

Table 13—Coefficients in Equations of Motion

## Vertical Mode

$$A_{11} = \int a_{11} dx$$

$$A_{13} = \int a_{13} dx$$

$$A_{31} = A_{13}$$

$$B_{11} = \int b_{11} dx$$

$$B_{13} = \int b_{13} dx$$

$$B_{31} = B_{13}$$

$$A_{15} = - \int x a_{13} dx - \frac{U_0}{\omega_e^2} B_{13}$$

$$B_{15} = - \int x b_{13} dx + U_0 \cdot A_{13}$$

$$A_{51} = - \int x a_{13} dx + \frac{U_0}{\omega_e^2} B_{31}$$

$$B_{51} = - \int x b_{31} dx - U_0 \cdot A_{13}$$

$$A_{33} = \int a_{33} dx$$

$$B_{33} = \int b_{33} dx$$

$$A_{35} = - \int x a_{33} dx - \frac{U_0}{\omega_e^2} B_{33}$$

$$B_{35} = - \int x b_{33} dx + U_0 A_{33}$$

$$A_{53} = - \int x a_{33} dx + \frac{U_0}{\omega_e^2} B_{33}$$

$$B_{53} = - \int x b_{33} dx - U_0 A_{33}$$

$$A_{55} = \int x^2 a_{33} dx + \frac{U_0^2}{\omega_e^2} A_{33}$$

$$B_{55} = \int x^2 b_{33} dx + \frac{U_0^2}{\omega_e^2} B_{33}$$

$$C_{33} = \int c_{33} dx = \rho g \int B(x) dx$$

$$C_{35} = C_{53} = - \int x c_{33} dx = -\rho g \int x B(x) dx$$

$$C_{55} = \rho g \nabla \overline{GM}_L + LCF^2 C_{33}$$

$$\approx \int x^2 c_{33} dx = \rho g \int x^2 B(x) dx$$

## Horizontal Mode

$$A_{22} = \int a_{22} dx$$

$$A_{24} = A_{42} = \int a_{24} dx$$

$$A_{26} = \int x a_{22} dx + \frac{U_0}{\omega_e^2} B_{22}$$

$$A_{44} = \int a_{44} dx$$

$$A_{46} = \int x a_{24} dx + \frac{U_0}{\omega_e^2} B_{24}$$

$$B_{22} = \int b_{22} dx$$

$$B_{24} = B_{42} = \int b_{24} dx$$

$$B_{26} = \int x b_{22} dx - U_0 A_{22}$$

$$B_{44} = \int b_{44} dx + B_e = B_{44}^*$$

$$B_{46} = \int x b_{24} dx - U_0 A_{24}$$

$$A_{62} = \int x a_{22} dx - \frac{U_0}{\omega_e^2} B_{22}$$

$$B_{62} = \int x b_{22} dx + U_0 A_{22}$$

$$A_{64} = \int x a_{24} dx - \frac{U_0}{\omega_e^2} B_{24}$$

$$B_{64} = \int x b_{24} dx + U_0 A_{24}$$

$$A_{66} = \int x^2 a_{22} dx + \frac{U_0^2}{\omega_e^2} A_{22}$$

$$B_{66} = \int x^2 b_{22} dx + \frac{U_0^2}{\omega_e^2} B_{22}$$

$$C_{44} \approx \rho g \nabla \overline{GM}_T$$

All integrals are taken over the ship length.

The generalized normals for  $k = 4, 5, 6$  can likewise be approximated by their two-dimensional equivalents,

$$\begin{aligned} n_4 &= yn_3 - zn_2 \\ &\approx N_4 \\ &= \left( y \frac{\partial b}{\partial z} + z \right) / \sqrt{1 + \left( \frac{\partial b}{\partial z} \right)^2} \end{aligned} \quad (149a)$$

$$\begin{aligned} n_5 &= zn_1 - xn_3 \\ &\approx -xN_3 \end{aligned} \quad (149b)$$

$$\begin{aligned} n_6 &= xn_2 - yn_1 \\ &\approx +xN_2 \end{aligned} \quad (149c)$$

It was at this point in the analysis by Salvesen, et al (1970) that the surge degree of freedom was eliminated by arguing that  $N_1 \ll N_k$ ,  $k = 2, 3, \dots, 6$ .