## 16.06 Principles of Automatic Control Lecture 34

Zeros:  $z = -0.9867.. \rightarrow W = -30,000$   $z = \infty \rightarrow W = +200$ Poles:  $z = 0.9802 \rightarrow W = -2$ 

Bode Gain:  $G_d(1) = 25$ .

Also, need to map crossover frequency:

$$\nu_c = \frac{\tan(\omega_c T/2)}{T/2} = 51.068$$

There's not much warping at  $\omega T = 0.5$  (2%). At  $\omega T = 1.0$ , there is 9% warping; at  $\omega T = 1.5$ , 24%. So for most problems, may not need to prewarp.

Bode plot of G:



To meet specs, need lead around  $\nu_c = 51$ , lag below  $\nu = 5.1$ .

$$\angle G(j51) = -189.7^{\circ}$$

So need phase from lead compensator

$$\phi_{\text{lead}} = -180^{\circ} - \angle G(j51) + 6^{\circ} + \text{PM}$$
  
= 65.7°

where  $6^{\circ}$  anticipates lag compensation.

$$\Rightarrow \sqrt{\frac{b}{a}} = 4.65$$
$$\Rightarrow b = 51 \cdot 4.65 = 237$$
$$a = 51/4.65 = 11.0$$
$$\Rightarrow K_{\text{lead}} = 5.44 \frac{1 + W/11}{1 + W/237}$$

For this compensator,  $K_p = 136$ . So need lag ratio of 36.76.

$$\Rightarrow K_{\text{lag}} = \frac{W+5}{W+0.136}$$

Therefore, the compensator is

$$K(W) = 5.44 \frac{W+5}{W+0.136} \frac{1+W/11}{1+W/237}$$

The discrete time compensator is the Tustin transform, yielding

$$K_d(z) = 57.97 \ \frac{(z - 0.9512)(z - 0.8957)}{(z - 0.9986)(z + 0.0847)}$$

Remarks:

- 1. Compensator is almost identical to what would be found if we used emulation, if we include effective T/2 delay of ZOH.
- 2. W-Transform approach guarantees stability of discrete-time system. Not really an issue for  $\omega_c T = 0.5$ , but might be for faster crossover.
- 3. Note RHP zero at  $wW = +\frac{2}{T} = 200$ . This zero limits achievable bandwidth of controller, just like time delay.

#### Example

Same plant as above. Make  $\omega_c$  ( $\nu_c$ ) as high as practical and still have 50° phase margin. Solution: Let's pick crossover frequency  $\nu_c$  to be factor of only 2 below NMP zero.

 $\nu_{c} = 100$ 

Use lead compensator to get desired PM and crossover:

$$\angle G_w(j\omega_0) = -204.1^{\circ}$$

$$\phi_{\text{lead}} = -180 - \angle G + \text{PM} = 74.1^{\circ}$$

$$\Rightarrow \sqrt{\frac{b}{a}} = 7.15$$

$$b = 100 \cdot 7.15 = 715$$

$$a = 100/7.15 = 14$$

$$\Rightarrow K_N(W) = 12.53 \frac{1 + W/14}{1 + W/715}$$

$$\Rightarrow K_d(z) = 149.7 \frac{z - 0.8692}{z + 0.5628}$$

See step response below:



# Direct Design

Suppose we have the usual unity feedback control structure:



(The system might be continuous or discrete). Suppose we want the closed loop transfer function

$$H = \frac{KG}{1 + KG}$$

to have a specific form, e.g., have a particular rise time, settling time, etc. Why not just solve for desired K in terms of G, H?

$$H(1 + KG) = KG$$
$$H = -KGH + KG$$
$$K = \frac{1}{G} \frac{H}{1 - H}$$

 $\operatorname{So}$ 

$$K = \frac{1}{G} \frac{H}{1-H}$$

Note that K essentially cancels G with the factor 1/G, so makes the loop gain

$$K = \frac{H}{1 - H}$$

exactly what is needed to have the desired closed loop transfer function. But we can't choose any H desired!

#### Constraints on H:

**Stability** In order that K not cancel on unstable pole or NMP zero, we must have that

1. H must have as zeros all the zeros of G outside the unit circle.

2. 1 - H must have as zeros all the unstable poles of G.

**Causality** In order that K be causal, we must have:

3. The relative degree of H is at least as large as the relative degree of G.

### Example

$$G(s) = \frac{25}{(1+s/2)^2}$$
  

$$G_d(z) = 0.004934 \frac{z+0.9867}{(z-0.9802)^2}$$
  

$$T = 0.01$$

do a direct design such that

- 1. The system is Type 1:  $\Rightarrow$  H(1) = 1.
- 2. The system is deadbeat (all poles of H at z = 0).

Therefore, might select

$$H(z) = \frac{1}{2} \frac{z+1}{z^2}$$

Then

$$K_d(z) = \frac{1}{G_d(z)} \cdot \frac{1}{2} \cdot \frac{z+1}{z^2 - 0.5z - 0.5z}$$

See responses on next two pages. Note the "ringing" in u[k]. To eliminate, put zero of H at -0.9867.





To eliminate ringing, choose





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