

Bedrock Channels and Tectonic Geomorphology, Cont.

Flow types:

Debris flow, lahar (volcanic), mud flow (few gravel, no boulders)

Flowing mixture of water, clay, silt, sand, gravel, boulder, etc.

Flowing is liquefied with about 15% of water by weight.

Rheology: function of grain size distribution.

Mud flow → non-newtonian fluid

Wet grain flow → friction and collisions with pore pressure

Mud flows:

Visco-plastic (simplification)

$$\tau = \tau_y + \mu \frac{\partial v}{\partial z}$$

$$\frac{\partial v}{\partial z} = \frac{1}{\mu} (\tau - \tau_y)$$

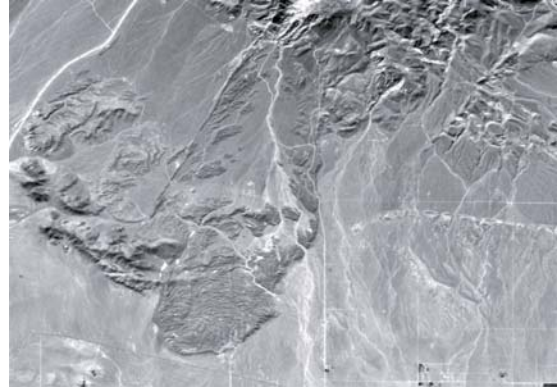
Simplification:

$$\tau_y = \text{constant} \quad (\text{f}(\text{grain size, H}_2\text{O}\%))$$

$$\mu = \text{constant} \quad (\text{f}(\text{grain size, H}_2\text{O}\%))$$

MOVIE SHOW (made by USGS in 1984)

Debris Flow:



Landslides:

Rock avalanches

Rock fall (toppling of blocks)

Shallow soil landslides (tabular)

Deep bedrock landslides (tabular)

Earth flows (slow oozing \Rightarrow reactivations over long time)

Rotation slumps

Slope stability (initiation of failure)

$F \Rightarrow$ factor of safety

$F = 1$, at failure (or critical)

$F > 1$, stable

$F < 1$, unstable

$$F = \frac{\text{strength (resisting force)}}{\text{driving force}} = \frac{s_t}{\tau_{b_{wet}}} = \frac{c + (\sigma_{wet} - p) \tan \phi}{\rho_{b_{wet}} g h S}$$

where ϕ is friction angle.

Infinite slope approximation \Rightarrow no end effects

$s_t = c + \sigma \tan \phi_i$ where ϕ_i is internal friction angle.

$s_t = c' + (\sigma - p) \tan \phi$ where c' is total effective cohesion.

$$F_s = \frac{s_t}{\text{driving stress}} \equiv 1 \text{ at failure}$$

$\tau_b = \rho_b gh \sin \alpha$ where ρ_b is wet soil bulk density.

$\rho_b = v_s \rho_s + m(1 - v_s) \rho_w$ where v_s is volume fraction solids and m is fraction of soil depth saturated.

$$\sigma = \rho_b gh \cos \alpha$$

$$F_s = \frac{c' + (\sigma - p) \tan \phi}{\tau_b} = \frac{c' + (\rho_b gh \cos \alpha - p) \tan \phi}{\rho_b gh \sin \alpha}$$

$$p = \rho_w gmh \cos \alpha$$

$$F_s = \frac{c' + (\rho_b - m\rho_w)gh \cos \alpha \tan \phi}{\rho_b gh \sin \alpha}$$

$$F_s \leq 1 \text{ failure}$$

Cohesionless soil

$$c' = 0 \quad \text{if cohesionless}$$

$$F_s = \frac{(\rho_b - m\rho_w) \tan \phi}{\rho_b \tan \alpha}$$

$$F_s = 1 \text{ at maximum stable slope}$$

$$\tan \alpha_{\max} = \frac{(\rho_b - m\rho_w) \tan \phi}{\rho_b}$$

$$\text{If dry, cohesionless, } \tan \alpha_{\max} = \tan \phi, \quad \alpha_{\max} = \phi$$

Iverson and Major (1986), WRR

Normal force (stress): $(\rho_b - \rho_w)gh \cos \alpha + \text{seepage force}(z)$

Driving stress: $(\rho_b - \rho_w)gh \sin \alpha + \text{seepage force}(x)$

where $\rho_b - \rho_w$ is buoyant weight of wet soil.

If parallel seepage, seepage force in $(z) = 0$

$$f_{seepage} = \frac{q}{K} \rho_w g \text{ where } q \text{ is water flux per unit volume.}$$

Darcy's law: $q = K \sin \alpha$ where K is hydraulic conductivity.

$$f_{seepage} = \rho_w g \sin \alpha$$

seepage force in $(x) = \rho_w g h \sin \alpha$

$$F_s = \frac{(\rho_b - \rho_w) g h \cos \alpha \tan \phi}{\rho_b g h \sin \alpha}$$