# 16.06 Principles of Automatic Control Lecture 21

## The Nyquist Stability Criterion

Can apply the argument principle to finding the stability of the closed loop system



The closed loop transfer function is

$$T(s) = \frac{Y(s)}{R} = \frac{kG(s)}{1 + kG(s)}$$

The closed loop poles of T(s) are the roots of

0 = 1 + kG(s)

That is, the closed loop poles of T(s) are zeros of 0 = 1 + kG(s). Note that the poles of 1 + kG(s) are just the open loop poles of G(s). This suggests the following test for stability of the closed loop system:

#### Stability Test, Version1:

Define the contour  $C_1$  as shown below:



The contour encloses (in the limit) the entire right half plane. For this contour, plot the contour map

1 + kG(s)

The number of CW encirclements of the origin by  $1 + kG(C_1)$  is equal to Z - P, where Z is the number of closed loop poles in the right half plane, and P is the number of open loop poles in the right half plane. As an equation

$$Z = N + P$$

where Z - the number of closed loop unstable poles, N - the number of CW encirclements of 0, P - the number of unstable poles

#### Stability Test, Version 2:

Since the "1" term in 1 + kG(s) just shifts the contour map of kG(s) by one unit to the right, it is often (usually) easier to plot kG(s) alone. This is known as the *polar plot* or *Nyquist* plot for the system. Note that for each encirclement of 0 by 1 + kG(s), there is one encirclement of -1 by kG(s). So the Nyquist Criterion, in the usual form, is

1. Plot kG(s) for  $-j\infty \leq s \leq j\infty$ . First evaluate  $kG(j\omega)$  for  $\omega \in [0,\infty]$  and plot. Then reflect the image about the real axis and add to the previous image. Note that there no need to calculate kG(s) on the circular part of  $C_1$  if  $kG(s) \to 0$  as  $s \to \infty$ .

- 2. Evaluate the number of CW encirclements about -1, and call that number N (see FPE for how to count encirclements).
- **3.** Determine the number of unstable poles of G(s), P.
- 4. The number of unstable poles of the closed loop system is

$$Z = N + P$$

Finally, if k is unknown, we can instead plot G(s), and count encirclements of the point -1/k. This is useful for determining the range of gains for which the closed loop system is stable, as in root locus.

#### Examples



Root locus:



Bode plot:



Nyquist plot:



Note that the Nyquist plot does not encircle -1, and therefore the number of unstable closed loop poles is

$$Z = N + P$$
  
= 0 + 0 (no unstable open loop poles)  
= 0, for  $k = 1$ .

However, we can conclude more than that. The number of encirclements of -1/k is zero for

$$\begin{aligned} & -\frac{1}{k} < 0 \quad \text{or} & & -\frac{1}{k} > 1 \\ & \Rightarrow \frac{1}{k} > 0 \quad \text{or} & & \frac{1}{k} < -1 \\ & \Rightarrow 0 < k < \infty \quad \text{or} & & 0 > k > -1 \end{aligned}$$

Therefore, the system is stable for k > -1. For k < -1, N = 1, so there is one unstable pole.

### Example:



#### The Nyquist plot is:



For -1/k < -1/8 (0 < k < 8), system is stable. For -1/k > 1 (0 > k > -1), system is stable. For -1/8 < -1/k < 0, (k > 8), system has 2 unstable poles.

For 0 < -1/k < 1 (k < -1), system has one unstable pole.

Of course, this agrees with our Routh and root locus analysis.

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