2.43 ADVANCED THERMODYNAMICS

Spring Term 2024 LECTURE 16

Room 3-442 Friday, April 5, 11:00am - 1:00pm

Instructor: Gian Paolo Beretta <u>beretta@mit.edu</u> Room 3-351d Liquid-vapor equilibria in ideal mixtures

Raoult's law principle of distillation boiling point elevation freezing point depression Henry's law

Raoult's law

Assume an ideal mixture and/or solution behavior of component 1 in both phases a and b $\mu_{1a}(T, p, y_{1a}) = \mu_{11a}(T, p) + RT \ln y_{1a} = \mu_{11a}(T, p_{\text{sat},11}^{ab}(T)) + \int_{p_{\text{sat},11}^{ab}(T)}^{p} v_{11a}(T, \tilde{p}) \,\mathrm{d}\tilde{p} + RT \ln y_{1a}$ $\mu_{1b}(T, p, y_{1b}) = \mu_{11b}(T, p) + RT \ln y_{1b} = \mu_{11b}(T, p_{\text{sat},11}^{ab}(T)) + \int_{p_{\text{out}-11}^{ab}(T)}^{p} v_{11b}(T, \tilde{p}) \,\mathrm{d}\tilde{p} + RT \ln y_{1b}$ Recall that $\mu_{11a}(T, p_{\text{sat},11}^{ab}(T)) = \mu_{11b}(T, p_{\text{sat},11}^{ab}(T))$ by definition of $p_{\text{sat},11}^{ab}(T)$, so at MSE, $\mu_{1a} = \mu_{1b}$: $RT \ln(y_{1a}/y_{1b}) = \int_{p_{aat}^{ab}}^{p} \left[v_{11b}(T,\tilde{p}) - v_{11a}(T,\tilde{p}) \right] d\tilde{p}$ (1)**Liquid-vapor equilibrium**, a = g, b = f, with p $p_{\mathrm{sat},11}^{\mathrm{fg}}(T)$ 2 non-volatile solute, 3 non-condensable gas $v_{11g}(T, \tilde{p}) = RT/\tilde{p}, v_{11f} = \text{const:}$ (1+3)g $RT \ln(y_{1g}/y_{1f}) = [p - p_{\text{sat.11}}^{\text{fg}}(T)]v_{11f} - RT \ln[p/p_{\text{sat.11}}^{\text{fg}}(T)]$ 11g and noting that $[p - p_{\text{sat.11}}^{\text{fg}}(T)]v_{11\text{f}}/RT \ll 1$ 11f (1+2)f $y_{1g}/y_{1f} \approx p/p_{\text{sat,}11}^{\text{fg}}(T)$ or, equivalently, $p_{11g} = y_{1g} p = y_{1f} p_{sat.11}^{fg}(T)$ Raoult's law, 1887 p $p_{\mathrm{sat},11}^{\mathrm{Jf}}(T)$ **Liquid-solid equilibrium**, a = f, b = j, with **2 non-freezing solute** so that $y_{1i} = 1$ (1+2)f11f $v_{11f} = \text{const}, v_{11j} = \text{const}, v_{11}^{jf} = v_{11f} - v_{11j}$ $RT \ln(y_{1\rm f}/y_{1\rm j}) = [p - p_{\rm sat.11}^{\rm jf}(T)](v_{11\rm j} - v_{11\rm f})$ or 11j 11j $y_{1f} = \exp\left(-[p - p_{\text{sat},11}^{\text{jf}}(T)]v_{11}^{\text{jf}}/RT\right)$

Raoult's law



Principle of distillation



Freezing point depression and boiling point elevation



© 2024 Gian Paolo Beretta @MIT 2.43 Advanced Thermodynamics

Non-ideal mixtures

Duhem-Margules relations excess mixing properties

Margules, van Laar, Redlich-Kister, Wilson, and Prausnitz models

Henry's law

Lennard-Jones binary mixture model

Experimental measurement of SES properties of mixtures: Mixture properties from the partial properties

So, in general (i.e., for small and large systems) we proved

$$S = \sum_{i=1}^{r} n_{i} s_{i} - \left(\frac{\partial Eu}{\partial T}\right)_{p,n} \xrightarrow{n \text{ large}} S = \sum_{i=1}^{r} n_{i} s_{i}$$

$$V = \sum_{i=1}^{r} n_{i} v_{i} + \left(\frac{\partial Eu}{\partial p}\right)_{T,n} \xrightarrow{n \text{ large}} V = \sum_{i=1}^{r} n_{i} v_{i}$$

$$\sum_{i=1}^{r} n_{i} \mu_{i,j} = -\left(\frac{\partial Eu}{\partial n_{j}}\right)_{T,p,n'_{j}} \xrightarrow{n \text{ large}} \sum_{i=1}^{r} n_{i} \mu_{i,j} = 0$$
Duhem-Margules relation

Moreover, recalling the definitions of Eu and partial properties

$$Eu = E - TS + pV - \boldsymbol{\mu} \cdot \boldsymbol{n} = F + pV - \boldsymbol{\mu} \cdot \boldsymbol{n} = G - \boldsymbol{\mu} \cdot \boldsymbol{n} = H - TS - \boldsymbol{\mu} \cdot \boldsymbol{n}$$
$$\mu_i = e_i - Ts_i + pv_i = f_i + pv_i = g_i = h_i - Ts_i$$

we also find the following relations, which justify calling partial properties that way:

$$E = \sum_{i=1}^{r} n_{i} e_{i} + Eu - T\left(\frac{\partial Eu}{\partial T}\right)_{p,n} - p\left(\frac{\partial Eu}{\partial p}\right)_{T,n} \xrightarrow{n \text{ large}} E = \sum_{i=1}^{r} n_{i} e_{i}$$

$$F = \sum_{i=1}^{r} n_{i} f_{i} + Eu - p\left(\frac{\partial Eu}{\partial p}\right)_{T,n} \xrightarrow{n \text{ large}} F = \sum_{i=1}^{r} n_{i} f_{i}$$

$$G = \sum_{i=1}^{r} n_{i} g_{i} + Eu = \sum_{i=1}^{r} n_{i} \mu_{i} + Eu \xrightarrow{n \text{ large}} G = \sum_{i=1}^{r} n_{i} g_{i} = \sum_{i=1}^{r} n_{i} \mu_{i}$$

$$H = \sum_{i=1}^{r} n_{i} h_{i} + Eu - T\left(\frac{\partial Eu}{\partial T}\right)_{p,n} \xrightarrow{n \text{ large}} H = \sum_{i=1}^{r} n_{i} h_{i}$$

© 2024 Gian Paolo Beretta @MIT 2.43 Advanced Thermodynamics

Modeling non-ideal SES behavior of mixtures:

Duhem-Margules relation, excess mixing properties

Recall, we defined
$$\mu_{i,j}(T, p, n\boldsymbol{y}) = \left(\frac{\partial \mu_i}{\partial n_j}\right)_{T, p, \boldsymbol{n}'_j} = \left(\frac{\partial^2 G}{\partial n_j \partial n_i}\right)_{T, p, \boldsymbol{n}'_{ij}} = \left(\frac{\partial \mu_j}{\partial n_i}\right)_{T, p, \boldsymbol{n}'_{ij}} = \mu_{j,i}(T, p, n\boldsymbol{y})$$

and proved that Eu = 0 (i.e., the Euler relation) implies the Duhem-Margules relations (which are valid, therefore, within the simple-system model, i.e., for large n)

$$\sum_{i=1}^{r} n_i \,\mu_{i,j} = 0 \quad \forall j \qquad \Rightarrow \qquad \frac{\partial(\mu_1, \dots, \mu_r)}{\partial(n_1, \dots, n_r)} = \det \operatorname{Hess}(G)|_{T,p} = 0$$

Indeed, the Duhem-Margules relations can be viewed as a homogeneous system of linear equations in the n_i 's, which has nontrivial solutions only if the determinant of the matrix of coefficients is zero. Define $\mu_i^{\text{id}} = \mu_{ii}(T, p) + RT \ln y_i$ and $\mu_i^{\text{ex}} = \Delta h_i^{\text{mix}} - T\Delta s_i^{\text{ex}}$ so that $\mu_i(T, p, \boldsymbol{y}) = \mu_i^{\text{id}}(T, p, y_i) + \mu_i^{\text{ex}}(T, p, \boldsymbol{y})$ where $\Delta s_i^{\text{ex}} = \Delta s_i^{\text{mix}} - \Delta s_i^{\text{id}}$ is the excess mixing entropy of component *i* and $\Delta s_i^{\text{id}} = -R \ln y_i$. Since $\frac{\partial \ln y_i}{\partial n_j} = \frac{\delta_{ij}}{n_i} - \frac{1}{n}$ so that $\sum_{i=1}^{'} n_i \frac{\partial \ln y_i}{\partial n_j} = \sum_{i=1}^{'} \delta_{ij} - \sum_{i=1}^{'} \frac{n_i}{n} = 1 - 1 = 0$ we have $\sum_{i=1}^{'} n_i \mu_{i,j}^{id} = 0$. So, modeling non-ideal behavior requires that $\sum_{i=1}^{r} n_i \mu_{i,j}^{\text{ex}}(T, p, \boldsymbol{y}) = \sum_{i=1}^{r} n_i \frac{\partial \left(\Delta h_i^{\text{mix}} - T\Delta s_i^{\text{ex}}\right)}{\partial n_i} = 0 \quad \forall j$ Defining $G^{id} = \sum_{i=1}^{r} n_i \mu_i^{id} = \sum_{i=1}^{r} n_i (\mu_{ii}(T, p) + RT \ln y_i)$ and $G^{ex} = \sum_{i=1}^{r} n_i \mu_i^{ex} = \sum_{i=1}^{r} n_i (\Delta h_i^{mix} - T\Delta s_i^{ex})$ we can write $\mu_i^{\text{id}} = \left(\frac{\partial G^{\text{id}}}{\partial n_i}\right)_{T,n,n'}$ $\mu_i^{\text{ex}} = \left(\frac{\partial G^{\text{ex}}}{\partial n_i}\right)_{T,n,n'}$ $\frac{\partial(\mu_1^{\text{ex}},\dots,\mu_r^{\text{ex}})}{\partial(n_1,\dots,n_r)} = \det \operatorname{Hess}(G^{\text{ex}})|_{T,p} = 0$

Modeling non-ideal SES behavior of mixtures:

simple and complex model relations for binary mixtures

 $q^{1d} = y_1 q_{11}(T, p) + y_2 q_{22}(T, p) + RT (y_1 \ln y_1 + y_2 \ln y_2)$ ideal mixture $\frac{\mu_1^{\text{id}} = g_{11}(T, p) + RT \ln y_1}{g_{\text{M1}}^{\text{ex}} = A(T, p) y_1 y_2} \qquad \frac{\mu_2^{\text{id}} = g_{22}(T, p) + RT \ln y_2}{\text{Margules, one parameter (1895)}}$ $\mu_{1.M1}^{\text{ex}} = A y_2^2 \qquad \mu_{2.M1}^{\text{ex}} = A y_1^2$ $\overline{q_{M2}^{\text{ex}}} = [A(T, p) y_2 + B(T, p) y_1] y_1 y_2 \qquad \text{Margules, two parameters (1895)}$ $\mu_{1,M2}^{\text{ex}} = y_2^2 \left[(2B - A) + 2(A - B)y_2 \right] \qquad \mu_{2,M2}^{\text{ex}} = y_1^2 \left[(2A - B) + 2(B - A)y_1 \right]$ $g_{\rm vL}^{\rm ex} = (y_1/B(T,p) + y_2/A(T,p))^{-1} y_1 y_2$ van Laar (1913) $\frac{\mu_{1,\text{vL}}^{\text{ex}} = A \left(1 + A y_1 / B y_2\right)^{-2}}{g_{\text{RK}}^{\text{ex}} = y_1 y_2 \sum_{k=0}^{K} A_k(T, p) (y_1 - y_2)^k} \quad (\text{Guggenheim (1937), Redlich-Kister (1948), Scatchard (1949)})$ $\frac{g_{\rm W}^{\rm ex} = -C(T,p) \left\{ y_1 \ln \left[y_1 + y_2 \frac{v_{22}}{v_{11}} \exp \left(\frac{\epsilon_{11} - \epsilon_{12}}{RT} \right) \right] + y_2 \ln \left[y_2 + y_1 \frac{v_{11}}{v_{22}} \exp \left(\frac{\epsilon_{22} - \epsilon_{12}}{RT} \right) \right] \right\}$ Wilson (1964) $\overline{g_{NRTL}^{ex}} =$ Non-Random Two-Liquid model, Renon-**Prausnitz** (1968) $g_{\mathbf{UNIQUAC}}^{\mathrm{ex}} = \mathrm{UNIversal} \mathrm{QUAsi-Chemical} \mathrm{model}, \mathrm{Abrams-Prausnitz} (1975)$ UNIquac Functional-group Activity Coefficient model, Fredenslund-Jones-Prausnitz (1975) $g_{\mathbf{UNIFAC}}^{\mathrm{ex}} =$ Recall $\Delta h_i^{\text{mix}} = \left(\frac{\partial(\mu_i^{\text{ex}}/T)}{\partial(1/T)}\right)_{n,u} = \mu_i^{\text{ex}} \left[1 + \left(\frac{\partial \ln \mu_i^{\text{ex}}}{\partial \ln T}\right)_{n,u}\right] \qquad \Delta s_i^{\text{mix,ex}} = \left(\frac{\partial(\mu_i^{\text{ex}})}{\partial T}\right)_{n,u}$

For example, assuming A and B constant in M1, M2, and vL yields $\Delta h_i^{\text{mix}} = \mu_i^{\text{ex}}$ and $\Delta s_i^{\text{mix,ex}} = 0$ so that For M1: $A = \Delta h_{1,\text{M1}}^{\text{mix}}|_{y_2=1} = \Delta h_{2,\text{M1}}^{\text{mix}}|_{y_1=1}$ For M2 and vL: $A = \Delta h_{1,\text{M2,vL}}^{\text{mix}}|_{y_2=1}$ $B = \Delta h_{2,\text{M2,vL}}^{\text{mix}}|_{y_1=1}$

Modeling non-ideal SES behavior of mixtures:

simple and complex model relations for binary mixtures



Alternative traditional ways to represent chemical potentials: Activities and activity coefficients

When the mixture is in a condensed form of aggregation, it is more convenient to define the *activity of constituent i in the mixture* as the dimensionless function $a_i(T, p, y_1, y_2, \ldots, y_r; p_0, y_{10}, y_{20}, \ldots, y_{r0})$ given by the relation

$$a_i(T, p, \boldsymbol{y}; p_o, \boldsymbol{y}_o) = \exp\left[\frac{\mu_i(T, p, \boldsymbol{y}) - \mu_i(T, p_o, \boldsymbol{y}_o)}{RT}\right]$$

Because for ideal behavior $a_i = y_i$, the activity coefficient of constituent i

$$\gamma_i = \frac{a_i(T, p, y; p_o, y_o)}{y_i}$$

is an indicator of departure from ideal behavior. In terms of the activity and the activity coefficient, the chemical potential may be expressed as

$$\begin{split} \mu_i &= \mu_{io} + RT \ln a_i \\ &= \mu_{io} + RT \ln y_i + RT \ln \gamma_i \end{split}$$

where again $\mu_{io} = \mu_i(T, p_o, y_o)$.

The choices of the reference values p_0 and y_0 depend on the application.

Equations and figures adapted from pp.515-516 of Gyftopoulos, Beretta, Thermodynamics. Foundations and applications, Dover, 2005

Alternative traditional ways to represent chemical potentials: **Fugacities and fugacity coefficients**

we define the fugacity of constituent i in the mixture, $\pi_i(T, p, y_1, y_2, \dots, y_r; p_0, y_{10}, y_{20}, \dots, y_{r0})$, by the relation

$$\pi_i(T, p, \boldsymbol{y}; p_o, \boldsymbol{y}_o) = \pi_i(T, p_o, \boldsymbol{y}_o; p_o, \boldsymbol{y}_o) \exp\left[\frac{\mu_i(T, p, \boldsymbol{y}) - \mu_i(T, p_o, \boldsymbol{y}_o)}{RT}\right]$$

together with the condition

 $\pi_i(T, p, y; p_o, y_o) = y_i p$ in the limits of high T and low p

that is, in the limits in which the system behaves as an ideal-gas mixture, where p_0 is a reference pressure and y_0 a reference composition.

The dimensionless ratio

$$\phi_i = \frac{\pi_i(T, p, \boldsymbol{y}; p_o, \boldsymbol{y}_o)}{y_i p}$$

is called the *fugacity coefficient of constituent i*, and indicates the departure from ideal mixture behavior.

When the mixture is in a gaseous form of aggregation, p_0 and y_{10} , y_{20} , ..., y_{r0} may be conveniently chosen to correspond to ideal-gas behavior of pure constituent *i*, that is, $y_{i0} = 1$ and p_0 sufficiently low so that $\mu_{i0} = \mu_{ii}(T, p_0)$, $\pi_{i0} = p_0$, and

$$\mu_i = \mu_{ii}(T, p_o) + RT \ln \frac{y_i p}{p_o} + RT \ln \phi_i$$

Equations and figures adapted from pp.515-516 of Gyftopoulos, Beretta, Thermodynamics. Foundations and applications, Dover, 2005

Alternative traditional ways to represent chemical potentials: activities for the Margules and van Laar models

Margules, 1 parameter

$$\ln a_1' = \ln y_1 + \frac{A}{RT} (1 - y_1)^2$$
$$\ln a_2' = \ln(1 - y_1) + \frac{A}{RT} (y_1)^2$$

van Laar

$$\ln a_1' = \ln y_1 + \frac{A/RT}{\left[1 + Ay_1/B(1 - y_1)\right]^2}$$
$$\ln a_2' = \ln(1 - y_1) + \frac{B/RT}{\left[1 + B(1 - y_1)/Ay_1\right]^2}$$



Margules, 2 parameters

$$\ln a_1' = \ln y_1 + \frac{2B - A}{RT} (1 - y_1)^2 + \frac{2(A - B)}{RT} (1 - y_1)^3$$
$$\ln a_2' = \ln(1 - y_1) + \frac{2A - B}{RT} (y_1)^2 + \frac{2(B - A)}{RT} (y_1)^3$$

Equations and figures adapted from pp.522-524 of Gyftopoulos, Beretta, Thermodynamics. Foundations and applications, Dover, 2005

Simple model of non-ideal liquid-vapor equilibrium:

liquid-vapor equilibrium modeled with the van Laar models

The conditions of mutual stable equilibrium of the two coexisting phases $y_{1g}p = a_{1f}p_{\text{sat},11}(T)$ approximated by the van Laar equations $y_{2g}p = a_{2f}p_{\text{sat},22}(T)$ $p = y_{\rm lf} \exp\left\{\frac{A/RT}{\left[1 + Ay_{\rm s}/B(1 - y_{\rm s})\right]^2}\right\} p_{\rm sat,11}(T) + (1 - y_{\rm lf}) \exp\left\{\frac{B/RT}{\left[1 + B(1 - y_{\rm s})/Ay_{\rm s})\right]^2}\right\} p_{\rm sat,22}(T)$ $\frac{1}{p} = \frac{y_{1g}}{p_{sat,11}(T)} \exp\left\{-\frac{A/RT}{\left[1 + Ay_{1}/B(1 - y_{1})\right]^{2}}\right\} + \frac{1 - y_{1g}}{p_{sat,22}(T)} \exp\left\{-\frac{B/RT}{\left[1 + B(1 - y_{1})/Ay_{1}\right]^{2}}\right\}$ 50 azeotrope $\leftarrow T \text{ vs. } y_{1f}$ $T = 45^{\circ}C$ nonideal p = 101.3 kPabubble line ideal, dew line 40 Van Laa bubble line ideal, bubble line A' = 1.8350 ideal. p (kPa) 05 T (K) Van Laar A' = 1.8345 R' = 1.4bubble line nonideal 20 azeotrope 340 - p vs. y 1e 335 10 0.9 0.8 1.0 0.5 0.6 0.7 0.0 0.1 0.2 0.3 0.4 0.4 0.5 0.6 0.0 0.1 0.2 0.3 0.7 0.8 0.9 1.0 *y*₁ *y*₁

Equations and figures adapted from pp.522-525 of Gyftopoulos, Beretta, Thermodynamics. Foundations and applications, Dover, 2005

Simple model of non-ideal liquid-vapor equilibrium:

liquid-vapor equilibrium modeled with the van Laar models



Equations and figures adapted from pp.522-525 of Gyftopoulos, Beretta, Thermodynamics. Foundations and applications, Dover, 2005

© 2024 Gian Paolo Beretta @MIT 2.43 Advanced Thermodynamics

MD and MC modeling of non-ideal SES mixture behavior: Lennard-Jones binary mixture



For $\xi = 1$ mixture behavior is close to ideal (Raoult's law). For $\xi > 1$ ($\xi < 1$) attraction (repulsion) between unlike particles is stronger than between like particles, and the mixture tends to form a high-boiling (lowboiling) azeotrope, i.e., higher (lower) pressures than for ideal behavior are required to stabilize the vapor-liquid equilibrium. Very low values of ξ result in liquid-liquid miscibility gap.



Liquid-vapor equilibria in non-ideal mixtures

stability and miscibility gap liquid-liquid spinodal decomposition

Liquid-vapor equilibria for non-ideal binary mixtures



Figure 26.1 On a $T - p - y_1$ diagram, two-phase states are represented by points in a region delimited by two saturation surfaces. The diagrams in Figures 26.1 to 26.5 are based on C. E. Wales, *Chem. Eng.*, May 27, p. 120, June 24, p. 111, July 22, p. 141, Aug. 19, p. 167, Sept. 16, p. 187 (1983).

Figure from p.470 of Gyftopoulos, Beretta, Thermodynamics. Foundations and Applications, Dover, 2005

Image Credits

Slide 5:

Figure 27.8 from the book *Thermodynamics: Foundations and Applications* © Dover Publications. All rights reserved. This content is excluded from our Creative Commons license. For more information, see https://ocw.mit.edu/help/faq-fair-use.

Slides 12–16:

Equations and figures from the book *Thermodynamics: Foundations and Applications* © Dover Publications. All rights reserved. This content is excluded from our Creative Commons license. For more information, see https://ocw.mit.edu/help/faq-fair-use.

Slide 17:

Four p-x phase diagrams of binary Lennard-Jones mixtures courtesy of <u>TimeStep89</u> on Wikipedia. License CC BY.

Slide 19:

Figure 26.1 from the book Thermodynamics: Foundations and Applications courtesy of Elias P. Gyftopoulos and Gian Paolo Beretta.

2.43 Advanced Thermodynamics Spring 2024

For information about citing these materials or our Terms of Use, visit: <u>https://ocw.mit.edu/terms</u>.