{[a]}{[a]_{o}}$$
in book,  $\pi = p$  (p. 46)
$$\frac{[a]_{o}}{[a]} = \frac{1}{1 - \pi}$$

$$\begin{bmatrix} a_o \end{bmatrix} kt = \frac{1}{1-\pi} - 1 = \overline{p_n} - 1$$
Notes:

- 1.  $[M] \propto \frac{1}{t}$  as time  $\uparrow$ , concentration of monomer  $\downarrow$
- 2.  $\overline{p_n}$  increases linearly with time

$a + b \xrightarrow{k_f} c + d$	$k_f >> k_r$
	LeChatlier's Principle: remove water
	To drive reaction forward

Making esters:

$$\sim$$
 COOH +  $\sim$  OH  $\stackrel{K_{eq}}{\longleftrightarrow} \sim \stackrel{O}{C} = 0 \sim + H_2O$ 

Ester can hydrolyze with water and go backwards (reverse rxn)  $\rightarrow$  drug delivery

$$K_{eq} = \frac{\begin{bmatrix} COO \end{bmatrix} \begin{bmatrix} H_2O \end{bmatrix}}{\begin{bmatrix} COOH \end{bmatrix} \begin{bmatrix} OH \end{bmatrix}}$$

Assume at t = 0:  $\left[ M \right] = \left[ M \right]$ 

Put in terms of  $\pi$ :

$$\begin{aligned} & = \begin{bmatrix} COO \end{bmatrix} &= \pi \begin{bmatrix} COOH \end{bmatrix}_o = \pi \begin{bmatrix} OH \end{bmatrix}_o = \pi \begin{bmatrix} M \end{bmatrix}_o \\ & [OH] = & & \\ & \begin{bmatrix} OH \end{bmatrix} = \begin{bmatrix} M \end{bmatrix}_o - \pi \begin{bmatrix} M \end{bmatrix}_o = \begin{bmatrix} M \end{bmatrix}_o (1 - \pi) \\ & K = \frac{\left(\pi \begin{bmatrix} M \end{bmatrix}_o\right)^2}{\left[M \end{bmatrix}_o^2 (1 - \pi)^2} \\ & K = \frac{\pi^2}{\left(1 - \pi\right)^2} \\ & \pi = \frac{\pi^2}{\left(1 - \pi\right)^2} \\ & \Pi \text{ closed system, limit} \end{aligned}$$

In closed system, limited by K (reaction constant).

That also means rxn and polymer limited by K.

$$\overline{p_n} = \frac{1}{1-\pi} = 1 + K^{\frac{1}{2}}$$

where  $\overline{p_n}$  is the # average degree of polymerization (# of units in polymer)

Polyesterification:	$\frac{\text{K: }1 \sim 10}{p_n} \sim 2 - 5 \text{ monomers}$
Polyamidation:	K: 100 – 1000 $\overline{\rho_n}$ : 10 - 40

In between: removing some of the water

## **Open Driven System**

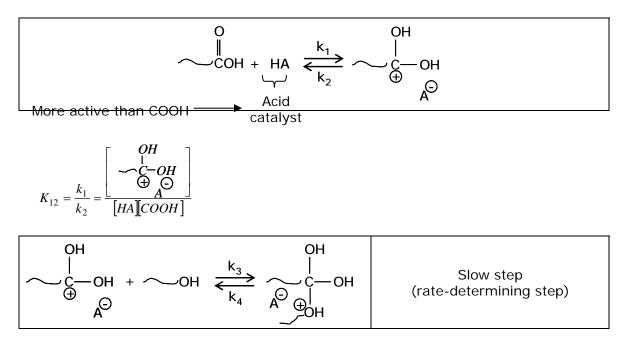
Removing byproduct

- H<sub>2</sub>O by temperature, low pressure, or N<sub>2</sub> blowing of water
- Acid like HCI, base neutralization
- $[H_2O] \leftrightarrow MW(\overline{\rho_n})$  How H<sub>2</sub>O affects  $\overline{\rho_n}$

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$$\begin{split} & \bigcap_{n=1}^{O} \bigcap_{COH + \infty} OH \quad \rightleftharpoons \quad \bigcap_{n=1}^{O} \bigcap_{C \to O \to +} H_2O \\ & \mathcal{K} = \overline{\begin{bmatrix} COO \\ 1 \end{bmatrix} \begin{bmatrix} H_2O \\ 0 \end{bmatrix}} = \frac{\pi \begin{bmatrix} H_2O \\ M \end{bmatrix}_0 (1 - \pi)^2}{\begin{bmatrix} M \end{bmatrix}_0 (1 - \pi)^2} \\ & \mathcal{K} = \frac{1}{1 - \pi} \cdot \frac{\pi}{1 - \pi} \cdot \frac{\begin{bmatrix} H_2O \\ M \end{bmatrix}_0}{\begin{bmatrix} M \end{bmatrix}_0} \\ & \overline{p_n} = \frac{1}{1 - \pi} \\ & \frac{\pi}{1 - \pi} = \frac{1}{1 - \pi} - \frac{1 - \pi}{1 - \pi} = \frac{1}{1 - \pi} - 1 = \overline{p_n} - 1 \\ & \mathcal{K} = \overline{p_n} \cdot \left(\overline{p_n} - 1\right) \frac{\begin{bmatrix} H_2O \\ M \end{bmatrix}_0}{\begin{bmatrix} M \end{bmatrix}_0} \\ & \text{only get down to a certain water concentration} \\ & \rightarrow \text{ solve for best } \overline{p_n} \text{ possible} \end{split}$$

## **Polyesterification Using Acid Catalysis**



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Citation: Professor Paula Hammond, 10.569 Synthesis of Polymers Fall 2006 course materials, MIT OpenCourseWare (http://ocw.mit.edu/index.html), Massachusetts Institute of Technology, Date

$$R_p = \frac{-d[COOH]}{dt}$$

Rate of disappearance of carboxylic monomer

$R_p$	$= K_3 \left[ C^+ \left( OH \right)_2 \right] \left[ OH \right]$	(from previous page)
	$= K_3 K_{12} [HA] [COOH] [OH]$	
	From equilibrium expression	[HA] is constant because it's regenerated.

$$R_{p} = \frac{-d[COOH]}{dt} = k[COOH][OH] \quad \text{where } k = k_{3}K_{12}[HA] \text{ constant}$$

Self-catalyzed: [HA] = [COOH]

$$R_{p} = \frac{-d[COOH]}{dt} = k"[COOH]^{2}[OH] \text{ where } k" = k_{3}K_{12}$$

$$R_p = \frac{-d[M]}{dt} = \kappa^{"} [M]^{3}$$
 separate and integrate

$$2k''t = \frac{1}{\left[M\right]^2} - \frac{1}{\left[M\right]^2_o}$$

 $[M] = [M]_o (1 - \pi)$ 

$$\left(\overline{\rho_n}\right)^2 = \frac{1}{\left(1-\pi\right)^2} = 2\left[M\right]_o^2 k't + 1$$

Much slower because of time-dependence ( $\sqrt{t}$ ) That's why people add acid to drive reaction.

High Temperature

- increase k
- remove byproduct (evaporate H<sub>2</sub>O)

Bulk or mass conditions (no solvent)

- [M]<sub>o</sub> is maximum
- no need to separate product

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- viscosity  $\eta$  low until high  $\pi$
- direct processing

Use solvent

- monomers are not miscible with each other but miscible with solvent
- allow high T
- dilute viscous media (carrier for viscous media)
   → improves processing
- improves heat and mass transfer

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