Imagine an arbitrary fluid element which in 2-D is a rectangle with width δx_1 in the x, 1 direction and height δx_2 in the y, 2 direction; the element also has a width δx_3 in the z, 3 direction (Figure 1). Stresses acting on each face can be calculated using the values at point O (center of the element) and applying a Taylor series expansion in each direction:

Shear stress acting on the right wall: $\tau_{12} \mid_{O} + \delta \tau_{a}$ Shear stress acting on the left wall: $\tau_{12} \mid_{O} - \delta \tau_{a}$ Shear stress acting on the bottom wall: $\tau_{21} \mid_{O} - \delta \tau_{b}$ Shear stress acting on the top wall: $\tau_{21} \mid_{O} + \delta \tau_{b}$

in which:

$$\delta \tau_a = \frac{\partial \tau_{12}}{\partial x_1} (\delta x_1/2)$$
$$\delta \tau_b = \frac{\partial \tau_{21}}{\partial x_2} (\delta x_2/2)$$

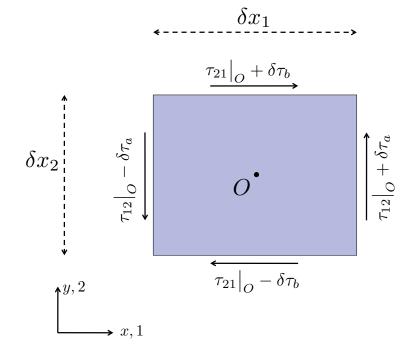


Figure 1: Taylor series expansion for the shear stresses acting on a material element of size $\delta x_1, \, \delta x_2$.

Knowing that the normal stresses acting on each plane will not lead to any net torque around axis x_3 passing through point O one can calculate the net exerted torque on the element (M_O) by accounting for all the shear stresses acting on the element:

$$\sum M_O = (\tau_{12} + \delta\tau_a)(\delta x_2 \delta x_3)(\delta x_1/2) + (\tau_{12} - \delta\tau_a)(\delta x_2 \delta x_3)(\delta x_1/2) - (\tau_{21} + \delta\tau_b)(\delta x_1 \delta x_3)(\delta x_2/2) - (\tau_{21} - \delta\tau_b)(\delta x_1 \delta x_3)(\delta x_2/2)$$

1

$$\sum M_O = (\tau_{12} - \tau_{21})\delta x_1 \delta x_2 \delta x_3 \tag{1}$$

On the other hand we know that the following holds:

$$\sum M_O = I\dot{\omega_3}$$

in which I is the moment of inertia around x_3 axis passing through point O and for a cuboidal element it is:

$$I = \frac{\rho}{12} \delta x_1 \delta x_2 \delta x_3 (\delta x_1^2 + \delta x_2^2) \tag{2}$$

Combining (1) and (2) will result in:

$$\dot{\omega_3} = \frac{12}{\rho} \frac{\tau_{12} - \tau_{21}}{\delta x_1^2 + \delta x_2^2}$$

It is easy to see that if one shrinks the element to a very small volume (i.e. δx_1 and $\delta x_2 \to 0$) the rotational acceleration of the element ($\dot{\omega}_3$) will diverge to infinity unless the shear stress difference also tends to zero at least as fast as $\delta x_i^2 \to 0$ (thus $\tau_{12} - \tau_{21} = 0$). Since infinite rotational acceleration is not physically possible the stress tensor should be symmetric, $\tau_{ij} = \tau_{ji}$.¹

 $\mathbf{2}$

 $^{^{1}}$ The mentioned proof is true in the absence of magneto-hydrodynamic forces or other non-conservative body forces.

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