

# 12.520 Lecture Notes 12

## Elasticity

So far:

Stress  $\rightarrow$  angle of repose vs accretionary wedge

Strain  $\rightarrow$  reaction to stress  $\rightarrow$  but how?

### Constitutive relations

$$\tau_{ij} = \tau_{ij}(\varepsilon_{kl}); \quad \varepsilon_{ij} = \varepsilon_{ij}(\tau_{kl})$$

For example,

Elasticity

Isotropic

Anisotropic

Viscous flow

Isotropic

Anisotropic

Power law creep

Viscoelasticity

Trade offs:

<b>simplicity</b>	$\leftrightarrow$	<b>realism</b>
constant		variable
isotropic		anisotropic
elastic, viscous		viscoelastic
history independent		history dependent

## Tensors

Most physical quantities that are important in continuum mechanics like temperature, force, and stress can be represented by a tensor. Temperature can be specified by stating a single numerical value called a scalar and is called a zeroth-order tensor. A force, however, must be specified by stating both a magnitude and direction. It is an example of a first-order tensor. Specifying a stress is even more complicated and requires stating a magnitude and two directions—the direction of a force vector and the direction of the normal vector to the plane on which the force acts. Stresses are represented by second-order tensors.

Tensors are quantities independent of coordinate system.

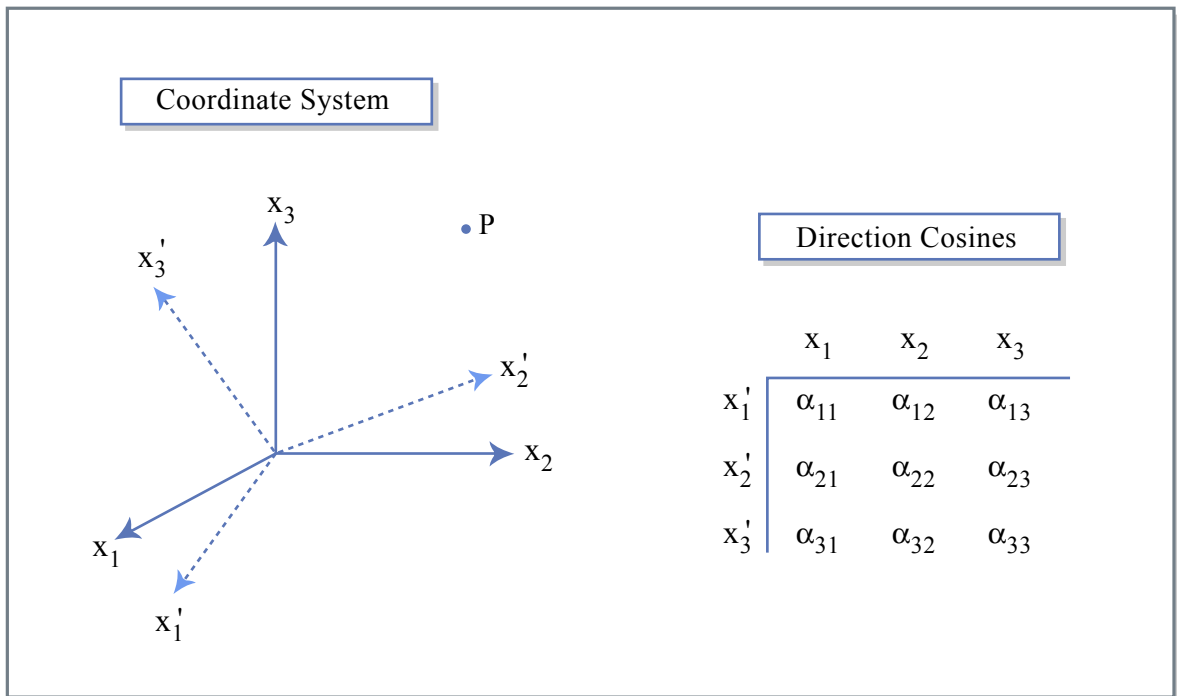


Figure 12.1

Figure by MIT OCW.

$$\alpha_{ij} = \cos \phi_{ij}$$

where  $\phi_{ij}$  is the angle of primed to original.

$$x_i' = \alpha_{ij} x_j$$

$$x_i = \alpha_{ji} x_j'$$

$$\alpha_{ij} = \frac{\partial x_i'}{\partial x_j} = \frac{\partial x_j}{\partial x_i'}$$

Tensors:

- a. 0<sup>th</sup> order (scalar) – quantity dependent only on position
- b. 1<sup>st</sup> order (3<sup>1</sup> components)  $A_i' = \alpha_{ij} A_j$
- c. 2<sup>nd</sup> order (3<sup>2</sup> = 9 components)  $A_{ij}' = \alpha_{is} \alpha_{jk} A_{sk}$
- d. 3<sup>rd</sup> order (3<sup>3</sup> = 27 components)  $A_{ijk}' = \alpha_{is} \alpha_{jt} \alpha_{kp} A_{stp}$
- e. 4<sup>th</sup> order (3<sup>4</sup> = 81 components)  $A_{ijkl}' = \alpha_{is} \alpha_{jt} \alpha_{kp} \alpha_{lq} A_{stpq}$

**Conventional moduli:**

1. Hydrostatic comp.

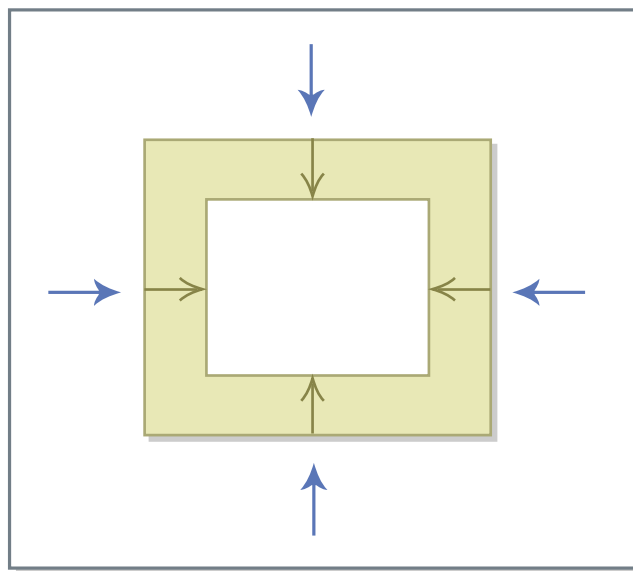


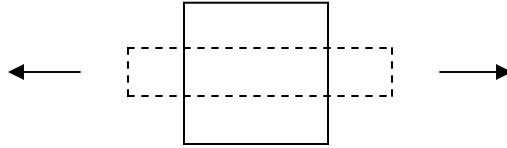
Figure 12.2

Figure by MIT OCW.

$$\begin{aligned}\tau_{ij} &= -p\delta_{ij} \\ \tau_{ii} &= -p\delta_{ii} = 3\lambda e_{kk} + 2\mu e_{ii} \\ &= -3p = (3\lambda + 2\mu)e_{ii} \\ -\frac{p}{e_{ii}} &= -\frac{VP}{\Delta V} \equiv K\end{aligned}$$

where  $K = \lambda + 2/3\mu$  is bulk modulus.

## 2. Uniaxial stress



$$\begin{aligned}\tau_{11} &= T \\ \text{other } \tau_{ij} &= 0 \\ 2\mu e_1 &= T - \frac{\lambda}{2\mu + 3\lambda} T \\ \frac{T}{e_1} &\equiv E \text{ (sometimes } Y\end{aligned}$$

where  $E = \frac{\mu(2\mu + 3\lambda)}{\mu + \lambda}$  is Young's modulus

Hook's law:

$$\begin{aligned}T &= Ee \\ \frac{e_{22}}{e_{11}} &= \frac{e_{33}}{e_{11}} \equiv -\nu \quad \text{This is called Poisson's ratio.} \\ 2\mu e_{22} &= -\frac{\lambda}{2\mu + 3\lambda} \tau_{11} \Rightarrow \nu = \frac{\lambda}{2(\mu + \lambda)}\end{aligned}$$

$$\theta = e_{11} + e_{22} + e_{33} = e_{11}(1 - 2\nu)$$

$$\text{fluid: } \mu \rightarrow 0 \Rightarrow \nu \rightarrow \frac{1}{2}$$

most material:  $\nu = 0.2 - 0.3$

$$\nu = \frac{1}{4} \Rightarrow \lambda = \mu \quad \text{It is Poisson solid.}$$

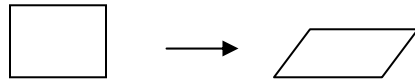
steel:  $\nu$ ; 0.3–0.33

seismically measured

$$v_p = \sqrt{\frac{\lambda + 2\mu}{\rho}} \quad v_s = \sqrt{\frac{\mu}{\rho}}$$

compare  $v_p, v_s \rightarrow \nu \rightarrow$  discriminate rock types

### 3. Simple shear



$$\tau_{12} = \tau_{21} = \tau$$

$$\tau_{12} = 2\mu e_{12} = 2G e_{12}$$

where  $G$  is shear modulus.

Note: Among  $\lambda, \mu, K, \nu, E, G$  only two are independent.