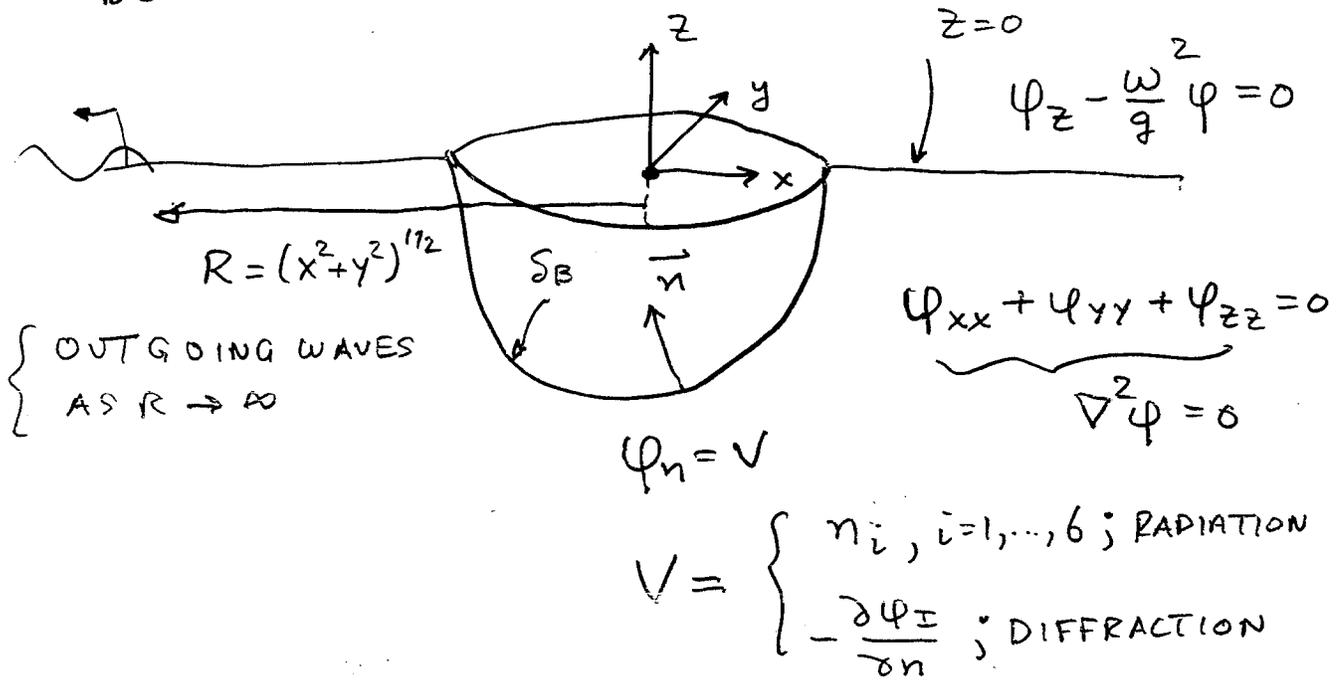


# SOLUTION OF WAVE-BODY INTERACTION PROBLEMS

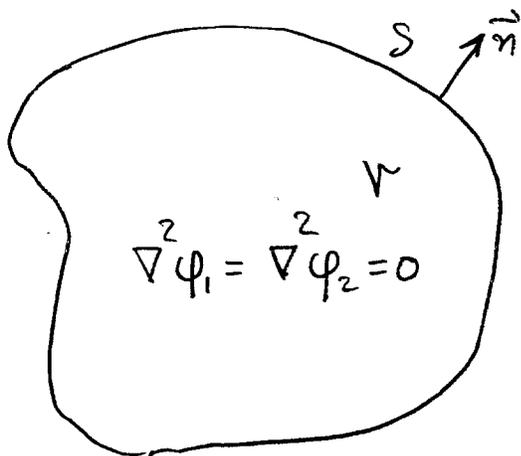
- TWO TYPES OF WAVE BODY INTERACTION PROBLEMS ARE ENCOUNTERED FREQUENTLY IN APPLICATIONS AND SOLVED BY THE METHODS DESCRIBED IN THIS SECTION
  - ZERO-SPEED LINEAR WAVE BODY INTERACTIONS IN THE FREQUENCY DOMAIN IN 2D AND 3D
  - FORWARD-SPEED SEAKEEPING PROBLEMS IN THE FREQUENCY OR TIME DOMAIN IN THREE DIMENSIONS (LINEAR & NONLINEAR)
- A CONSENSUS HAS BEEN REACHED OVER THE PAST TWO DECADES THAT THE MOST EFFICIENT AND ROBUST SOLUTION METHODS ARE BASED ON GREEN'S THEOREM USING EITHER A WAVE-SOURCE POTENTIAL OR THE RANKINE SOURCE AS THE GREEN FUNCTION. —
- THE NUMERICAL SOLUTION OF THE RESULTING INTEGRAL EQUATIONS IN PRACTICE IS IN ALMOST ALL CASES CARRIED OUT BY PANEL METHODS. —

# FREQUENCY-DOMAIN RADIATION-DIFFRACTION, $\omega = 0$

BOUNDARY-VALUE PROBLEM:



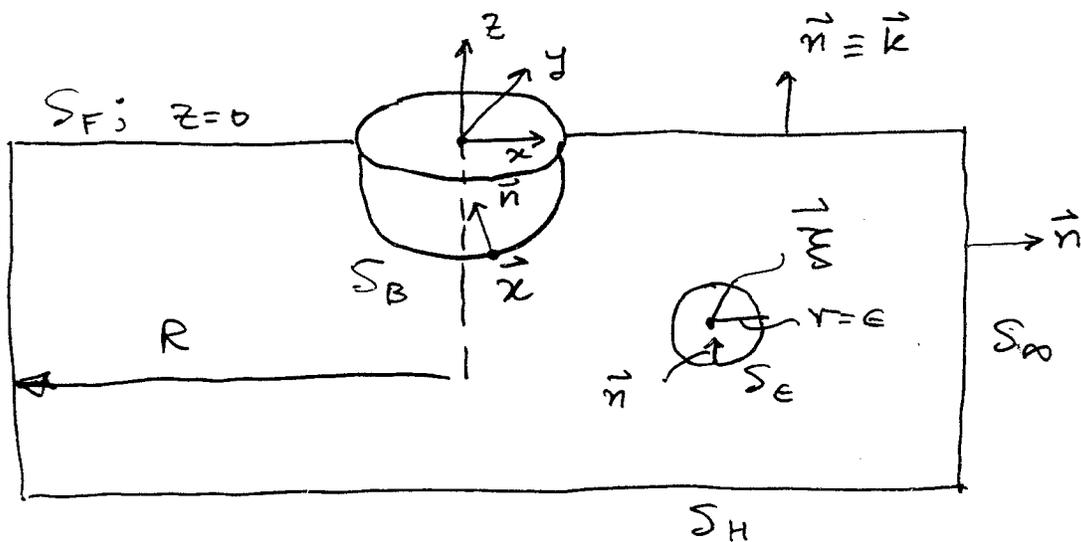
- GREEN'S THEOREM GENERATES A BOUNDARY INTEGRAL EQUATION FOR THE COMPLEX POTENTIAL  $\phi$  OVER THE BODY BOUNDARY  $S_B$  FOR THE PROPER CHOICE OF THE GREEN FUNCTION:



$$\oint_S \left( \phi_1 \frac{\partial \phi_2}{\partial n} - \phi_2 \frac{\partial \phi_1}{\partial n} \right) ds = 0$$

FOR ANY  $\phi_1, \phi_2$  THAT SOLVE THE LAPLACE EQ. IN A CLOSED VOLUME  $V$ .

DEFINE THE VOLUME  $V$  AND  $S$  AS FOLLOWS:



THE FLUID VOLUME  $V$  IS ENCLOSED BY THE UNION OF SEVERAL SURFACES

$$S \equiv S_B + S_F + S_\infty + S_H + S_e$$

$S_B$ : MEAN POSITION OF BODY SURFACE

$S_F$ : MEAN POSITION OF THE FREE SURFACE

$S_\infty$ : BOUNDING CYLINDRICAL SURFACE WITH RADIUS  $R = (x^2 + y^2)^{1/2}$ . WILL BE ALLOWED TO EXPAND AFTER THE STATEMENT OF GREEN'S THEOREM

$S_H$ : SEAFLOOR (ASSUMED FLAT) OR A SURFACE WHICH WILL BE ALLOWED TO APPROACH  $z = -\infty$

$S_e$ : SPHERICAL SURFACE WITH RADIUS  $r=e$  CENTERED AT POINT  $\vec{x}$  IN THE FLUID DOMAIN

$\vec{n}$ : UNIT NORMAL VECTOR ON  $S$ , AT POINT  $\vec{x}$  ON  $S$

DEFINE TWO VELOCITY POTENTIALS  $\varphi_i(\vec{x})$ :

$\varphi_1(\vec{x}) = \varphi(\vec{x}) \equiv$  UNKNOWN COMPLEX  
RADIATION OR DIFFRACTION  
POTENTIAL

$\varphi_2(\vec{x}) = G(\vec{x}; \vec{\xi}) \equiv$  GREEN FUNCTION VALUE  
AT POINT  $\vec{x}$  DUE TO A  
SINGULARITY CENTERED  
AT POINT  $\vec{\xi}$ .

TWO TYPES OF GREEN FUNCTIONS WILL BE  
USED:

● RANKINE SOURCE:  $\nabla_x^2 G = 0$

$$\begin{aligned} G(\vec{x}; \vec{\xi}) &= -\frac{1}{4\pi} |\vec{x} - \vec{\xi}|^{-1} = -\frac{1}{4\pi r} = \\ &= -\frac{1}{4\pi} \left\{ (x-\xi)^2 + (y-\eta)^2 + (z-\zeta)^2 \right\}^{-1/2} \end{aligned}$$

NOTE THAT THE FLUX OF FLUID EMITTED  
FROM  $\vec{\xi}$  IS EQUAL TO 1. (VERIFY)

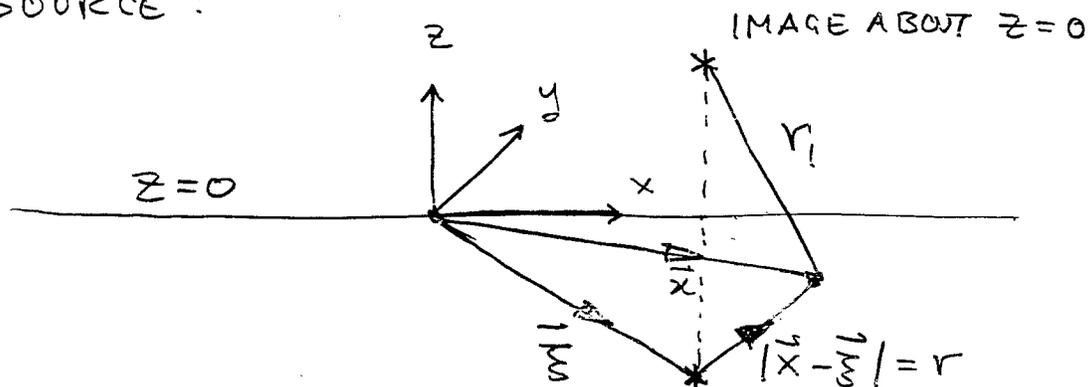
— THIS RANKINE SOURCE AND ITS GRADIENT WITH  
RESPECT TO  $\vec{\xi}$  (DIPOLES) IS THE GREEN FUNCTION  
THAT WILL BE USED IN THE SHIP SEA KEEPING  
PROBLEM

## ● HAVELOCK'S WAVE SOURCE POTENTIAL

... ALSO KNOWN AS THE  $U=0$  WAVE GREEN FUNCTION IN THE FREQUENCY DOMAIN.

— SATISFIES THE FREE SURFACE CONDITION AND NEAR  $\frac{\omega}{g} = 0$  BEHAVES LIKE A RANKINE

SOURCE :



THE FOLLOWING CHOICE FOR  $G(\vec{x}; \vec{\xi})$  SATISFIES THE LAPLACE EQUATION AND THE FREE-SURFACE CONDITION :

$$G(\vec{x}, \vec{\xi}) = -\frac{1}{4\pi} \left( \frac{1}{r} + \frac{1}{r_1} \right)$$

$$-\frac{k}{2\pi} \int_0^{\infty} \frac{du}{u-k} e^{u(z+\xi)} J_0(uR)$$

WHERE:  $k = \omega^2/g$

$$R^2 = (x-\xi)^2 + (y-\eta)^2$$

$J_0(uR)$  = BESSEL FUNCTION OF ORDER ZERO

$\int_0^{\infty}$  : CONTOUR INDENTED ABOVE POLE  $u=k$

VERIFY THAT WITH RESPECT TO THE ARGUMENT  $\vec{x}$ , THE VELOCITY POTENTIAL  $\varphi_2(\vec{x}) \equiv G(\vec{x}; \vec{\xi})$  SATISFIES THE FREE SURFACE CONDITION:

$$\frac{\partial \varphi_2}{\partial z} - k \varphi_2 = 0, \quad z=0$$

$$\varphi_2 \sim -\frac{1}{4\pi} r^{-1}, \quad \vec{x} \rightarrow \infty$$

AS  $kR \rightarrow \infty$ :

$$G \sim -\frac{i}{2} k e^{k(z+\xi)} H_0^{(2)}(kR)$$

WHERE  $H_0^{(2)}(kR)$  IS THE HANKEL FUNCTION OF THE SECOND KIND AND ORDER ZERO.

AS  $kR \rightarrow \infty$ :

$$H_0^{(2)}(kR) \sim \sqrt{\frac{2}{\pi kR}} e^{-i(kR - \frac{\pi}{4})} + O(1/R)$$

• THEREFORE THE REAL VELOCITY POTENTIAL

$$G = \text{Re} \{ G e^{i\omega t} \}$$

REPRESENTS OUTGOING RING WAVES OF THE FORM  $\propto e^{i(\omega t - kR)}$  HENCE SATISFYING THE RADIATION CONDITION. —

- A SIMILAR FAR-FIELD RADIATION CONDITION IS SATISFIED BY THE VELOCITY POTENTIAL  $\varphi_1(\vec{x}) \equiv \varphi(\vec{x})$

$$\varphi_1 \sim \frac{A(\theta)}{(kR)^{1/2}} e^{kz - ikR} + O(1/R)$$

IT FOLLOWS THAT ON  $S_\infty$ :

- $\frac{\partial \varphi_1}{\partial n} = \frac{\partial \varphi_1}{\partial R} = -ik\varphi_1 \dots$

- $\frac{\partial \varphi_2}{\partial n} = \frac{\partial \varphi_2}{\partial R} = -ik\varphi_2 \dots$

THEREFORE:

$$\varphi_1 \frac{\partial \varphi_2}{\partial n} - \varphi_2 \frac{\partial \varphi_1}{\partial n} = -ik(\varphi_1 \varphi_2 - \varphi_2 \varphi_1) = 0$$

WITH ERRORS THAT DECAY LIKE  $R^{-3/2}$ , HENCE FASTER THAN  $R$ , WHICH IS THE RATE AT WHICH THE SURFACE  $S_\infty$  GROWS AS  $R \rightarrow \infty$ .

ON  $S_F (z=0)$ :  $\frac{\partial \varphi_1}{\partial n} = \frac{\partial \varphi_1}{\partial z}$ ,  $\frac{\partial \varphi_2}{\partial n} = \frac{\partial \varphi_2}{\partial z} \dots$

$$\varphi_1 \frac{\partial \varphi_2}{\partial n} - \varphi_2 \frac{\partial \varphi_1}{\partial n} = \varphi_1 \frac{\partial \varphi_2}{\partial z} - \varphi_2 \frac{\partial \varphi_1}{\partial z} = \gamma(\varphi_1 \varphi_2 - \varphi_2 \varphi_1) = 0 \dots$$

- IT FOLLOWS THAT UPON APPLICATION OF GREEN'S THEOREM ON THE UNKNOWN POTENTIAL

$\varphi_1 \equiv \varphi$  AND THE WAVE GREEN FUNCTION

$\varphi_2 \equiv G$  ONLY THE INTEGRALS OVER  $S_B$

AND  $S_E$  SURVIVE.

- OVER  $S_H$ , EITHER  $\frac{\partial \varphi_1}{\partial n} = \frac{\partial \varphi_2}{\partial n} = 0$  BY VIRTUE

OF THE BOUNDARY CONDITION IF THE WATER

DEPTH IS FINITE OR  $\frac{\partial \varphi_1}{\partial z} \rightarrow 0, \frac{\partial \varphi_2}{\partial z} \rightarrow 0$  AS

$z \rightarrow -\infty$  BY VIRTUE OF THE VANISHING OF

THE RESPECTIVE FLOW VELOCITIES AT LARGE

DEPTHS.

- THERE REMAINS TO INTERPRET AND EVALUATE

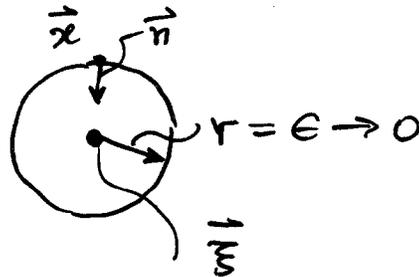
THE INTEGRAL OVER  $S_E$  AND  $S_B$ . START

WITH  $S_E$ :

$$I_E = \iint_{S_E} \left( \varphi_1 \frac{\partial \varphi_2}{\partial n} - \varphi_2 \frac{\partial \varphi_1}{\partial n} \right) ds$$

OR

$$I_\epsilon = \iint_{S_\epsilon} \left( \psi \frac{\partial G}{\partial n} - G \frac{\partial \psi}{\partial n} \right) dS_x,$$



NOTE THAT THE INTEGRAL OVER  $S_\epsilon$  IS OVER THE  $\vec{x}$  VARIABLE WITH  $\vec{x}$  BEING THE FIXED POINT WHERE THE SOURCE IS CENTERED.

$$\text{NEAR } \vec{x}: G \sim -\frac{1}{4\pi r}, \quad \frac{\partial G}{\partial n} = -\frac{\partial G}{\partial r} \sim \frac{1}{4\pi r^2}$$

$$\psi \rightarrow \psi\left(\frac{\vec{x}}{\epsilon}\right) = \psi(\vec{x}) \quad \text{AS } \epsilon \rightarrow 0$$

$\vec{x} \leftrightarrow \frac{\vec{x}}{\epsilon}$

IN THE LIMIT AS  $r \rightarrow 0$ , THE INTEGRAND OVER THE SPHERE  $S_\epsilon$  BECOMES SPHERICALLY SYMMETRIC AND WITH VANISHING ERRORS

$$I_\epsilon \rightarrow 4\pi r^2 \left[ \psi\left(\frac{\vec{x}}{\epsilon}\right) \frac{1}{4\pi r^2} + G \frac{\partial \psi}{\partial r} \right]$$

$$= \psi\left(\frac{\vec{x}}{\epsilon}\right)$$

IN SUMMARY:

$$\varphi(\vec{\xi}) + \iint_{S_B} \left[ \varphi(\vec{x}) \frac{\partial G(\vec{x}; \vec{\xi})}{\partial n_x} - G(\vec{x}; \vec{\xi}) \frac{\partial \varphi}{\partial n_x} \right] ds_x = 0$$

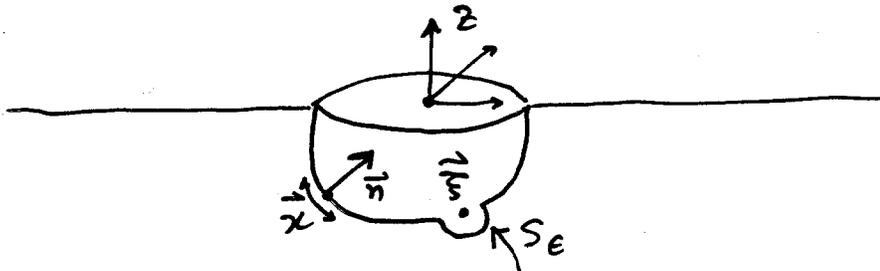
ON  $S_B$ :  $\frac{\partial \varphi}{\partial n_x} = V(x) =$  KNOWN FROM THE BOUNDARY CONDITION OF THE RADIATION AND DIFFRACTION PROBLEMS

- IT FOLLOWS THAT A RELATIONSHIP IS OBTAINED BETWEEN THE VALUE OF  $\varphi(\vec{\xi})$  AT SOME POINT IN THE FLUID DOMAIN AND ITS VALUES  $\varphi(\vec{x})$  AND NORMAL DERIVATIVES OVER THE BODY BOUNDARY:

$$\varphi(\vec{\xi}) + \iint_{S_B} \varphi(\vec{x}) \frac{\partial G(\vec{x}; \vec{\xi})}{\partial n_x} ds_x = \iint_{S_B} G(\vec{x}; \vec{\xi}) V(\vec{x}) ds_x$$

STATED DIFFERENTLY, KNOWLEDGE OF  $\varphi$  AND  $\frac{\partial \varphi}{\partial n}$  OVER THE BODY BOUNDARY ALLOWS THE DETERMINATION OF  $\varphi$  AND UPON DIFFERENTIATION OF  $\nabla \varphi$  IN THE FLUID DOMAIN.

IN ORDER TO DETERMINE  $\varphi(\vec{x})$  ON THE BODY BOUNDARY  $S_B$ , SIMPLY ALLOW  $\vec{s} \rightarrow S_B$  IN WHICH CASE THE SPHERE  $S_\epsilon$  BECOMES A  $1/2$  SPHERE AS  $\epsilon \rightarrow 0$ :



- NOTE THAT  $\vec{s}$  IS A FIXED POINT WHERE THE POINT SOURCE IS CENTERED AND  $\vec{x}$  IS A DUMMY INTEGRATION VARIABLE MOVING OVER THE BODY BOUNDARY  $S_B$ .
- THE REDUCTION OF GREEN'S THEOREM DERIVED ABOVE SURVIVES ALMOST IDENTICALLY WITH A FACTOR OF  $1/2$  NOW MULTIPLYING THE  $I_\epsilon$  INTEGRAL SINCE ONLY  $1/2$  OF THE  $S_\epsilon$  SURFACE LIES IN THE FLUID DOMAIN IN THE LIMIT AS  $\epsilon \rightarrow 0$  AND FOR A BODY SURFACE WHICH IS SMOOTH. IT FOLLOWS THAT:

$$\bullet \quad \frac{1}{2} \varphi(\vec{\xi}) + \iint_{S_B} \varphi(\vec{x}) \frac{\partial G(\vec{x}; \vec{\xi})}{\partial n_x} dS_x$$

$$= \iint_{S_B} G(\vec{x}; \vec{\xi}) V(\vec{x}) dS_x$$

WHERE NOW BOTH  $\vec{x}$  AND  $\vec{\xi}$  LIE ON THE BODY SURFACE. THIS BECOMES AN INTEGRAL EQUATION FOR  $\varphi(\vec{x})$  OVER A SURFACE  $S_B$  OF BOUNDED EXTENT. ITS SOLUTION IS CARRIED OUT WITH PANEL METHODS DESCRIBED BELOW

THE INTERPRETATION OF THE DERIVATIVE UNDER THE INTEGRAL SIGN IS AS FOLLOWS:

$$\begin{aligned} \frac{\partial G}{\partial n_x} &\equiv \vec{n}_x \cdot \nabla_x G(\vec{x}; \vec{\xi}) \\ &\equiv \left( n_1 \frac{\partial}{\partial x} + n_2 \frac{\partial}{\partial y} + n_3 \frac{\partial}{\partial z} \right) G(\vec{x}; \vec{\xi}) \end{aligned}$$

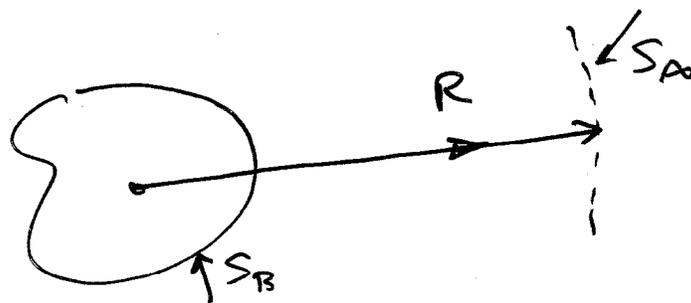
WHERE DERIVATIVES ARE TAKEN WRT THE FIRST ARGUMENT FOR A POINT SOURCE CENTERED AT POINT  $\vec{\xi}$ .

## INFINITE DOMAIN POTENTIAL FLOW SOLUTIONS

IN THE ABSENCE OF THE FREE SURFACE, THE DERIVATION OF THE GREEN INTEGRAL EQUATION REMAINS ALMOST UNCHANGED USING  $G$ :

$$\begin{aligned}\varphi_2(\vec{x}) &= -\frac{1}{4\pi} |\vec{x} - \frac{\vec{z}}{R}|^{-1} \\ &\equiv G(\vec{x}; \frac{\vec{z}}{R})\end{aligned}$$

THE RANKINE SOURCE AS THE GREEN FUNCTION AND USING THE PROPERTY THAT AS  $R \rightarrow \infty$



$$|\nabla\varphi| \sim 1/R^2$$

$$|\nabla G| \sim 1/R^2$$

FOR CLOSED BOUNDARIES  $S_B$  WITH NO SHED WAKES RESPONSIBLE FOR LIFTING EFFECTS

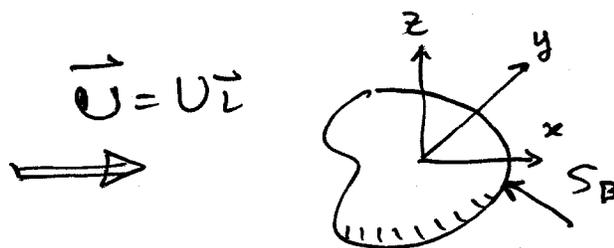
THE RESULTING INTEGRAL EQUATION FOR  $\varphi(\vec{x})$  OVER THE BODY BOUNDARY BECOMES:

$$\bullet \quad \frac{1}{2} \varphi(\vec{\xi}) + \iint_{S_B} \varphi(\vec{x}) \frac{\partial G(\vec{x}; \vec{\xi})}{\partial n_x} dS_x$$

$$= \iint_{S_B} G(\vec{x}; \vec{\xi}) V(\vec{x}) dS_x$$

WITH  $V(\vec{x}) = \frac{\partial \varphi}{\partial n}$ , on  $S_B$

EXAMPLE: UNIFORM FLOW PAST  $S_B$



$$\Phi = Ux + \varphi, \quad \frac{\partial \Phi}{\partial n} = 0, \text{ on } S_B$$

$$\Rightarrow \frac{\partial \varphi}{\partial n} = - \frac{\partial}{\partial n} (Ux) = -n_x U \equiv V(\vec{x})$$

SO THE RHS OF THE GREEN EQUATION BECOMES:

$$\text{RHS} = \iint_{S_B} G(\vec{x}; \vec{\xi}) (-U n_{1x}) dS_x \text{. —}$$