

Application Tasks

5. The 2-D stress-strain equation for an orthotropic material can be written as:

$$\sigma_{\alpha\beta} = E_{\alpha\beta\gamma\delta}^* \epsilon_{\gamma\delta} \Rightarrow \sigma_{11} = E_{1111}^* \epsilon_{11} + E_{1122}^* \epsilon_{22} \quad (1)$$

$$\sigma_{22} = E_{1122}^* \epsilon_{11} + E_{2222}^* \epsilon_{22} \quad (2)$$

$$\sigma_{12} = 2E_{1212}^* \epsilon_{12} \quad (3)$$

Next, write the stress-strain equations in terms of the strains (compliances! See Unit 5, p. 17)

$$\epsilon_{11} = \frac{1}{E_L} \sigma_{11} - \frac{\nu_{LT}}{E_L} \sigma_{22} - \frac{\nu_{L3}}{E_L} \sigma_{33} \quad (4)$$

$$\epsilon_{22} = -\frac{\nu_{TL}}{E_L} \sigma_{11} + \frac{1}{E_T} \sigma_{22} - \frac{\nu_{T3}}{E_T} \sigma_{33} \quad (5)$$

$$\epsilon_{33} = -\frac{\nu_{L3}}{E_L} \sigma_{11} - \frac{\nu_{T3}}{E_T} \sigma_{22} + \frac{1}{E_3} \sigma_{33} \quad (6)$$

$$\epsilon_{23} = \frac{1}{2G_{T3}} \sigma_{23} \quad (7)$$

$$\epsilon_{13} = \frac{1}{2G_{L3}} \sigma_{13} \quad (8)$$

$$\epsilon_{12} = \frac{1}{2G_{LT}} \sigma_{12} \quad (9)$$

* Note that the subscript L and T correspond to

1 and 2, respectively.

Now substitute the plane stress condition of

$$\sigma_{33} = \sigma_{12} = \sigma_{23} = 0 \quad (10)$$

into equations (4) - (9) to get:

$$(4) \rightarrow \epsilon_{11} = \frac{1}{E_L} \sigma_{11} - \frac{\nu_{LT}}{E_L} \sigma_{22} \quad (11)$$

$$(5) \rightarrow \epsilon_{22} = -\frac{\nu_{TL}}{E_T} \sigma_{11} + \frac{1}{E_T} \sigma_{22} \quad (12)$$

$$(6) \rightarrow \epsilon_{33} = -\frac{\nu_{L3}}{E_L} \sigma_{11} - \frac{\nu_{T3}}{E_T} \sigma_{22} \quad (13)$$

$$(7) \rightarrow \epsilon_{23} = 0 \quad (14)$$

$$(8) \rightarrow \epsilon_{13} = 0 \quad (15)$$

$$(9) \rightarrow \epsilon_{12} = \frac{1}{2G_{LT}} \sigma_{12} \quad (16)$$

The out-of-plane deformation is expressed in equation (13) but is not of primary interest in this problem. Neither are the out-of-plane shear strains which are zero as found in equations (14) and (15).

We can now relate the 2-D stiffness tensor, E_{ijkl}^* , to the elastic constants by comparing equations

(1) - (3) with equations (11), (12) and (16). Use matrix form to make the comparison straightforward.

For equations (1) - (3):

$$\begin{Bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{Bmatrix} = \begin{bmatrix} E_{1111}^* & E_{1122}^* & 0 \\ E_{1122}^* & E_{2222}^* & 0 \\ 0 & 0 & E_{1212}^* \end{bmatrix} \begin{Bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{12} \end{Bmatrix} \quad (17)$$

Similarly for (11), (12) and (16):

$$\begin{Bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{12} \end{Bmatrix} = \begin{bmatrix} 1/E_L & -\nu_{LT}/E_L & 0 \\ -\nu_{TL}/E_T & 1/E_T & 0 \\ 0 & 0 & 1/2G_{LT} \end{bmatrix} \begin{Bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{Bmatrix} \quad (18)$$

(2-D compliance form: $\underline{\epsilon} = \underline{S} \underline{\sigma}$)

In order to compare equation (17) with equation (18) one of the equations needs to be inverted.

Choosing equation (17):

$$\begin{Bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{12} \end{Bmatrix} = \begin{bmatrix} \frac{E_{2222}^*}{E_{1111}^* E_{2222}^* - (E_{1122}^*)^2} & \frac{-E_{1122}^*}{E_{1111}^* E_{2222}^* - (E_{1122}^*)^2} & 0 \\ \frac{-E_{1122}^*}{E_{1111}^* E_{2222}^* - (E_{1122}^*)^2} & \frac{E_{1111}^*}{E_{1111}^* E_{2222}^* - (E_{1122}^*)^2} & 0 \\ 0 & 0 & \frac{1}{2E_{1212}^*} \end{bmatrix} \begin{Bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{Bmatrix}$$

↳ (19)

Now compare the elements of equations (18) and (19):

$$\bullet \quad \frac{1}{\bar{E}_L} = \frac{\bar{E}_{2222}^*}{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2}$$

$$\Rightarrow \bar{E}_L = E_{1111}^* - \frac{(\bar{E}_{1122}^*)^2}{\bar{E}_{2222}^*} \quad (20a)$$

$$\bullet \quad -\frac{\nu_{LT}}{\bar{E}_L} = -\frac{\bar{E}_{1122}^*}{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2}$$

$$\Rightarrow \nu_{LT} = \frac{\bar{E}_{1122}^*}{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2} \bar{E}_L$$

Using the result above of equation (20a):

$$\nu_{LT} = \frac{\bar{E}_{1122}^*}{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2} \frac{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2}{\bar{E}_{2222}^*}$$

$$\Rightarrow \nu_{LT} = \frac{\bar{E}_{1122}^*}{\bar{E}_{2222}^*} \quad (20b)$$

$$\bullet \quad \frac{1}{\bar{E}_T} = \frac{E_{1111}^*}{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2}$$

$$\Rightarrow \bar{E}_T = \bar{E}_{2222}^* - \frac{(\bar{E}_{1122}^*)^2}{E_{1111}^*} \quad (20c)$$

$$\bullet \quad -\frac{\nu_{TL}}{\bar{E}_T} = -\frac{\bar{E}_{1122}^*}{E_{1111}^* \bar{E}_{2222}^* - (\bar{E}_{1122}^*)^2}$$

using the result above of equation (20c):

$$N_{TL} = \frac{E_{1122}^*}{E_{1111}^* E_{2222}^* - (E_{1122}^*)^2} \frac{E_{1111}^* E_{2222}^* - (E_{1122}^*)^2}{E_{1111}^*}$$

$$\Rightarrow N_{TL} = \frac{E_{1122}^*}{E_{1111}^*} \quad (20d)$$

$$\bullet \frac{1}{2G_{LT}} = \frac{1}{2\bar{E}_{1212}^*}$$

$$\Rightarrow G_{LT} = \bar{E}_{1212}^* \quad (20e)$$

Summarizing:

$$E_L = E_{1111}^* - \frac{(E_{1122}^*)^2}{E_{2222}^*}$$

$$E_T = E_{2222}^* - \frac{(E_{1122}^*)^2}{E_{1111}^*}$$

$$N_{LT} = E_{1122}^* / E_{2222}^*$$

$$N_{TL} = E_{1122}^* / E_{1111}^*$$

$$G_{LT} = \bar{E}_{1212}^*$$

(20a-e)

If instead of inverting equation (17) one inverted equation (18) and then did the comparison of equations, one would get the relations in inverse: E_{eff}^* in terms of the in-plane engineering constants:

$$\begin{aligned}
 E_{1111}^* &= \frac{E_L}{1 - \nu_{LT}\nu_{TL}} \\
 E_{2222}^* &= \frac{\nu_{LT}E_T}{1 - \nu_{LT}\nu_{TL}} = \frac{\nu_{TL}E_L}{1 - \nu_{LT}\nu_{TL}} \\
 E_{2222}^* &= \frac{E_T}{1 - \nu_{LT}\nu_{TL}} \\
 E_{1212}^* &= G_{LT}
 \end{aligned} \tag{21}$$

6. For the isotropic case, the same relation between E_{eff}^* and the elastic constants hold. The differences are that isotropic materials have the same properties in all directions:

$$E_L = E_T = E$$

$$\nu_{LT} = \nu_{TL} = \nu$$

$$\text{and } E_{1111}^* = E_{2222}^* \text{ (found in problem \# 2)}$$

and there is a relationship between E , ν , and G :

$$G = \frac{E}{2(1+\nu)}$$

We also had from Problem #2:

$$E_{1212}^* = \frac{E_{1111} - E_{1122}}{2}$$

with: $E_{1111}^* = E_{1111} - \frac{E_{1122}^2}{E_{1111}}$ and $E_{1122}^* = E_{1122} - \frac{E_{1122}^2}{E_{1111}}$

So: $E_{1111} = E_{1111}^* + \frac{E_{1122}^2}{E_{1111}}$ and $E_{1122} = E_{1122}^* + \frac{E_{1122}^2}{E_{1111}}$

Using in the expression for E_{1212}^* :

$$E_{1212}^* = \frac{1}{2} \left\{ E_{1111}^* + \frac{E_{1122}^2}{E_{1111}} - \left(E_{1122}^* + \frac{E_{1122}^2}{E_{1111}} \right) \right\}$$

finally: $E_{1212}^* = \frac{1}{2} (E_{1111}^* - E_{1122}^*)$

again, only 2 independent constants

Using these facts in Equations (20 a-c)

$$\left. \begin{aligned} E_L = \bar{E} &= E_{1111}^* - \frac{(E_{1122}^*)^2}{E_{1111}^*} \\ E_T = E &= E_{1111}^* - \frac{(E_{1122}^*)^2}{E_{1111}^*} \end{aligned} \right\} \text{the same}$$

$$\begin{array}{l}
 \dots \\
 \nu_{LT} = \nu = \frac{E_{1122}^*}{E_{1111}^*} \dots \\
 \nu_{TL} = \nu = \frac{E_{1122}^*}{E_{1111}^*} \dots \\
 G_{LT} = \frac{E_{1111}^* - E_{1122}^*}{2}
 \end{array}
 \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{the same}$$

If one goes the other way and uses equations (2), then:

$$\begin{array}{l}
 E_{1111}^* = \frac{E}{1-\nu^2} \\
 E_{1122}^* = \frac{\nu E}{1-\nu^2} \\
 E_{2222}^* = \frac{E}{1-\nu^2} \quad \leftarrow \text{the same} \\
 \text{or } E_{1111}^* \\
 E_{1212}^* = G = \frac{E}{2(1+\nu)}
 \end{array}$$

Does $E_{1212}^* = \frac{1}{2}(E_{1111}^* - E_{1122}^*)$? check

$$E_{1212}^* = \frac{E}{2(1+\nu)} \stackrel{?}{=} \frac{1}{2}(E_{1111}^* - E_{1122}^*) = \frac{E - \nu E}{2(1+\nu)}$$

$$1 - \nu^2 = (1 + \nu)(1 - \nu)$$

$$\Rightarrow \frac{E - \nu E}{2(1 - \nu^2)} = \frac{E(1 - \nu)}{2(1 + \nu)(1 - \nu)}$$

$$\text{So: } \frac{E}{2(1 + \nu)} \stackrel{?}{=} \frac{E}{2(1 + \nu)} \quad \underline{\underline{\text{YES!}}}$$