## Capstan—a mechanical amplifier

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A schematic diagram of a basic capstan and a force diagram for a small segment of the rope are shown in the figures.

 $F_{normal} = F \sin \Delta \theta / 2 + (F + \Delta F) \sin \Delta \theta / 2$ 

In the limit of small angles

 $F_{normal} = F d\theta/2 + (F+dF) d\theta/2$ 

Assuming continuous slip and Coulomb friction between rope and drum,

 $dF = \mu F_{normal} = \mu \frac{2F + dF}{2} d\theta$   $dF = F d\theta \text{ or } d \ln F = \mu d\theta$ Integrating from 0 to  $\theta$   $F_{out} = e^{\mu\theta} F_{control}$ Note that this relation is only valid if  $\omega r \ge v_{control}$ From continuity:  $v_{control} = v_{out}$ Torque required of capstan drive:  $\tau = (F_{out} - F_{control}) r = (e^{\mu\theta} - 1) r F_{control}$ Power dissipated:

 $P_{dissipated} = \tau \omega + F_{control} v_{control} - F_{out} v_{out}$ 

 $P_{dissipated} = (e^{\mu\theta} - 1) r F_{control} \omega - (e^{\mu\theta} - 1) F_{control} v_{control}$ 

Note that  $P_{dissipated} \ge 0$  with  $P_{dissipated} = 0$  if  $\omega r = v_{control}$ 

A bond graph follows:



Mod. Sim. Dyn. Sys.

This is a three-port resistor.



Typical boundary conditions result in the following causality.



Constitutive equations are

F <sub>out</sub>	0	0	e <sup>μθ</sup> -	Vout
$  \tau   =$	0	0	$(e^{\mu\theta}-1)r$	ω
_v <sub>control</sub> _	$L_1$	0	0 _	Fcontrol