

2.43 ADVANCED THERMODYNAMICS

Spring Term 2024

LECTURE 13

Room 3-442

Tuesday, March 19, 2:30pm - 4:30pm

Instructor: Gian Paolo Beretta

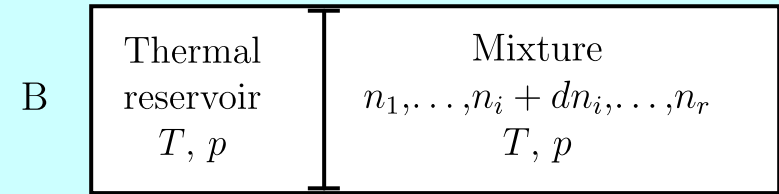
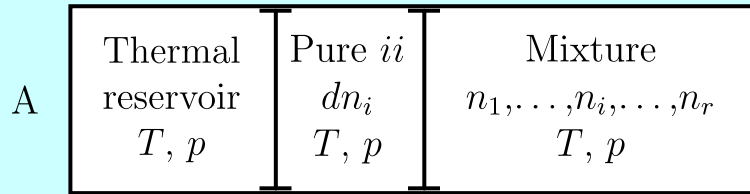
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Room 3-351d

**Stable-equilibrium properties of
MIXTURES
(within the simple-system model)**

**Partial properties
Gibbs-Dalton ideal mixtures
Mixing and separation
Osmotic pressure and blue energy
Stratification**

Partial properties from properties of isothermobaric mixing



Enthalpy of Tp -mixing*

$$\Delta h_i^{\text{mix}} = \frac{H(T, p, n_1, \dots, n_i + dn_i, \dots, n_r) - [H(T, p, n_1, \dots, n_i, \dots, n_r) + h_{ii}(T, p) dn_i]}{dn_i}$$

$$= \lim_{dn_i \rightarrow 0} \frac{H_B - H_A}{dn_i} = \left(\frac{\partial H}{\partial n_i} \right)_{T, p, \mathbf{n}'_i} - h_{ii}(T, p) = h_i(T, p, \mathbf{n}\mathbf{y}) - h_{ii}(T, p)$$

Similarly, we define the volume, energy, and entropy of Tp -mixing

$$\Delta v_i^{\text{mix}} = v_i(T, p, \mathbf{n}\mathbf{y}) - v_{ii}(T, p) \quad \Delta e_i^{\text{mix}} = e_i(T, p, \mathbf{n}\mathbf{y}) - e_{ii}(T, p) \quad \Delta s_i^{\text{mix}} = s_i(T, p, \mathbf{n}\mathbf{y}) - s_{ii}(T, p)$$

They are all measurable and allow the measurement of partial properties, once the pure-substance properties of the mixture components are known. as a result, we can write

$$\mu_i = h_i - T s_i = h_{ii} + \Delta h_i^{\text{mix}} - T s_{ii} - T \Delta s_i^{\text{mix}} = \mu_{ii}(T, p) + \Delta h_i^{\text{mix}} - T \Delta s_i^{\text{mix}} = \mu_{ii}(T, p_{ii})$$

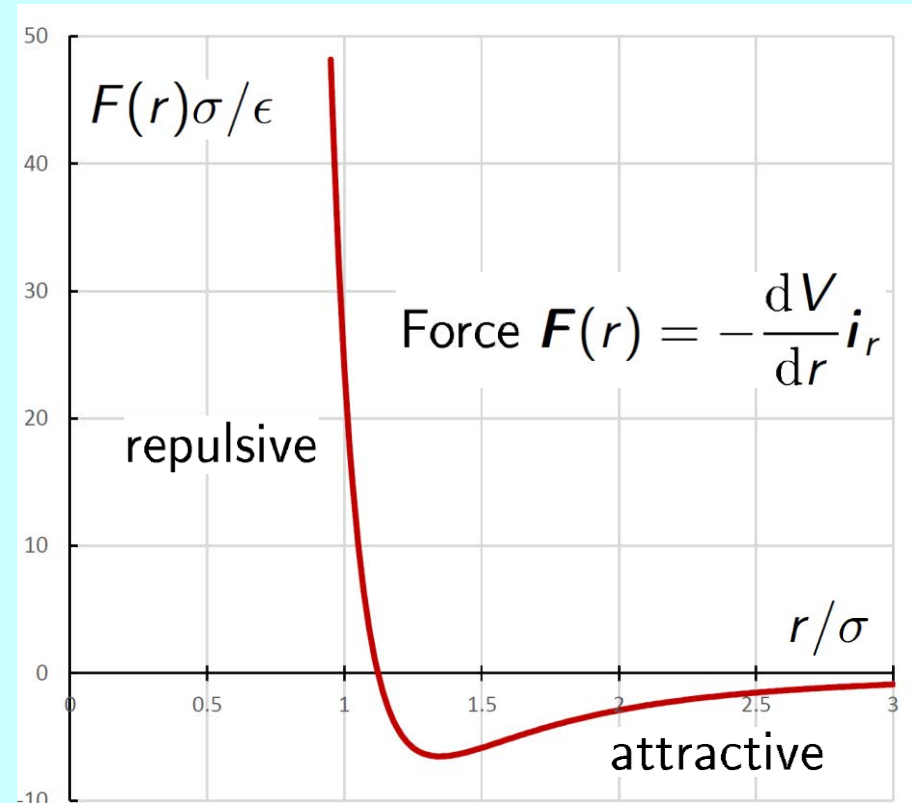
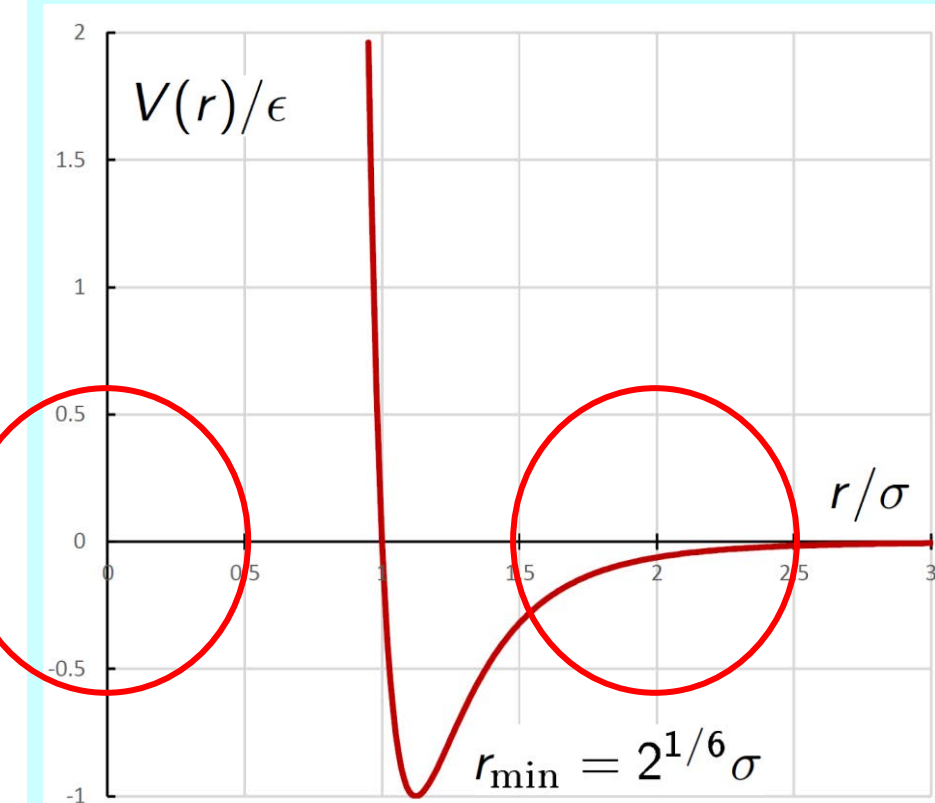
$$\mu_{ii}(T, p_{ii}) - \mu_{ii}(T, p) = \int_p^{p_{ii}} v_{ii}(T, p') dp' = \Delta h_i^{\text{mix}} - T \Delta s_i^{\text{mix}} = \begin{cases} RT \ln \frac{p_{ii}}{p} & \text{ideal gas} \\ -(p - p_{ii})v_{ii} & \text{ideal liquid or solid} \end{cases}$$

* Recall that the enthalpy is additive for systems in SES at the same pressure.

Lennard-Jones potential (model of intermolecular forces)

$$V(r) = 4\epsilon \left[\left(\frac{\sigma}{r} \right)^{12} - \left(\frac{\sigma}{r} \right)^6 \right]$$
$$= \epsilon \left[\left(\frac{r_{\min}}{r} \right)^{12} - 2 \left(\frac{r_{\min}}{r} \right)^6 \right]$$

$$F(r) = 24 \frac{\epsilon}{\sigma} \left(\frac{\sigma}{r} \right)^3 \left[2 \left(\frac{\sigma}{r} \right)^6 - 1 \right]$$
$$= 12 \frac{2^{2/3} \epsilon}{r_{\min}} \left(\frac{r_{\min}}{r} \right)^3 \left[\left(\frac{r_{\min}}{r} \right)^6 - 1 \right]$$



Ideal Gibbs-Dalton behavior

Ideal Gibbs-Dalton behavior is defined by

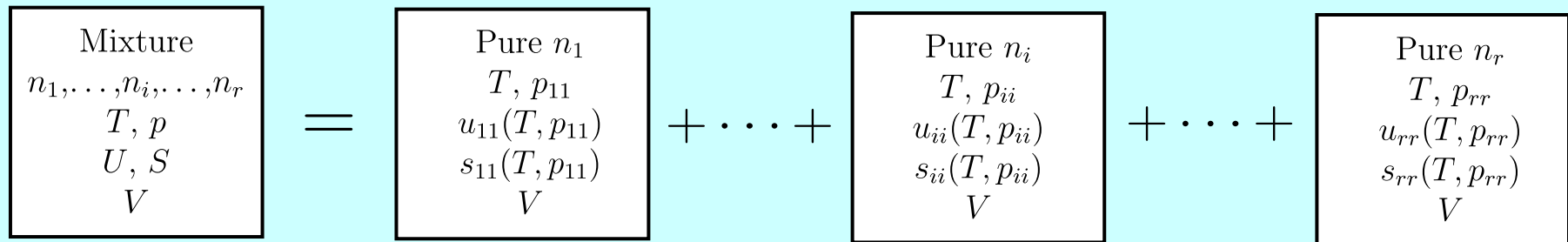
Assumption 1: $U = \sum_{i=1}^r n_i u_i(T, p, \mathbf{y}) = \sum_{i=1}^r n_i u_{ii}(T, p_{ii})$

Assumption 2: $S = \sum_{i=1}^r n_i s_i(T, p, \mathbf{y}) = \sum_{i=1}^r n_i s_{ii}(T, p_{ii})$

Assumption 3: $V = \sum_{i=1}^r n_i v_i(T, p, \mathbf{y}) = n_i v_{ii}(T, p_{ii}) \quad \forall i \quad (\text{no sum!})$

here the first equalities recall the relations in terms of partial properties.

The assumptions can be interpreted like this:



Ideal Gibbs-Dalton mixture of ideal gases

$$\forall i \text{ we have } v_{ii}(T, p_{ii}) = \frac{RT}{p_{ii}} \quad v_{ii}(T, p) = \frac{RT}{p} \quad V = n_i v_{ii}(T, p_{ii}) = n_i \frac{RT}{p_{ii}}$$

$$p_{ii} = n_i \frac{RT}{V} \quad p = \sum_i p_{ii} = \sum_i n_i \frac{RT}{V} = n \frac{RT}{V} \quad \frac{p_{ii}}{p} = \frac{n_i}{n} = y_i \quad \Rightarrow \quad p_{ii} = y_i p$$

$$\mu_i(T, p, \mathbf{y}) = \mu_{ii}(T, p_{ii}) = \mu_{ii}(T, p) + \int_p^{p_{ii}} \left(\frac{\partial \mu_{ii}}{\partial p} \right)_T dp' = \mu_{ii}(T, p) + \int_p^{p_{ii}} v_{ii}(T, p') dp'$$

$$= \mu_{ii}(T, p) + \int_p^{p_{ii}} \frac{RT}{p'} dp' = \mu_{ii}(T, p) + RT \ln \frac{p_{ii}}{p} = \mu_{ii}(T, p) + RT \ln y_i$$

Ideal Gibbs-Dalton mixtures of ideal gases

$$\forall i \text{ we have } v_{ii}(T, p_{ii}) = \frac{RT}{p_{ii}} \quad v_{ii}(T, p) = \frac{RT}{p} \quad V = n_i v_{ii}(T, p_{ii}) = n_i \frac{RT}{p_{ii}}$$

$$p_{ii} = n_i \frac{RT}{V} \quad p = \sum_i p_{ii} = \sum_i n_i \frac{RT}{V} = n \frac{RT}{V} \quad \frac{p_{ii}}{p} = \frac{n_i}{n} = y_i \quad \Rightarrow \quad p_{ii} = y_i p$$

$$\mu_i(T, p, \mathbf{y}) = \mu_{ii}(T, p_{ii}) = \mu_{ii}(T, p) + \int_p^{p_{ii}} \left(\frac{\partial \mu_{ii}}{\partial p} \right)_T dp' = \mu_{ii}(T, p) + \int_p^{p_{ii}} v_{ii}(T, p') dp'$$

$$= \mu_{ii}(T, p) + \int_p^{p_{ii}} \frac{RT}{p'} dp' = \mu_{ii}(T, p) + RT \ln \frac{p_{ii}}{p} = \mu_{ii}(T, p) + RT \ln y_i$$

$$s_i(T, p, \mathbf{y}) = - \left(\frac{\partial \mu_i}{\partial T} \right)_{p, \mathbf{n}} = s_{ii}(T, p) - R \ln y_i = s_{ii}(T, p_{ii}) \quad v_i(T, p, \mathbf{y}) = \left(\frac{\partial \mu_i}{\partial p} \right)_{T, \mathbf{n}} = v_{ii}(T, p) = \frac{RT}{p}$$

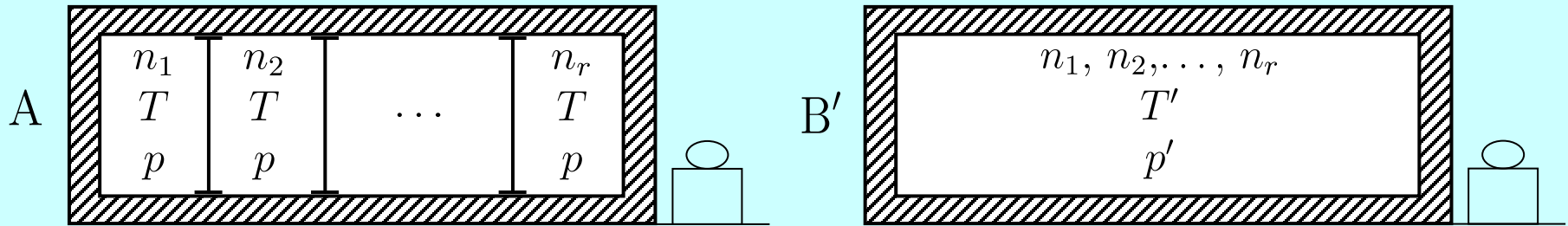
$$h_i(T, p, \mathbf{y}) = \left(\frac{\partial(\mu_i/T)}{\partial(1/T)} \right)_{p, \mathbf{n}} = h_{ii}(T) \quad u_i(T, p, \mathbf{y}) = T s_i - p v_i + \mu_i = u_{ii}(T)$$

Note also that $V = \sum_{i=1}^r V_i' = \sum_{i=1}^r n_i v_{ii}(T, p)$ (Amagat law of additive volumes)

where $V_i' = n_i v_{ii}(T, p)$ is called proper volume of i

Mixture $n_1, \dots, n_i, \dots, n_r$ T, p U, S V	=	<table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 25%; padding: 5px;">Pure n_1 T, p $u_{11}(T)$ $s_{11}(T, p)$ $V_1' = \frac{n_1 RT}{p}$</td> <td style="width: 25%; padding: 5px;">Pure n_2 T, p $u_{22}(T)$ $s_{22}(T, p)$ $V_2' = \frac{n_2 RT}{p}$</td> <td style="width: 25%; text-align: center; vertical-align: middle;">\dots</td> <td style="width: 25%; padding: 5px;">Pure n_r T, p $u_{rr}(T)$ $s_{rr}(T, p)$ $V_r' = \frac{n_r RT}{p}$</td> </tr> </table>	Pure n_1 T, p $u_{11}(T)$ $s_{11}(T, p)$ $V_1' = \frac{n_1 RT}{p}$	Pure n_2 T, p $u_{22}(T)$ $s_{22}(T, p)$ $V_2' = \frac{n_2 RT}{p}$	\dots	Pure n_r T, p $u_{rr}(T)$ $s_{rr}(T, p)$ $V_r' = \frac{n_r RT}{p}$
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Entropy of spontaneous mixing



Remove partitions allowing spontaneous mixing. Using energy, volume, and entropy additivity for A, and ideal G-D-mixture model for B',

$$U_A = \sum_i n_i u_{ii}(T) \quad V_A = \sum_i n_i v_{ii}(T, p) = \frac{nRT}{p} \quad S_A = \sum_i n_i s_{ii}(T, p)$$

$$U_{B'} = \sum_i n_i u_{ii}(T') \quad V_{B'} = \sum_i n_i v_{ii}(T', p') = \frac{nRT'}{p'} \quad S_{B'} = \sum_i n_i s_{ii}(T', p'_{ii})$$

Energy balance for the isolated system, $U_{B'} - U_A = 0$, recalling $du_{ii} = c_{v,ii}(T) dT$,

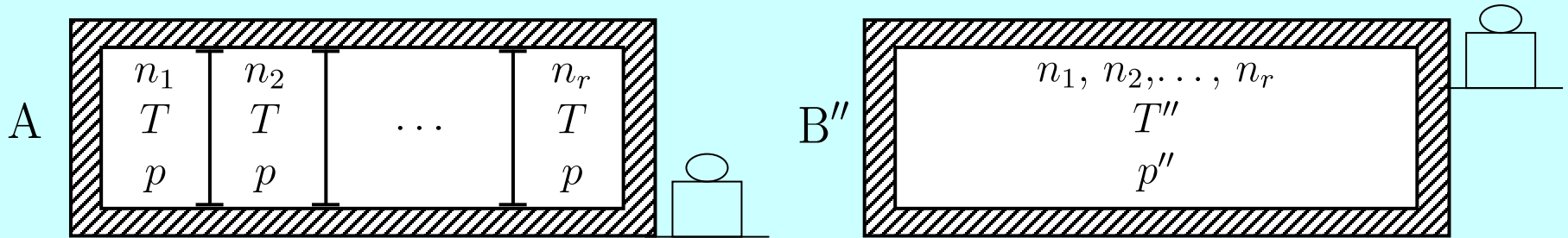
$$U_{B'} - U_A = \sum_i n_i [u_{ii}(T') - u_{ii}(T)] = \sum_i n_i \int_T^{T'} c_{v,ii}(\theta) d\theta = 0$$

Since $c_{v,ii}(T) > 0$ for any T , the integral can only be zero if $T' = T$. Therefore, the volume balance $V_{B'} = U_A$ yields $p' = p$.

Entropy balance for the isolated system, $S_{B'} - S_A = s_{\text{irr}}$, recalling $ds_{ii} = c_{p,ii}(T) dT/T - R dp/p$, so that $s_{ii}(T', p'_{ii}) = s_{ii}(T', p) - R \ln y_i$, yields (for $T' = T$ and $p' = p$)

$$S_{\text{irr}} = S_{B'} - S_A = \sum_i n_i [s_{ii}(T', p'_{ii}) - s_{ii}(T, p)] = \sum_i n_i \Delta s_i^{\text{mix}} = \sum_i n_i [-R \ln y_i] = -nR \sum_i y_i \ln y_i \geq 0$$

Extracting the adiabatic availability of mixing



Do the mixing with a reversible weight process. Using energy, volume, and entropy additivity for A, and ideal G-D-mixture model for B'',

$$U_A = \sum_i n_i u_{ii}(T) \quad V_A = \sum_i n_i v_{ii}(T, p) = \frac{nRT}{p} \quad S_A = \sum_i n_i s_{ii}(T, p)$$

$$U_{B''} = \sum_i n_i u_{ii}(T'') \quad V_{B''} = \sum_i n_i v_{ii}(T'', p'') = \frac{nRT''}{p''} \quad S_{B''} = \sum_i n_i s_{ii}(T'', p''_{ii})$$

The volume balance $V_{B''} = V_A$ imposes $p''/T'' = p/T$. Thus, recalling $p''_{ii} = y_i p''$, assuming constant specific heats, defining $c_{v,mix} = \sum_i y_i c_{v,ii}$, and using

$$s_{ii}\left(T'', p''_{ii} = y_i \frac{T''}{T} p\right) - s_{ii}(T, p) = c_{p,ii} \ln \frac{T''}{T} - R \ln \left(y_i \frac{T''}{T}\right) = c_{v,ii} \ln \frac{T''}{T} - R \ln y_i$$

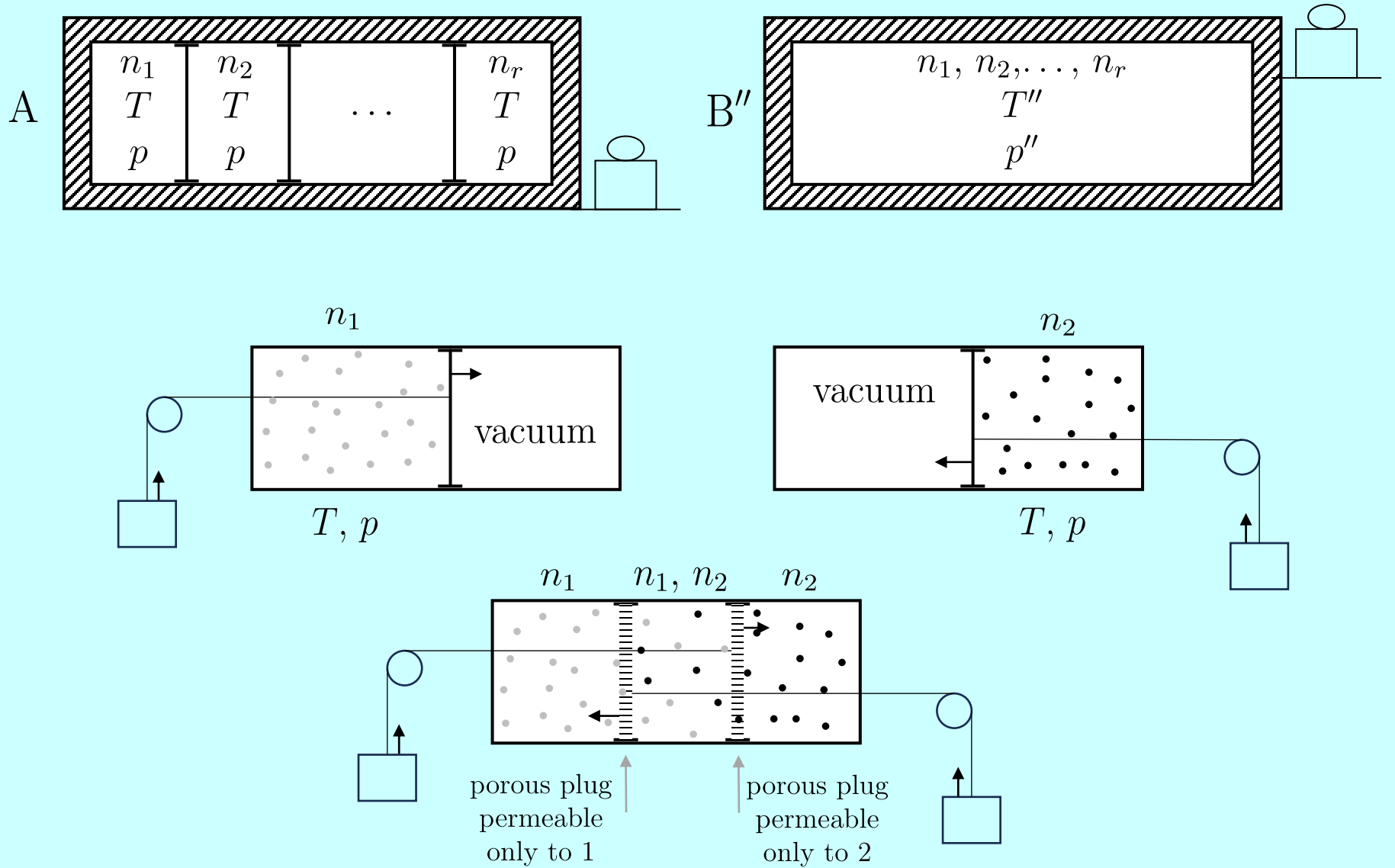
the entropy balance for the reversible weight process, $S_{B''} - S_A = 0$, becomes

$$0 = S_{B''} - S_A = \sum_i n_i [s_{ii}(T'', p''_{ii}) - s_{ii}(T, p)] = \sum_i n_i [c_{v,ii} \ln \frac{T''}{T} - R \ln y_i] = n [c_{v,mix} \ln \frac{T''}{T} - R \sum_i y_i \ln y_i]$$

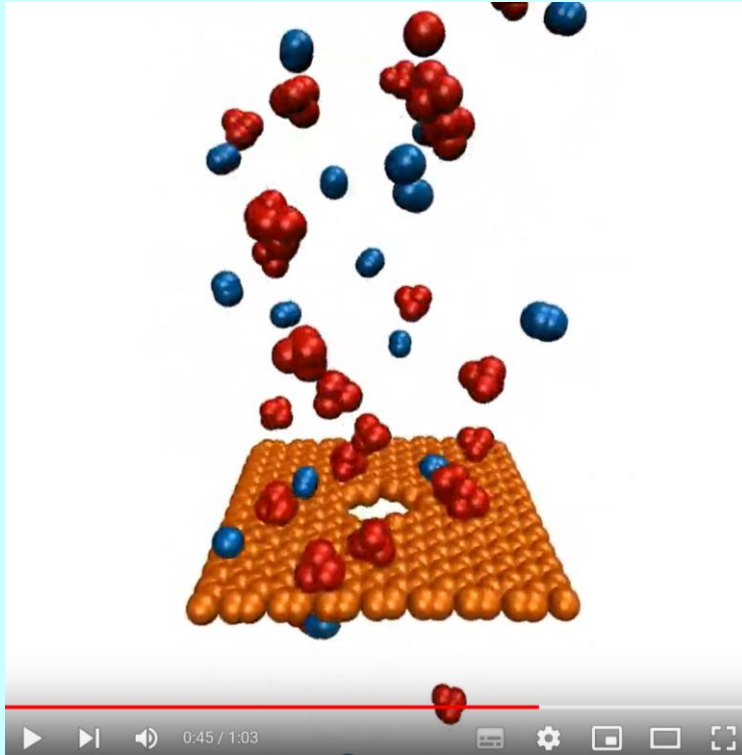
and yields $T'' = T \exp\left(\frac{R}{c_{v,mix}} \sum_i y_i \ln y_i\right)$ (clearly $T'' < T$). Therefore, the energy balance for the weight process, $U_{B''} - U_A = -W_{rev}^{\rightarrow}$, yields

$$W_{rev}^{\rightarrow} = U_A - U_{B''} = \sum_i n_i [u_{ii}(T'') - u_{ii}(T)] = n c_{v,mix} (T - T'') = n c_{v,mix} T \left[1 - \exp\left(\frac{R}{c_{v,mix}} \sum_i y_i \ln y_i\right)\right]$$

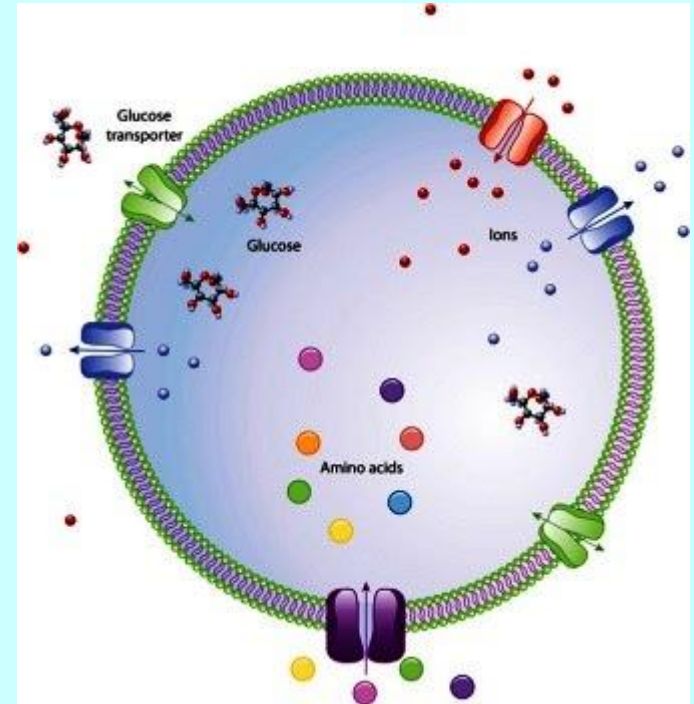
Extracting the adiabatic availability of mixing



Semipermeable (passive transport) vs selective (active transport) Membranes

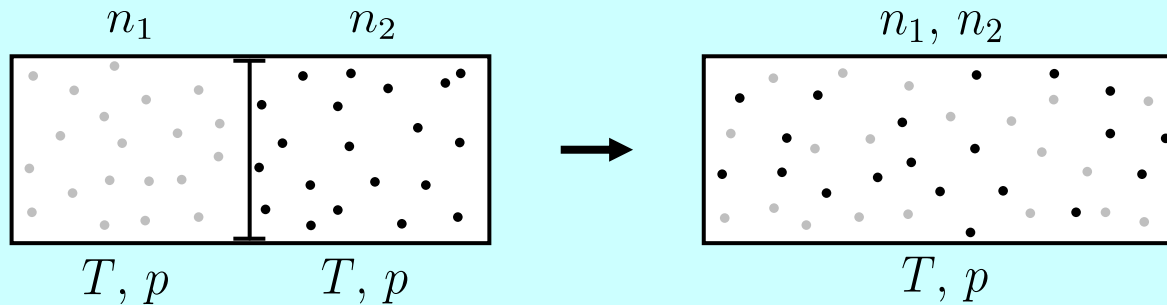


<https://www.youtube.com/watch?v=hxFj8qgejek>



<https://www.youtube.com/watch?v=XbnhmrNNe-w>

Entropy of spontaneous mixing (**Gibbs paradox** resolved)

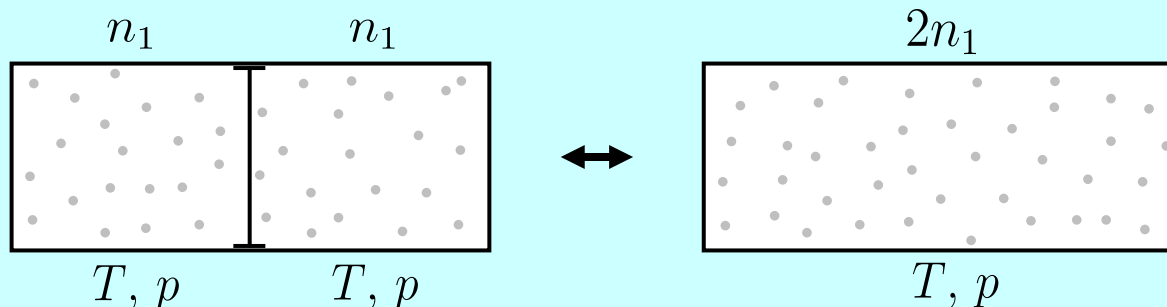


$$y_1 = \frac{n_1}{n} \quad y_2 = 1 - y_1 = \frac{n_2}{n} \quad n = n_1 + n_2$$

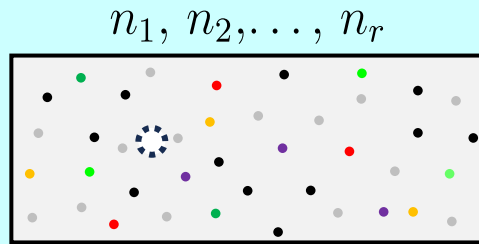
$$S_{\text{irr}} = -nR \sum_i y_i \ln y_i = -nR [y_1 \ln y_1 + (1 - y_1) \ln(1 - y_1)] \geq 0$$

For example, for $n_1 = n_2 = n/2$, $y_1 = y_2 = 1/2$, $S_{\text{irr}} = nR \ln 2$.

However, if particles 1 and 2 are identical, removing (and adding) partitions, within the simple system model, changes no SES property. So, in this case $S_{\text{irr}} = 0$.



Shannon information entropy



	probability	surprise	normalized
	p	$-\ln(p)$	$-\ln(p)/-\ln(0.5)$
	1	0.0	0
N2	0.79	0.2	0.3
50%	0.5	0.7	1
O2	0.21	1.6	2
Ar	0.009	4.7	7
CO2	0.0005	7.6	11

Suppose we have r possible types of particles, with molecular masses M_1, \dots, M_r .

The probability to observe a particle of type i is $p_i = \frac{n_i}{n} = y_i$. Note: $p_i \geq 0$ and $\sum_{i=1}^r p_i = 1$

The mean or expected value of the mass is $\langle M \rangle = \sum_{i=1}^r p_i M_i$.

The degree of uncertainty, about which M_i will be observed next, is measured by the

Shannon information entropy $S_I = - \sum_{i=1}^r p_i \ln p_i$

Example. Suppose we do not know the y_i 's, but we have measured $\langle M \rangle$.

What is the **least biased assignment of y_i 's** compatible with the measured $\langle M \rangle$?

Maximize $-\sum_{i=1}^r p_i \ln p_i$ subject to the constraints $\sum_{i=1}^r p_i = 1$ and $\sum_{i=1}^r p_i M_i = \langle M \rangle$.

With the method of Lagrange multipliers obtain $p_i = \frac{\exp(-\lambda_M M_i)}{\sum_i \exp(-\lambda_M M_i)}$.

Inserting these in the constraint, $\sum_{i=1}^r M_i \exp(-\lambda_M M_i) / Z = \langle M \rangle$, yields $\lambda_M = \lambda_M(\langle M \rangle)$.

Ideal gas equation of state for a single particle in a box

For a system consisting of a single particle ($n = 1$ molecule = $1/N_{\text{Av}}$ mol) of mass m with no internal structure and only translational degrees of freedom, confined in a parallelepiped-shaped container with sides ℓ_1, ℓ_2, ℓ_3 (and volume $V = \ell_1\ell_2\ell_3$), the quantized energy levels are

$$\epsilon_{j_1, j_2, j_3} = \epsilon_{j_1} + \epsilon_{j_2} + \epsilon_{j_3} = \frac{h^2}{8m} \left(\frac{j_1^2}{\ell_1^2} + \frac{j_2^2}{\ell_2^2} + \frac{j_3^2}{\ell_3^2} \right) \quad \text{where } j_1, j_2, j_3 = 1, 2, 3, \dots, \infty$$

The maximum entropy principle implies that the SES probability distribution $\{p_{j_1, j_2, j_3}\}$ is given by the solution of the constrained maximization problem

$$\max_{\{p_{j_1, j_2, j_3}\}} S = -nR \sum_{\mathbf{j}} p_{j_1, j_2, j_3} \ln p_{j_1, j_2, j_3} \quad \text{subject to} \quad \sum_{\mathbf{j}} p_{j_1, j_2, j_3} = 1 \quad \text{and} \quad \sum_{\mathbf{j}} p_{j_1, j_2, j_3} \epsilon_{j_1, j_2, j_3} = E$$

where $\sum_{\mathbf{j}} = \sum_{j_1=1}^{\infty} \sum_{j_2=1}^{\infty} \sum_{j_3=1}^{\infty}$. Assigning the Lagrange multiplier $1/k_{\text{B}}T$ to the energy constraint, and noting that $nR = R/N_{\text{Av}} = k_{\text{B}}$ (the Boltzmann constant), we find the SES distribution

$$p_{j_1, j_2, j_3} = \frac{\exp(-\epsilon_{j_1, j_2, j_3}/k_{\text{B}}T)}{\mathcal{Q}} = p_{j_1} p_{j_2} p_{j_3} = \frac{\exp(-\epsilon_{j_1}/k_{\text{B}}T)}{\mathcal{Q}_1} \frac{\exp(-\epsilon_{j_2}/k_{\text{B}}T)}{\mathcal{Q}_2} \frac{\exp(-\epsilon_{j_3}/k_{\text{B}}T)}{\mathcal{Q}_3}$$

where we define the partition functions $\mathcal{Q} = \mathcal{Q}_1 \mathcal{Q}_2 \mathcal{Q}_3$, $\mathcal{Q}_i = \sum_{j_i=1}^{\infty} \exp(-\epsilon_{j_i}/k_{\text{B}}T)$. It is easy to verify that the probabilities and all the properties can be obtained from derivatives of the \mathcal{Q}_i 's and that $T = (\partial E / \partial S)_{\ell_1, \ell_2, \ell_3}$, i.e., the Lagrange multiplier indeed represents the temperature

$$E = k_{\text{B}}T^2 \left(\frac{\partial \ln \mathcal{Q}}{\partial T} \right)_{\ell} = E_1 + E_2 + E_3 \quad E_i = \sum_{j_i} p_{j_i} \epsilon_{j_i} = k_{\text{B}}T^2 \left(\frac{\partial \ln \mathcal{Q}_i}{\partial T} \right)_{\ell_i} \quad p_{j_i} = -k_{\text{B}}T \left(\frac{\partial \ln \mathcal{Q}_i}{\partial \epsilon_{j_i}} \right)_T$$

$$S = k_{\text{B}} \left(\frac{\partial T \ln \mathcal{Q}}{\partial T} \right)_{\ell} = S_1 + S_2 + S_3 \quad S_i = -k_{\text{B}} \sum_{j_i} p_{j_i} \ln p_{j_i} = k_{\text{B}} \left(\frac{\partial T \ln \mathcal{Q}_i}{\partial T} \right)_{\ell_i} = \frac{E_i}{T} + k_{\text{B}} \ln \mathcal{Q}_i$$

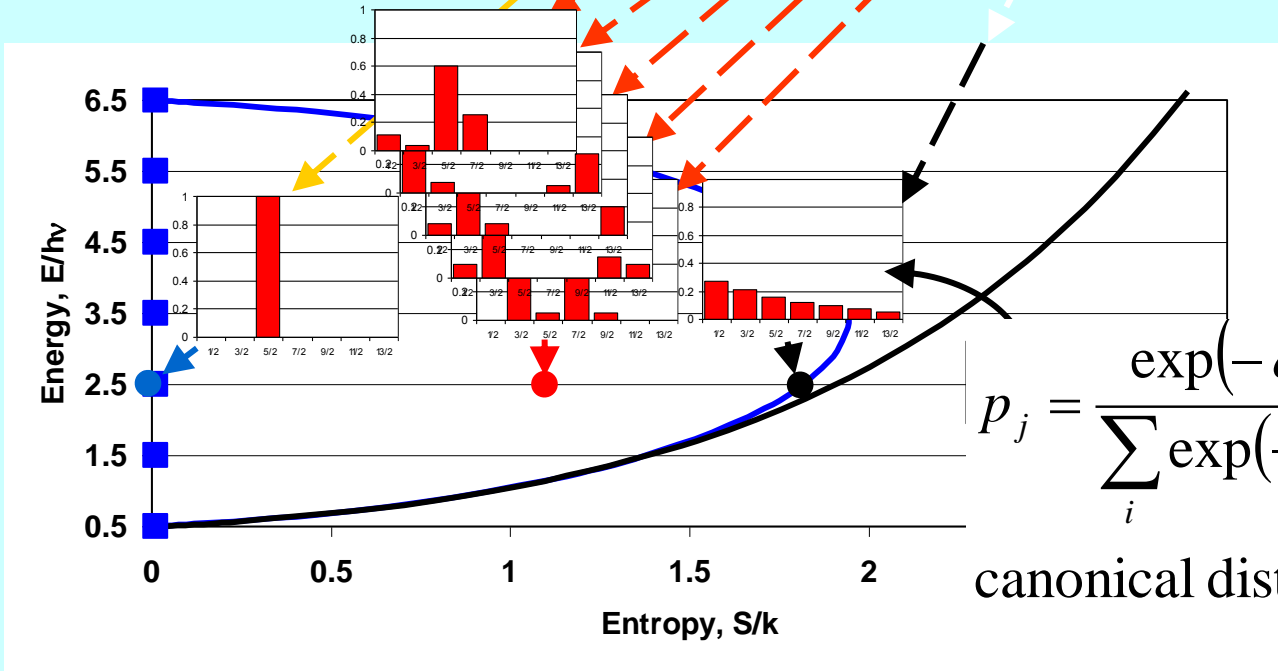
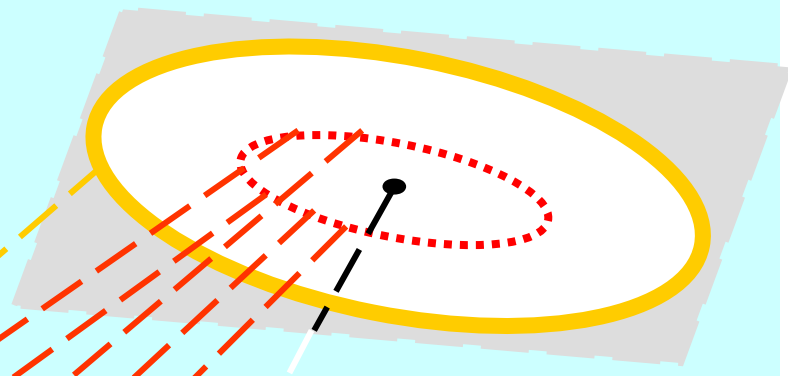
Upper bounded vs unbounded energy spectrum

energy levels $e_j \quad j = 1, 2, \dots, N$

$E = \sum_j p_j e_j$ energy (assuming $\rho\mathbf{H} = \mathbf{H}\rho$)

probability p_j measures the degree of involvement of level e_j in sharing the energy load

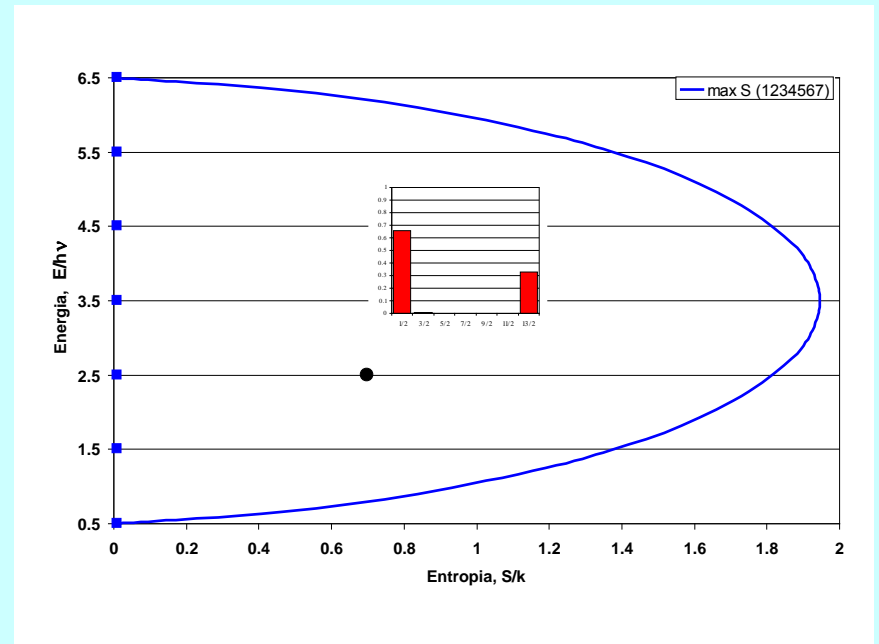
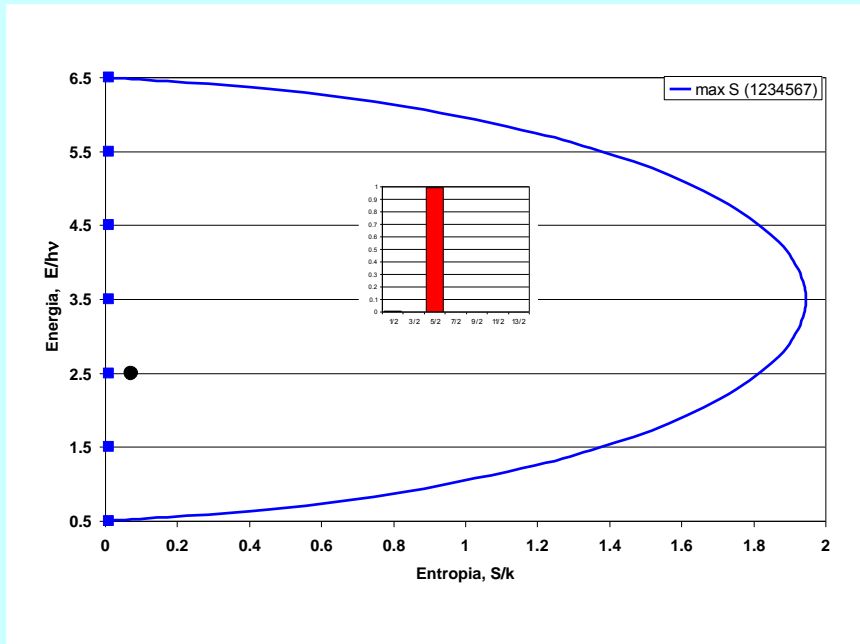
$S = -k_B \sum_j p_j \ln p_j$ entropy measures the global degree of sharing the energy load among levels



$$p_j = \frac{\exp(-e_j/k_B T)}{\sum_i \exp(-e_i/k_B T)}$$

canonical distribution

Steepest entropy ascent equation of motion models the time evolution of the state (probability distribution) towards SES



Ideal gas equation of state for a single particle in a box

For $i = 1, 2, 3$,
$$\epsilon_{j_i} = \frac{h^2}{8m} \left(\frac{j_i^2}{\ell_i^2} \right) \quad \mathcal{Q}_i = \sum_{j_i=1}^{\infty} \exp \left(- \frac{\epsilon_{j_i}}{k_B T} \right) = \sum_{j_i=1}^{\infty} \exp \left(- \frac{h^2 j_i^2}{8mk_B T \ell_i^2} \right)$$

$$\mathcal{Q}_i = \mathcal{Q}_i(T, \ell_i) \quad d \ln \mathcal{Q}_i = \frac{E_i}{k_B T^2} dT + \frac{2E_i}{k_B T} \frac{d\ell_i}{\ell_i} \quad \left(\frac{\partial \ln \mathcal{Q}_i}{\partial T} \right)_{\ell_i} = \frac{E_i}{k_B T^2} \quad \left(\frac{\partial \ln \mathcal{Q}_i}{\partial \ln \ell_i} \right)_T = \frac{2E_i}{k_B T}$$

$$S_i = \frac{E_i}{T} + k_B \ln \mathcal{Q}_i \quad dS_i = \frac{1}{T} dE_i + \frac{2E_i}{T} \frac{d\ell_i}{\ell_i} \quad dE_i = T dS_i - 2E_i \frac{d\ell_i}{\ell_i} = T dS_i - \pi_i V \frac{d\ell_i}{\ell_i}$$

where we defined the directional pressure
$$\pi_i = - \left(\frac{\partial E_i}{\partial V} \right)_{S, \ell'_i} = - \frac{1}{V} \left(\frac{\partial E_i}{\partial \ln \ell_i} \right)_{S, \ell'_i} = \frac{2E_i}{V}$$

representing the change in energy ∂E_i at constant S_i due to a change in the volume $V = \ell_1 \ell_2 \ell_3$ obtained by changing only ℓ_i , so that $\partial V/V = \partial \ell_i/\ell_i$. We finally obtain,

$$E = E_1 + E_2 + E_3 = (\pi_1 + \pi_2 + \pi_3) \frac{V}{2} \quad dE = T dS - \pi_1 V \frac{d\ell_1}{\ell_1} - \pi_2 V \frac{d\ell_2}{\ell_2} - \pi_3 V \frac{d\ell_3}{\ell_3}$$

For 'practical' values of m , ℓ_1 , ℓ_2 , ℓ_3 , and T , the values of $h^2/8mk_B T \ell_i^2$ are much smaller than one, and therefore the sum in \mathcal{Q}_i can be approximated by an integral,

$$\mathcal{Q}_i = \sum_{j_i=0}^{\infty} e^{-\frac{h^2}{8mk_B T} \frac{j_i^2}{\ell_i^2}} \approx \int_0^{\infty} e^{-\frac{h^2}{8mk_B T} \frac{x^2}{\ell_i^2}} dx = \left(\frac{2\pi mk_B T \ell_i^2}{h^2} \right)^{1/2} \Rightarrow \mathcal{Q} = \mathcal{Q}_1 \mathcal{Q}_2 \mathcal{Q}_3 \approx \left(\frac{2\pi mk_B T V^{2/3}}{h^2} \right)^{3/2}$$

Consequently, the details of the shape of the container become irrelevant, given the same volume V , as the separate dependence of \mathcal{Q} on the individual ℓ_i 's disappears.

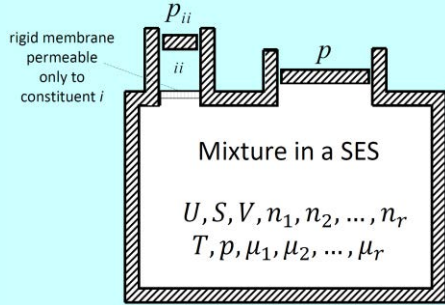
$$\left(\frac{\partial \ln \mathcal{Q}_i}{\partial T} \right)_{\ell_i} = \frac{1}{2T} \quad E_i = \frac{1}{2} k_B T \quad \pi_i = \frac{k_B T}{V} \quad S_i = \frac{1}{2} k_B + \frac{1}{2} k_B \ln \frac{2\pi mk_B T \ell_i^2}{h^2}$$

$$E = \frac{3}{2} k_B T \quad dE = T dS - k_B T \left(\frac{d\ell_1}{\ell_1} + \frac{d\ell_2}{\ell_2} + \frac{d\ell_3}{\ell_3} \right) = dE = T dS - k_B T \frac{dV}{V} \Rightarrow p = \frac{k_B T}{V}$$

$$S = \frac{3}{2} k_B \left(1 + \ln \frac{2\pi mk_B T V^{2/3}}{h^2} \right) \quad \text{Recall: valid at large } T \text{ for given } V \text{ so that } TV^{2/3} \gg \frac{h^2}{8mk_B}$$

Are mixture properties determined by the pure-substance properties of its constituents?

Ideal solution behavior



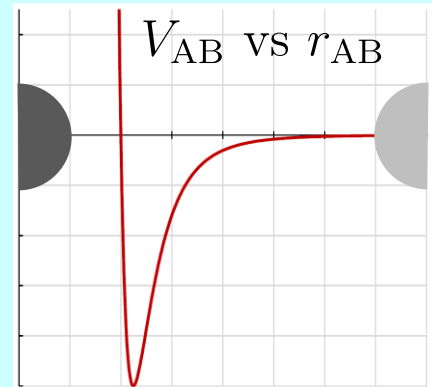
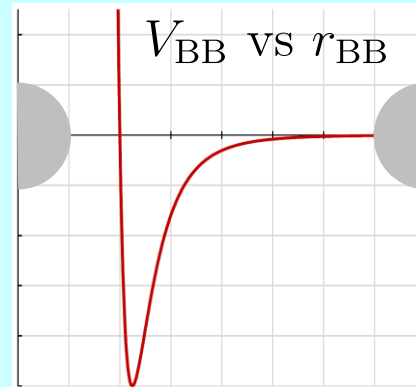
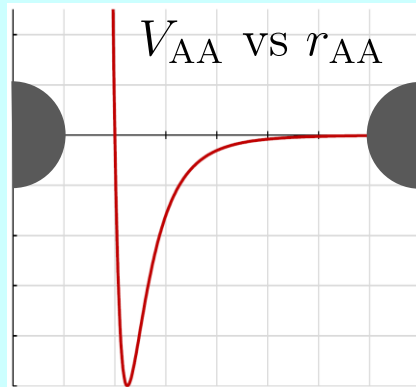
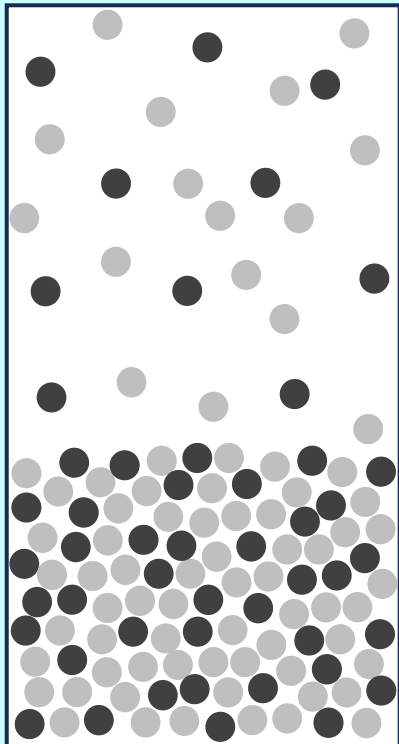
Ideal solution behavior is defined by

Assumption 1: $\Delta h_i^{\text{mix}} = 0 \quad \forall i$

Assumption 2: $\Delta s_i^{\text{mix}} = -R \ln y_i \quad \forall i$

Assumption 3: $\Delta v_i^{\text{mix}} = 0 \quad \forall i$

Ideal GD mixture of ideal gases: $\langle V_{AA} \rangle \approx \langle V_{BB} \rangle \approx \langle V_{AB} \rangle \approx 0$
 because $\langle r_{AA} \rangle \gg r_{\text{min}}^{\text{AA}}$, $\langle r_{BB} \rangle \gg r_{\text{min}}^{\text{BB}}$, $\langle r_{AB} \rangle \gg r_{\text{min}}^{\text{AB}}$.



Ideal solution: $\langle V_{AA} \rangle \approx \langle V_{BB} \rangle \approx \langle V_{AB} \rangle$.

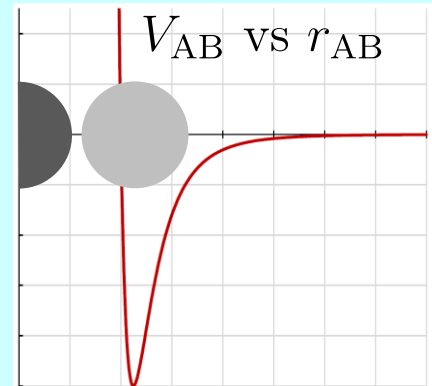
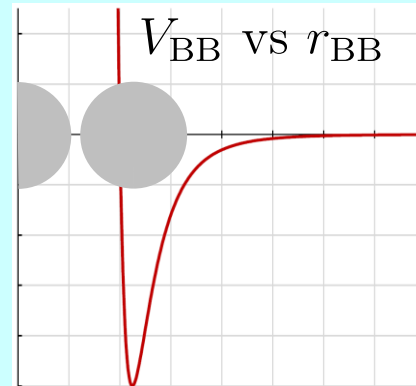
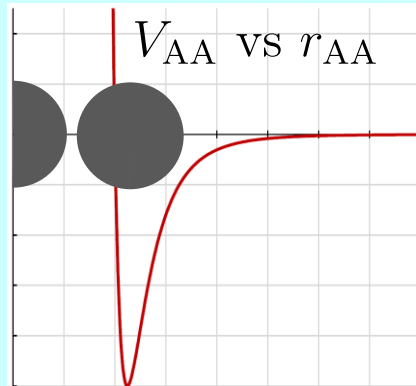


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