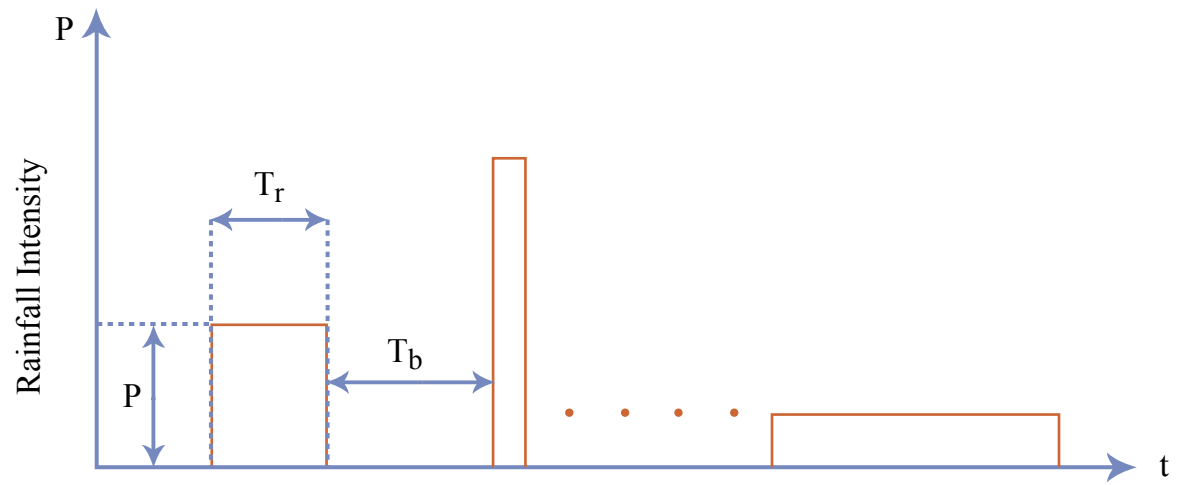


(a) Actual

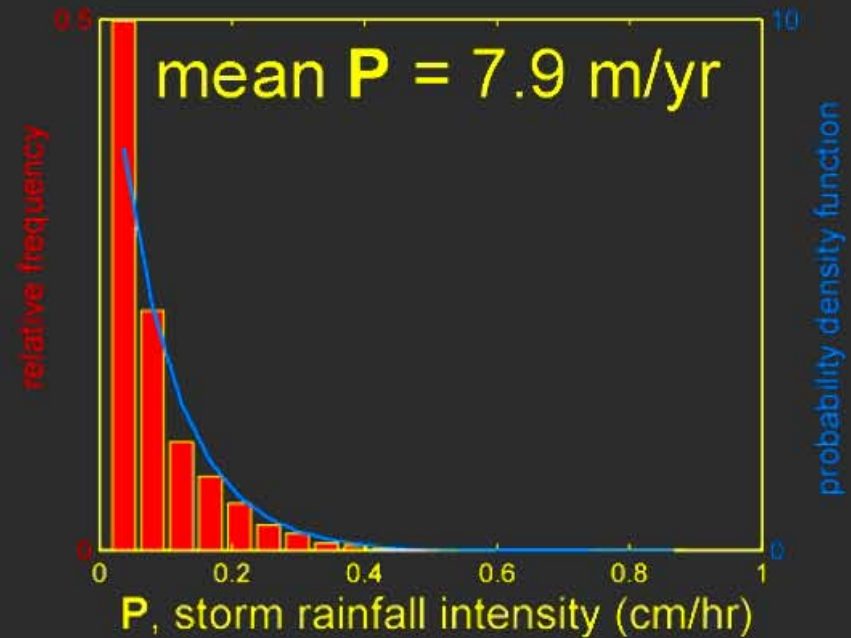
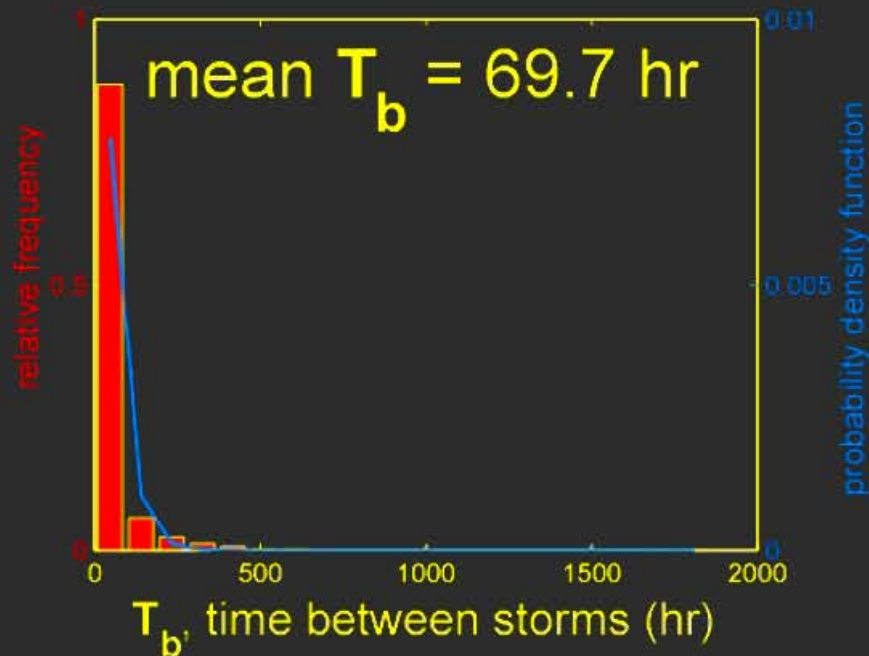
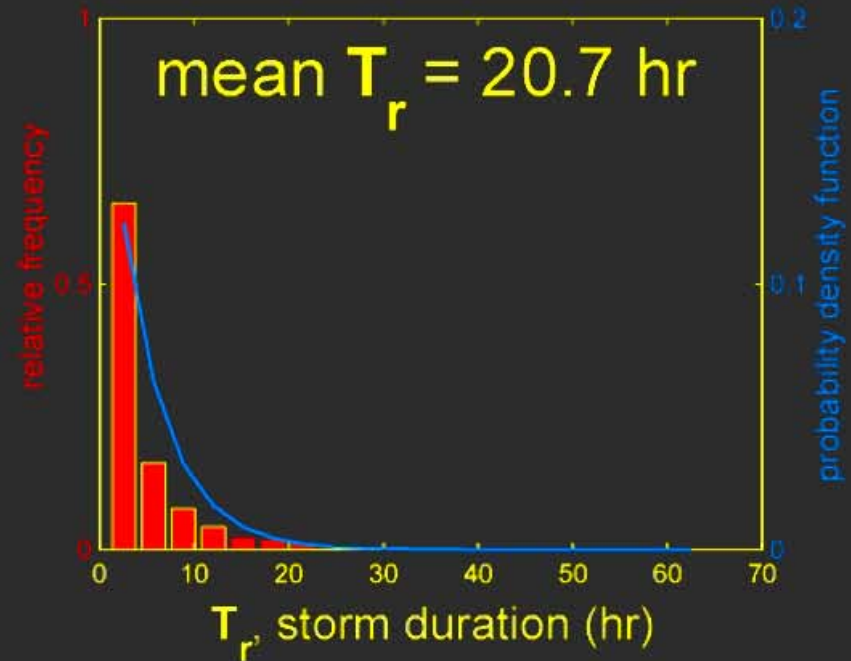


(b) Model

Schematic Illustration of Poisson Rectangular Pulse Rainfall Model

# Poisson pulse rainfall model parameters for Eureka, California (Eagleson, 1978)

hourly precipitation data, 1954-1993  
National Climatic Data Center  
([www.ncdc.gov](http://www.ncdc.gov))



- Tucker & Bras used the Poisson pulse rainfall model of Eagleson (1978).
- Parameterizes climate using exponential distributions of storm duration, interstorm duration, and rainfall intensity.
- These distributions can be derived from hourly precipitation data, a resource readily downloaded for hundreds of stations in the U.S. from the NCDC website.

# Stochastic-threshold incision model

(Tucker & Bras, 2000)

$$E = K_R K_C K_{\tau_c} A^m S^n$$

- $K_R = K_R$  (physical parameters,  $\rho$ ,  $g$ ,  $k_e$ , width, lithology)
- $K_C = K_C$  (climate parameters,  $P$ ,  $T_r$ ,  $T_b$ )
- $K_{\tau_c} = K_{\tau_c}$  ( $R_c/P \propto \tau_c/P$ ,  $A$ ,  $S$ ; varies from 0 to 1)
- Key unknown parameters:  $\tau_c$ ,  $k_e$ , and  $a$  (or  $n$ )
  - From the basic postulate,  $E = k_e (\tau_b^a - \tau_c^a)$

The Tucker & Bras approach can be simplified to this form. Incision rate set by area and slope, and three coefficients.

- $K_R$ , typical parameters
- $K_C$ , the climate parameters from the Eagleson model.
- $K_{\tau_c}$ , A critical runoff set by the  $T_c/P$  and also dependent on  $A$  and  $S$  in a complicated way.

## Bedrock Channel Incision Models

Basic Postulate

$$E = k_r (\tau - \tau_{cr})^a \quad \text{or} \quad E = k_r (\tau^a - \tau_{cr}^a)$$

$$E = K_{eff} A^m S^n$$

$$K_{eff} = K_r K_c \beta_{\tau_{cr}} \quad ; \quad n = \frac{2}{3} a \quad ; \quad m = \frac{2}{3} ac(1-b)$$

### Stream Power Model

$$K_r = k_r k_w^{-2a/3} k_s^a$$

$$K_c = k_c^{2a/3(1-b)}$$

$$\beta_{\tau_{cr}} = 1$$

### Empirical Relations

$$k_r = C_r^{3/2} \rho g^{2/3}$$

$$Q_c = k_q A^s$$

$$w_{Mf} = k_w Q_{Mf}^b$$

$$(w/w_{Mf}) = (Q/Q_{Mf})^s$$

### Stochastic Model (Tucker and Bras)

$$K_r = k_r k_w^{-2a/3} k_s^a$$

$$K_c = \langle P \rangle^{\gamma_b - \varepsilon_b} F_{\gamma_b}^{\gamma_b - 1} \exp(-I/\langle P \rangle F_{\gamma_b}) \Gamma(\gamma_b + 1)$$

$$\beta_{\tau_{cr}} = \frac{\left[ \Gamma(\gamma_b + 1, R_c/P) - (R_c/P)^{\gamma_b} \exp(-R_c/P) \right]}{\Gamma(\gamma_b + 1)}$$

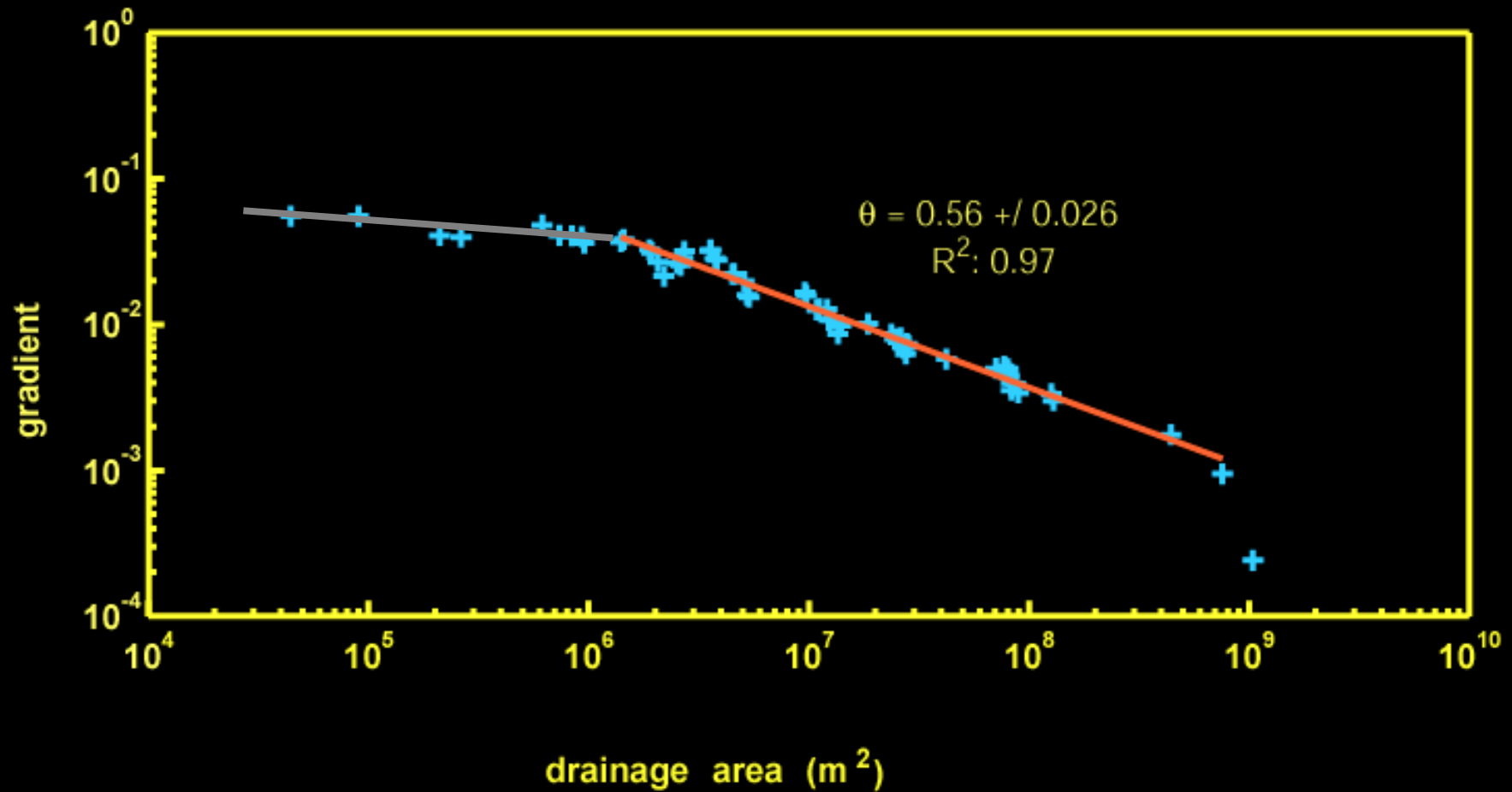
### Exponents (Stochastic Model)

$$c = 1$$

$$\gamma_b = 2a(1-s)/3$$

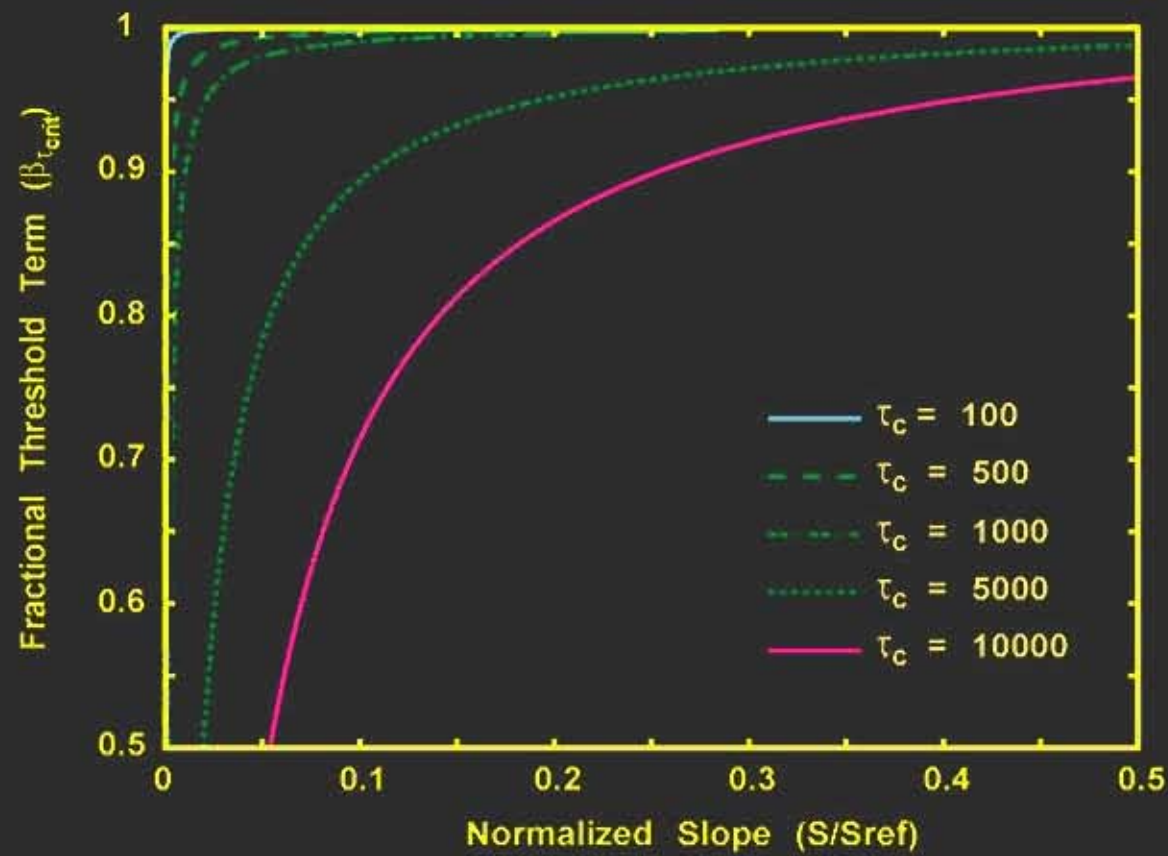
$$\varepsilon_b = 2a(b-s)/3$$

## Mixed Bedrock-Alluvial Stream (Appalachians, VA)

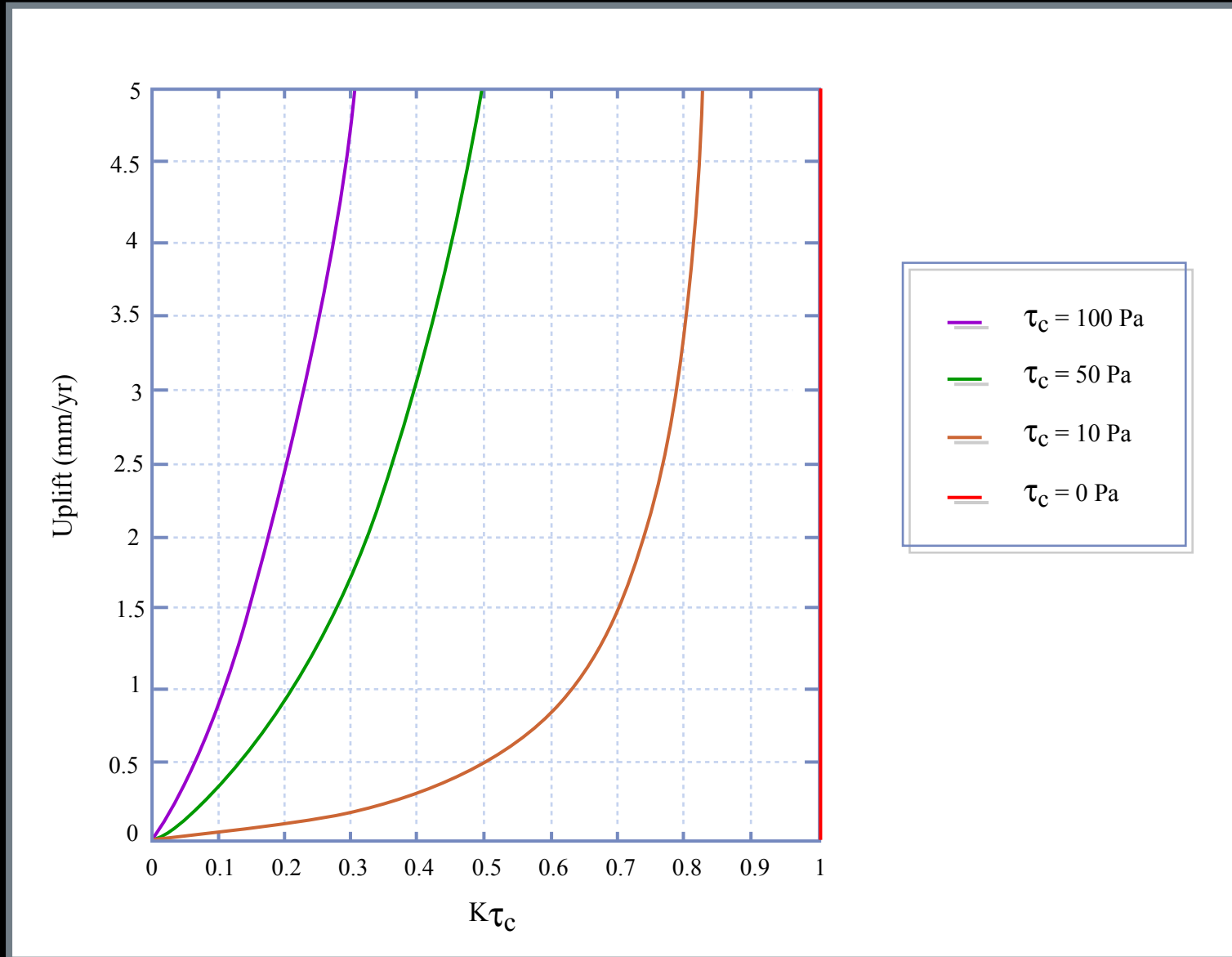


Concavity Index indistinguishable from detachment-limited bedrock channels



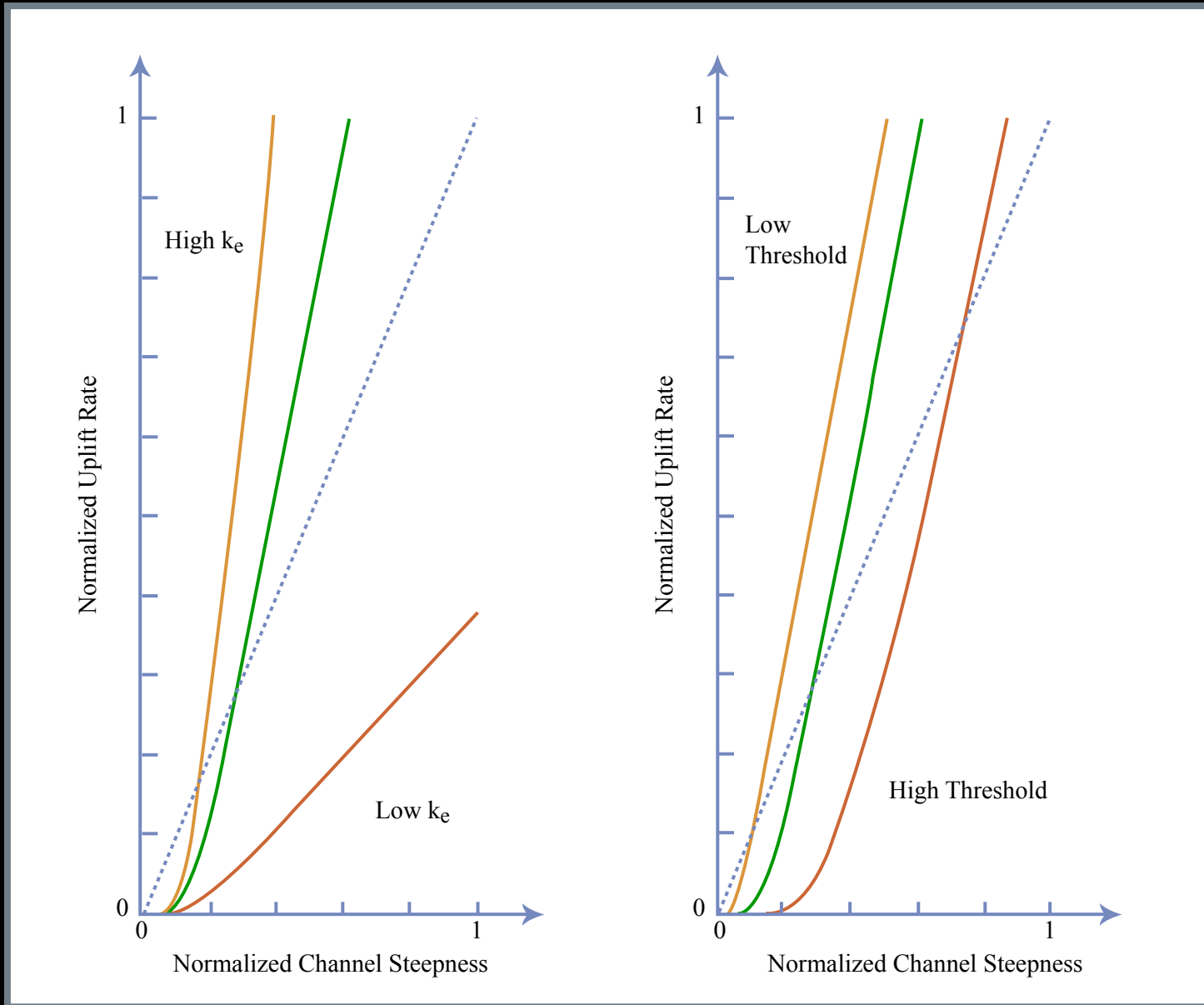


# $K_{\tau_c}$ at steady state



$K\tau_c$  varies between 0 and 1. For the no-threshold case, simply equals 1. For other cases, in steady-state streams it's constant downstream and varies with uplift rate.

# Model effect on relief-uplift rate relation



But, the important point is heuristic. Thresholds fundamentally change the predicted relationship between relief and U.

- $n=1$
- Simple model is dashed line-- linear relation between slope and uplift rate for ss channels.
- Top plot varies  $k_e$ , shear stress-erosion rate coefficient. Low  $k_e$  (hard rocks) stronger relationship btw U and S. High  $k_e$  (weak rocks, fast E), weaker relation at high U. Small changes in S yield large changes in E because more events exceed the threshold.
- Effect of the  $T_c$  is less pronounced. Simply the presence of the  $T_c$  is important. Of course  $T_c$  and  $k_e$  will covary in lithologies.