

5.4) Fully Coupled Iteration

B) 3D IBLT

Reading: See reference list
Veldman, Orta.

6.1) Stability and Transition

A) Small Perturbation Theory

B) Orr-Sommerfeld Eqn.

Reading: Sch 449-483, White 335-355

A) Fully Coupled Iteration

Last lecture, we showed that weakly coupled viscous-inviscid iteration is unstable - need ^{mutual} interaction laws

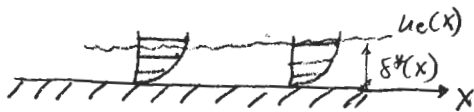
Example 2D flow

IBLT: $u_c = \frac{m/p}{h - \delta^*}$

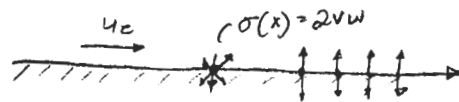
Classical: $u_c = \frac{m/p}{h}$

Solve 3x3 system for θ , δ^* , and u_c

In 2D IBLT, local interaction law is not strictly correct, since outer flow may be elliptic $\Rightarrow u_c(x)$ depends on $\delta^*(x)$ everywhere. One approximate solution is Hilbert integral from thin airfoil theory. Applied rigorously to flat plate



\Rightarrow



$\sigma = \Delta(\vec{v} \cdot \hat{n}) = 2v_w$
 $= 2 \frac{d}{dx}(u_c \delta^*)$

$\Phi(x, y) = \frac{1}{2\pi} \int \sigma(x_0) \ln \sqrt{(x-x_0)^2 + y^2} dx_0$

$u(x, y) = \frac{1}{2\pi} \int \sigma(x_0) \frac{x-x_0}{(x-x_0)^2 + y^2} dx_0$. at $y=0$ $u(x, 0) = u_0 = \frac{1}{2\pi} \int \frac{\sigma(x_0) dx_0}{x-x_0} = 2 \frac{d}{dx}(m/p)$

$$\nabla \cdot (\phi_1 \nabla \phi_2) - \nabla \cdot (\phi_2 \nabla \phi_1)$$

$$\cancel{\nabla \phi_1 \cdot \nabla \phi_2} + \phi_1 \nabla^2 \phi_2 - \cancel{\nabla \phi_2 \cdot \nabla \phi_1} - \phi_2 \nabla^2 \phi_1$$

$$\bar{\Phi} = U_\infty(x + \varphi)$$

$$\frac{\partial \bar{\Phi}}{\partial x} = u_c = U_\infty + \varphi_x$$

$$u_c = U_\infty + \frac{1}{2\pi} \int \frac{\sigma(x_0) dx_0}{x - x_0}$$

$$= U_\infty + \frac{1}{\pi} \int \frac{d(M/\rho)}{x - x_0}$$

← Veldman.

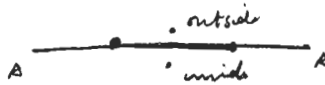
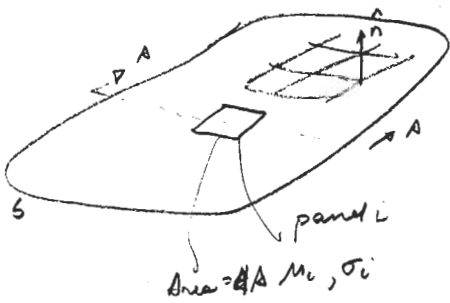
$u_c(x)$ is influenced by $\sigma(x)$ distribution at upstream and downstream points. ① Effect dies off as $1/r$, ② neglects "high sensitivity" regions like T-E.

Numerical implementation:

$$u_c^{n+1}(x) - u_c^n(x) = \frac{1}{\pi} \int \frac{d[(M/\rho)^{n+1} - (M/\rho)^n]}{x - x_0}$$

incremental update.

"Exact" interaction law for 2-D and 3-D flows is developed using panel methods (20-30) + BL method (usually integral)



$$\phi_o - \phi_{in} = \mu \text{ doublet strength}$$

$$\frac{\partial \phi_o}{\partial n}_{out} - \frac{\partial \phi}{\partial n}_{in} = \sigma \text{ source strength}$$

Green's theorem:

$$\bar{\Phi}(P) = \frac{1}{4\pi} \oint_A \left(\frac{1}{r} \nabla \phi - \phi \nabla \frac{1}{r} \right) \cdot \hat{n} dA + \phi_{\infty}$$

value of $\bar{\Phi}$ at any point in terms of $\frac{\partial \phi}{\partial n}$ at boundary and ϕ

$$\Phi = \oint_S \left[M \nabla \cdot \hat{n} + \frac{1}{r} \sigma \right] \frac{dA}{4\pi} + \Phi_\infty$$

$$4\pi \bar{I} \bar{M} = \bar{a} \bar{M} + \bar{b} \bar{\sigma} + 4\pi \bar{I} \Phi_\infty$$

$$\bar{A} \bar{M} = \bar{b} \bar{\sigma} + 4\pi \bar{I} \Phi_\infty$$

$$\bar{M} = \bar{b}' \bar{\sigma} + 4\pi \bar{A}'^{-1} \Phi_\infty$$

$$\bar{\Phi} = \bar{b}' \left(\frac{\partial \bar{M}}{\partial s} \right) + 4\pi \bar{A}'^{-1} \Phi_\infty$$

↑ streamwise gradient of mass def. ?

$$\bar{u}_c = \bar{b}' \bar{M} + \bar{c} \Phi_\infty$$

↳ insert in BL eqn.

Hy Coupled Theories

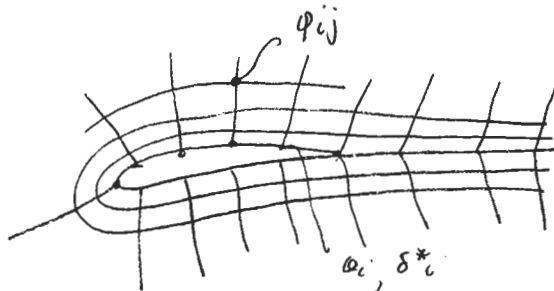
combine Φ, θ, δ^* into one state vector. The governing equations are

$$\nabla^2 \Phi = 0$$

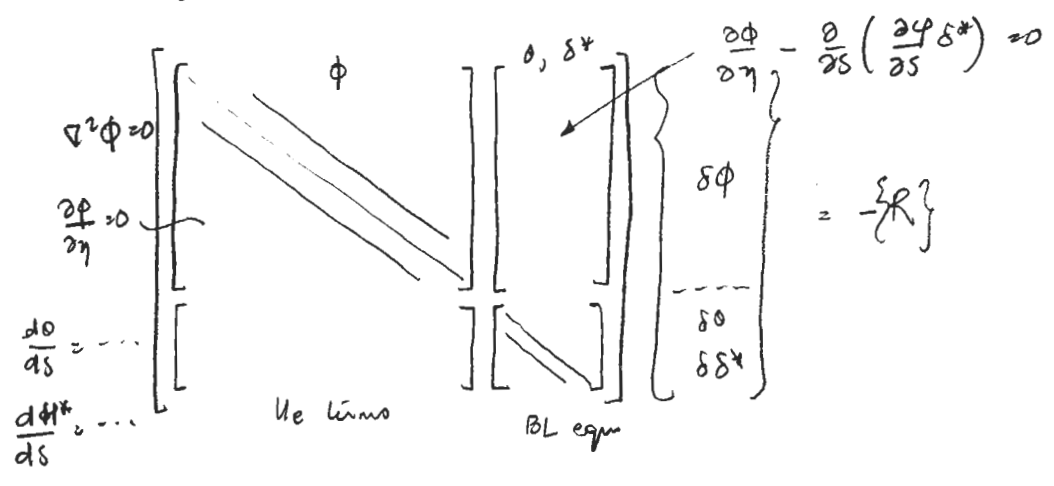
$$\frac{\partial \Phi}{\partial n} = V_w = \frac{\partial}{\partial s} \left(\frac{\partial \Phi}{\partial s} \cdot \delta^* \right)$$

$$\frac{d\theta}{ds} = \dots$$

$$\frac{dH^*}{ds} = \dots$$



Resulting in one overall Newton system



- Direct/inverse iteration neglects off-diagonal matrices
- Finite-diff method can also be used, but at significant increase in computation cost. (F_{ij}, U_{ij}, S_{ij})
- Integral method natural choice for IBLT approach.



References:

- [1] M.J. Lighthill. On displacement thickness. *Journal of Fluid Mechanics*, 4:383-392, 9 1958.
- [2] J.E. Carter. A new boundary layer inviscid iteration technique for separated flow. AIAA-79-1450, Jul 1979.
- [3] R.E. Melnik. Turbulent interactions on airfoils at transonic speeds - recent developments. In *Conference on Computation of Viscous-Inviscid Interactions*, 1980. AGARD-CP-291.
- [4] A.E.P. Veldman. The calculation of incompressible boundary layers with strong viscous-inviscid interaction. In *Conference on Computation of Viscous-Inviscid Interactions*, 1980. AGARD-CP-291.
- [5] L.B. Wigton and M. Holt. Viscous-inviscid interaction in transonic flow. AIAA-81-1003, 1981.
- [6] J.C. Le Balleur. Strong matching method for computing transonic viscous flows including wakes and separations. *La Recherche Aerospaciale*, 1981-3:21-45, 1981. English Edition.
- [7] D.E. Edwards and J.E. Carter. A quasi-simultaneous finite difference approach for strongly interacting flow. In *Third Symposium on Numerical and Physical Aspects of Aerodynamic Flows*, Long Beach, California, Jan 1985.
- [8] R.E. Melnik, R.S. Rudman, and J.W. Brook. The computation of viscous/ inviscid interaction on airfoils with separated flow. In *Third Symposium on Numerical and Physical Aspects of Aerodynamic Flows*, Long Beach, California, Jan 1985.
- [9] M. Drela and M.B. Giles. Viscous-inviscid analysis of transonic and low Reynolds number airfoils. *AIAA Journal*, 25(10): 1347-1355, Oct 1987.
- [10] R.C. Lock and B.R. Williams. Viscous-inviscid interactions in external aerodynamics. *Progress in Aeronautical Sciences*, 24:51-1717 1987.
- [11] M. Drela. XFOIL: An analysis and design system for low Reynolds number airfoils. In T. J. Mueller, editor, *Low Reynolds Number Aerodynamics*. Springer-Verlag, Jun 1989. Lecture Notes in Engineering, No. 54.