

**Massachusetts Institute of Technology**  
**Department of Aeronautics and**  
**Astronautics**  
**Cambridge, MA 02139**

---

**16.03/16.04 Unified Engineering III, IV**  
**Spring 2004**

**Problem Set 3**

Name: \_\_\_\_\_

Due Date: 2/24/04

	<b>Time Spent (min)</b>
<b>F7</b>	
<b>F8</b>	
<b>F9/F10</b>	
<b>M7/M8</b>	
<b>M9</b>	
<b>Study Time</b>	

---

Announcements:

---

---

F7. The profile drag of a particular wing is assumed to be some given constant over the expected range of operating  $C_L$ 's.

$$c_d \simeq \text{constant}$$

For an elliptically-loaded wing of some aspect ratio  $AR \dots$

a) Determine the operating  $C_L$  at which the lift/drag ratio  $C_L/C_D$  is maximized. This is the desirable operating point for maximum range. Determine how the  $C_D$  at this operating point compares to  $c_d$ .

b) Determine the operating  $C_L$  at which the “power coefficient”  $C_L^{3/2}/C_D$  is maximized. This is the desirable operating point for maximum endurance. Determine how the  $C_D$  at this operating point compares to  $c_d$ .

F8. A wing is to have an elliptic circulation distribution.

$$\Gamma(y) = \Gamma_0 \sqrt{1 - \left(\frac{2y}{b}\right)^2}$$

The planform is to be a straight taper, with root and tip chords defined in terms of the average chord  $c_{\text{avg}}$  and the *taper ratio*  $r = c_t/c_r$ .

$$c_r = c_{\text{avg}} \frac{2}{1+r} \qquad c_t = c_{\text{avg}} \frac{2r}{1+r}$$

a) Define the chord distribution  $c(y)$  in terms of  $c_{\text{avg}}$  and  $r$ . Assuming  $c_{\text{avg}}/b = 0.125$ , draw the planforms for  $r = 0.75, 0.5, 0.25$ .

b) Determine the spanwise  $c_\ell(y)$  distribution, and plot for  $r = 0.75, 0.5, 0.25$ .

Note: Only the shape of the  $c_\ell(y)$  curve is of interest. All scaling constants like  $\Gamma_0$ ,  $c_{\text{avg}}$ , etc. can be set to unity for plotting purposes.

c) Local stall is obviously undesirable. If the airfoil is the same across the span, which taper ratio appears to be most attractive for the purpose of giving the largest stall margin everywhere on the wing?

F9+F10. The circulation distribution on a wing is

$$\Gamma(\theta) = 2bV_\infty (A_1 \sin \theta + A_2 \sin 2\theta)$$

where  $A_1 = 0.05$ , and  $A_2 = 0.01$ .

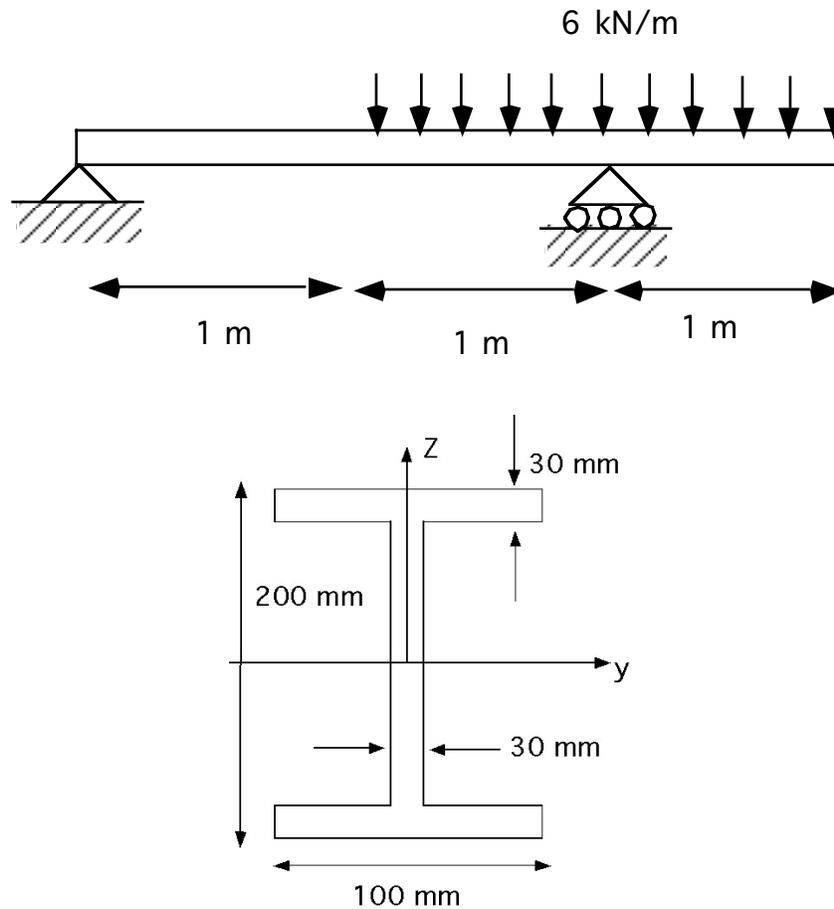
a) Determine and plot  $\alpha_i(y)$ .

b) Determine the rolling moment on the entire wing.

$$M_{\text{roll}} = \int_{-b/2}^{b/2} \rho V_\infty \Gamma y dy$$

**Problem M7 and M8 (this is a two hour question)**

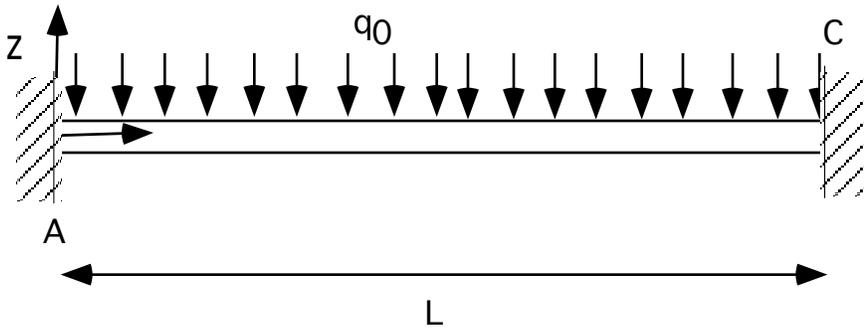
A simply supported aluminum alloy beam is 3 m long and has a cross-section which is an "I" cross-section 200 mm high and 100 mm wide. A uniform distributed load of 6 kN/m acts on the left hand two thirds of the beam. The Young's modulus of the aluminum alloy is 70 GPa. The yield stress is 300 MPa.



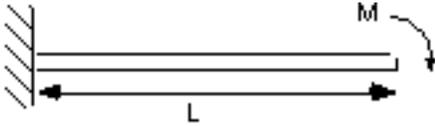
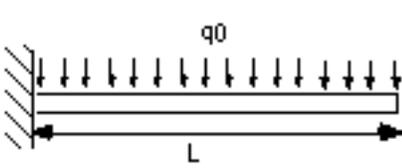
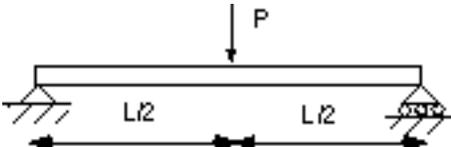
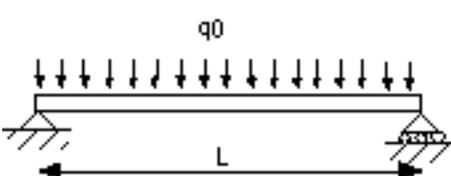
- Determine the loading, shear force and bending moment as functions of the distance  $x$  measured from the left end of the beam. Draw the appropriate diagrams.
- Determine the maximum deflection(s) of the beam and its (their) location(s).
- Determine the magnitudes and locations of the maximum axial stress,  $\sigma_{xx}$  and the maximum shear stress,  $\tau_{xz}$ . Will the aluminum alloy yield?

### Problem M9

A beam of length  $L$  and flexural rigidity  $EI$  is clamped at each end. The beam has a continuous load of magnitude  $q_0$  applied along the beam. Using the “standard solutions” below, or by other means, solve for the reactions at A and C.



### Standard solutions for deflections of beams under commonly encountered loading

Configuration	End slope $dw/dx (x=L)$	End deflection, $w(L)$	Central deflection, $w(L/2)$
	$\frac{ML}{EI}$	$\frac{ML^2}{2EI}$	
	$\frac{PL^2}{2EI}$	$\frac{PL^3}{3EI}$	
	$\frac{q_0L^3}{6EI}$	$\frac{q_0L^4}{8EI}$	
	$\frac{PL^2}{16EI}$		$\frac{PL^3}{48EI}$
	$\frac{q_0L^3}{24EI}$		$\frac{q_0L^4}{384EI}$