

## Engine Heat Transfer

1. Impact of heat transfer on engine operation
2. Heat transfer environment
3. Energy flow in an engine
4. Engine heat transfer
  - Fundamentals
  - Spark-ignition engine heat transfer
  - Diesel engine heat transfer
5. Component temperature and heat flow

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## Engine Heat Transfer

- Heat transfer is a parasitic process that contributes to a loss in fuel conversion efficiency
- The process is a “surface” effect
- Relative importance reduces with:
  - Larger engine displacement
  - Higher load

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## Engine Heat Transfer: Impact

- **Efficiency and Power:** Heat transfer in the inlet decrease volumetric efficiency. In the cylinder, heat losses to the wall is a loss of availability.
- **Exhaust temperature:** Heat losses to exhaust influence the turbocharger performance. In- cylinder and exhaust system heat transfer has impact on catalyst light up.
- **Friction:** Heat transfer governs liner, piston/ ring, and oil temperatures. It also affects piston and bore distortion. All of these effects influence friction. Thermal loading determined fan, oil and water cooler capacities and pumping power.
- **Component design:** The operating temperatures of critical engine components affects their durability; e.g. via mechanical stress, lubricant behavior

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## Engine Heat Transfer: Impact

- **Mixture preparation in SI engines:** Heat transfer to the fuel significantly affect fuel evaporation and cold start calibration
- **Cold start of diesel engines:** The compression ratio of diesel engines are often governed by cold start requirement
- **SI engine octane requirement:** Heat transfer influences inlet mixture temperature, chamber, cylinder head, liner, piston and valve temperatures, and therefore end-gas temperatures, which affect knock. Heat transfer also affects build up of in-cylinder deposit which affects knock.

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## Engine heat transfer environment

- Gas temperature: ~300 – 3000°K
- Heat flux to wall:  $\dot{Q}/A < 0$  (during intake) to 10 MW/m<sup>2</sup>
- Materials limit:
  - Cast iron ~ 400°C
  - Aluminum ~ 300°C
  - Liner (oil film) ~200°C
- Hottest components
  - Spark plug > Exhaust valve > Piston crown > Head
  - Liner is relatively cool because of limited exposure to burned gas
- Source
  - Hot burned gas
  - Radiation from particles in diesel engines

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## Energy flow diagram for an IC engine

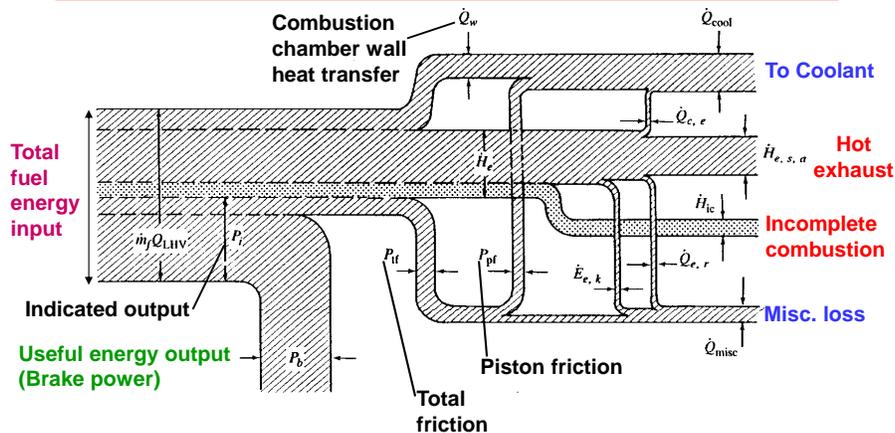


FIGURE 12-3

Energy flow diagram for IC engine.  $(\dot{m}_f Q_{LHV})$  = fuel flow rate  $\times$  lower heating value,  $\dot{Q}_w$  = heat-transfer rate to combustion chamber wall,  $\dot{H}_e$  = exhaust gas enthalpy flux,  $P_b$  = brake power,  $P_{tf}$  = total friction power,  $P_i$  = indicated power,  $P_{pf}$  = piston friction power,  $\dot{Q}_{cool}$  = heat-rejection rate to coolant,  $\dot{Q}_{e,e}$  = heat-transfer rate to coolant in exhaust ports,  $\dot{H}_{e,s,a}$  = exhaust sensible enthalpy flux entering atmosphere,  $\dot{H}_{e,ic}$  = exhaust chemical enthalpy flux due to incomplete combustion,  $\dot{Q}_{e,r}$  = heat flux radiated from exhaust system,  $\dot{E}_{e,k}$  = exhaust kinetic energy flux,  $\dot{Q}_{misc}$  = sum of remaining energy fluxes and transfers.

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## Energy flow distribution for SI and Diesel

TABLE 12.1

Energy balance for automotive engines at maximum power

	$P_b$	$\dot{Q}_{cool}$	$\dot{Q}_{misc}$	$\dot{H}_{e,lc}$	$\dot{m}h_{e,s}$
	(percentage of fuel heating value)				
SI engine	25–28	17–26	3–10	2–5	34–45
Diesel	34–38	16–35	2–6	1–2	22–35

Sources: From Khovakh,<sup>3</sup> Sitkei,<sup>4</sup> and Burke *et al.*<sup>5</sup>

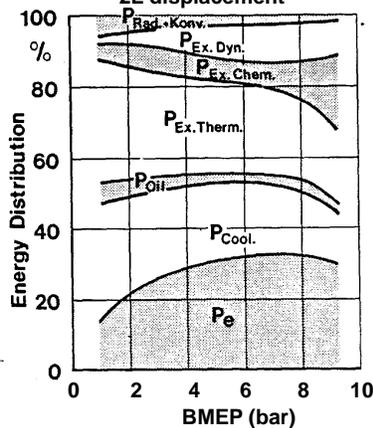
Update for modern engines:  
SI engine in the low 30's  
Diesel in the low 40's

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## Energy distribution in SI engine

2000 rpm, water cooled SI engine  
2L displacement



"Heat Balance of Modern Passenger Car SI Engines", Gruden, Kuper and Porsche, in *Heat and Mass Transfer in Gasoline and Diesel Engines*, ed. by Spalding and Afgan

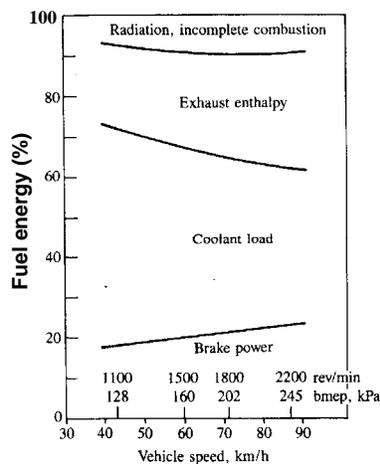
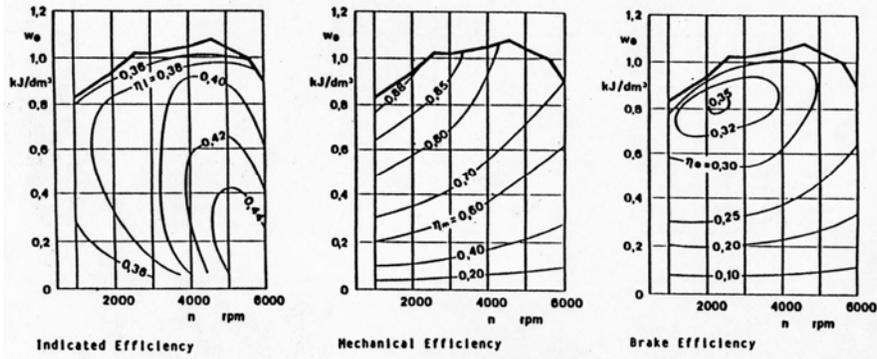


Fig. 12-4 SI engine energy distribution under road load condition, 6 cylinder engine; SAE Paper 770221, 1977

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## Efficiency of Passenger Car SI Engines



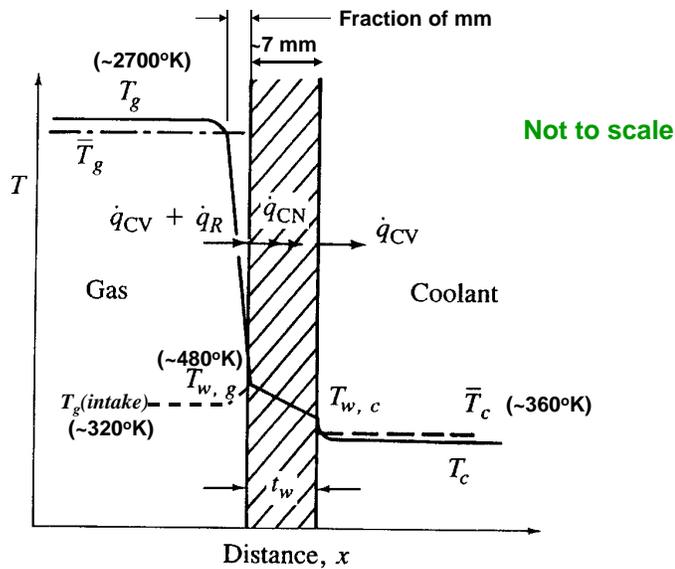
Source: D. Gruden, P.F., and F. Porsche AG. R & D Center Weissach, 1989.

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## Heat transfer process in engines

- **Areas where heat transfer is important**
  - Intake system: manifold, port, valves
  - In-cylinder: cylinder head, piston, valves, liner
  - Exhaust system: valves, port, manifold, exhaust pipe
  - Coolant system: head, block, radiator
  - Oil system: head, piston, crank, oil cooler, sump
- **Information of interest**
  - Heat transfer per unit time (rate)
  - Heat transfer per cycle (often normalized by fuel heating value)
  - Variation with time and location of heat flux (heat transfer rate per unit area)

**Schematic of temperature distribution and heat flow across the combustion chamber wall (Fig. 12-1)**



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**Combustion Chamber Heat Transfer**

**Turbulent convection: hot gas to wall**

$$\dot{Q} = Ah_g(\bar{T}_g - T_{wg})$$

**Conduction through wall**

$$\dot{Q} = A \frac{\kappa}{t_w} (T_{wg} - T_{wc})$$

**Turbulent convection: wall to coolant**

$$\dot{Q} = Ah_c(T_{wc} - \bar{T}_c)$$

**Overall heat transfer**

$$\dot{Q} = Ah(\bar{T}_g - \bar{T}_c)$$

**Overall thermal resistance: three resistance in series**

$$\frac{1}{h} = \frac{1}{h_g} + \frac{t_w}{\kappa} + \frac{1}{h_c}$$

(  $\kappa_{\text{alum}}$  ~180 W/m-k  
 $\kappa_{\text{cast iron}}$  ~ 60 W/m-k  
 $\kappa_{\text{stainless steel}}$  ~18 W/m-k)

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## Turbulent Convective Heat Transfer Correlation

**Approach:** Use Nusselt- Reynolds number correlations similar to those for turbulent pipe or flat plate flows.

e.g. In-cylinder:

$$\text{Nu} = \frac{hL}{\kappa} = a(\text{Re})^{0.8}$$

$h$  = Heat transfer coefficient

$L$  = Characteristic length (e.g. bore)

$\text{Re}$  = Reynolds number,  $\rho UL/\mu$

$U$  = Characteristic gas velocity

$\kappa$  = Gas thermal conductivity

$\mu$  = Gas viscosity

$\rho$  = Gas density

$a$  = Turbulent pipe flow correlation coefficient

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## Radiative Heat Transfer

- Important in diesels due to presence of hot radiating particles (particulate matters) in the flame
- Radiation from hot gas relatively small

$$\dot{Q}_{\text{rad}} = \varepsilon \cdot \sigma \cdot T_{\text{particle}}^4$$

$\sigma$  = Stefan Boltzman Constant ( $5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4$ )

$\varepsilon$  = Emissivity

where

$$T_{\text{cyl. ave}} < T_{\text{particle}} < T_{\text{max burned gas}}$$

- Radiation spectrum peaks at  $\lambda_{\text{max}}$   
 $\lambda_{\text{max}} T = \text{constant}$  ( $\lambda_{\text{max}} = 3 \mu\text{m}$  at 1000K)

Typically, in diesels:  $\bar{Q}_{\text{rad}} \approx 0.2 \bar{Q}_{\text{total}}$  (cycle cum)

$\dot{Q}_{\text{rad, max}} \approx 0.4 \dot{Q}_{\text{total, max}}$  (peak value)

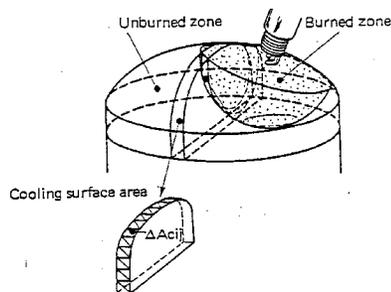
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## IC Engine heat transfer

- Heat transfer mostly from hot burned gas
  - That from unburned gas is relatively small
  - Flame geometry and charge motion/turbulence level affects heat transfer rate
- Order of Magnitude
  - SI engine peak heat flux ~ 1-3 MW/m<sup>2</sup>
  - Diesel engine peak heat flux ~ 10 MW/m<sup>2</sup>
- For SI engine at part load, a reduction in heat losses by 10% results in an improvement in fuel consumption by 3%
  - Effect substantially less at high load

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## SI Engine Heat Transfer



- Heat transfer dominated by that from the hot burned gas
- Burned gas wetted area determine by cylinder/ flame geometry
- Gas motion (swirl/ tumble) affects heat transfer coefficient

### Heat transfer

**Burned zone: sum over area "wetted" by burned gas**

$$\dot{Q}_b = \sum_i A_{ci,b} h_b (T_b - T_{w,i})$$

**Unburned zone: sum over area "wetted" by unburned gas**

$$\dot{Q}_u = \sum_i A_{ci,u} h_u (T_u - T_{w,i})$$

**Note: Burned zone heat flux >> unburned zone heat flux**

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## SI engine heat transfer environment

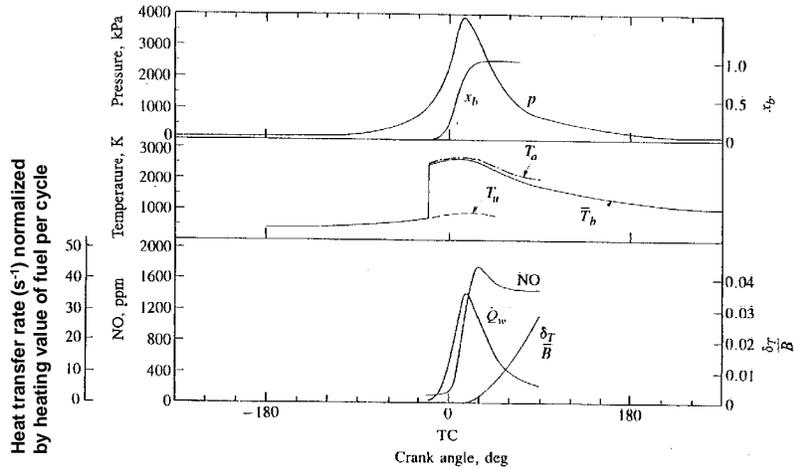
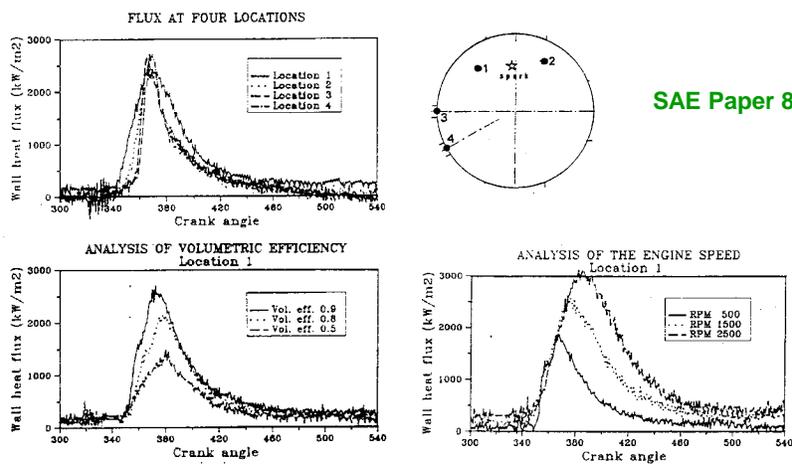


Fig. 14-9 5.7 L displacement, 8 cylinder engine at WOT, 2500 rpm; fuel equivalence ratio 1.1; GIMEP 918 kPa; specific fuel consumption 24 g/kW-hr.

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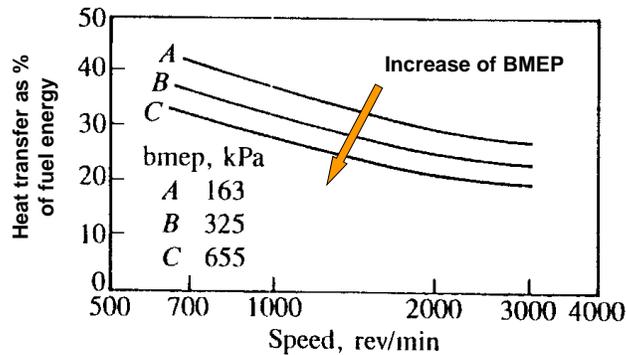
## SI engine heat flux



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## Heat transfer scaling



**Nu correlation: heat transfer rate**  $\propto \rho^{0.8} N^{0.8}$   
**Time available (per cycle)**  $\propto 1/N$   
**Fuel energy**  $\propto \rho$   
**BMEP**  $\propto \rho$

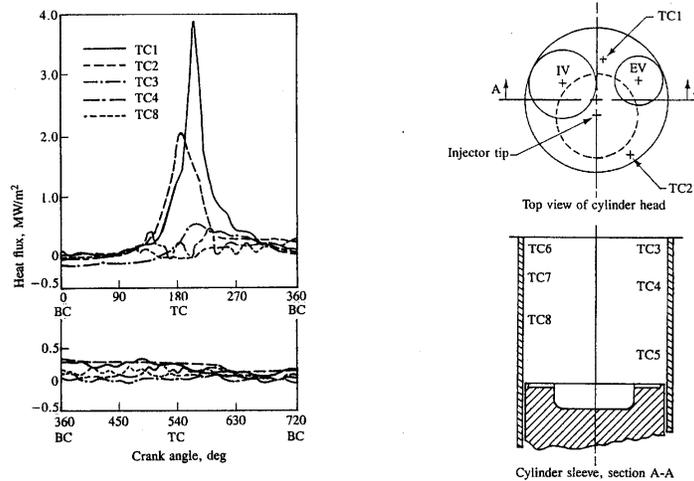
Fig. 12-25

**Thus Heat Transfer/Fuel energy**  $\propto \text{BMEP}^{-0.2} N^{-0.2}$

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## Diesel engine heat transfer

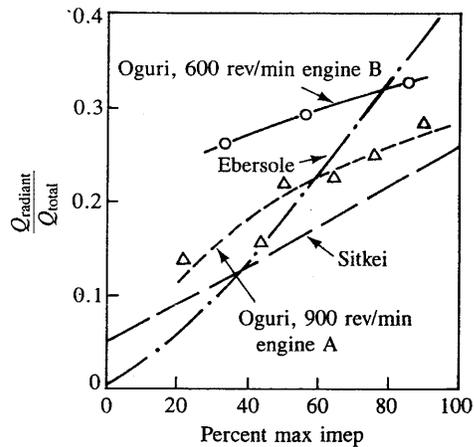


**Fig. 12-13 Measured surface heat fluxes at different locations in cylinder head and liner of naturally aspirated 4-stroke DI diesel engine. Bore=stroke=114mm; 2000 rpm; overall fuel equivalence ratio = 0.45.**

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## Diesel engine radiative heat transfer

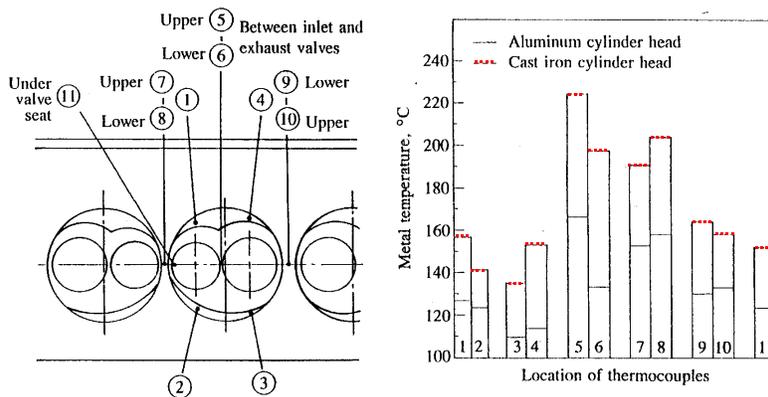


**Fig. 12-15**  
Radiant heat flux as fraction of total heat flux over the load range of several different diesel engines

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## Heat transfer effect on component temperatures Temperature distribution in head

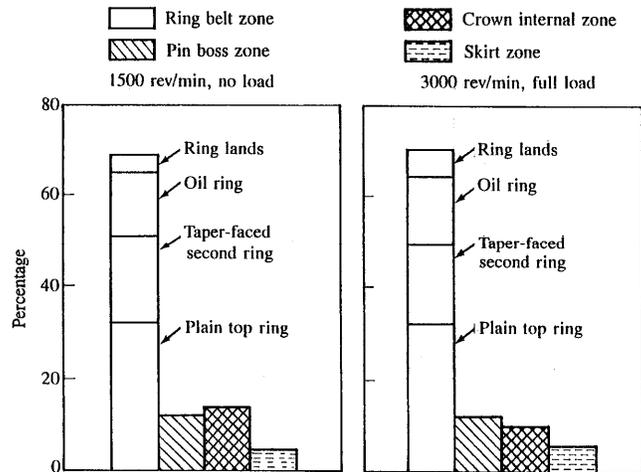


**Fig. 12-20** Variation of cylinder head temperature with measurement location in SI engine operating at 2000 rpm, WOT, with coolant water at 95°C and 2 atmosphere.

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## Heat transfer paths from piston

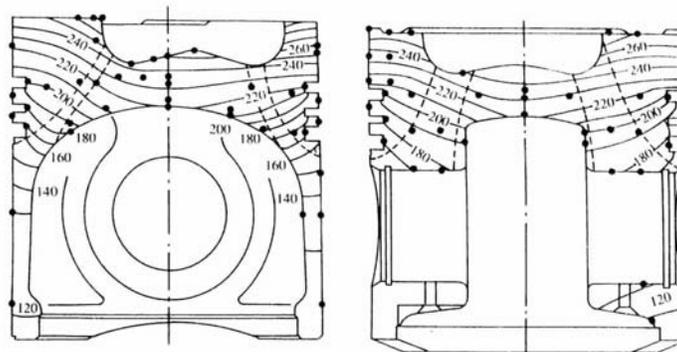


**Fig. 12-4** Heat outflow from various zones of piston as percentage of heat flow in from combustion chamber. High-speed DI diesel engine, 125 mm bore, 110 mm stroke, CR=17

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## Piston Temperature Distribution



**Figure 12-19**

Isothermal contours (solid lines) and heat flow paths (dashed lines) determined from measured temperature distribution in piston of high speed DI diesel engine. Bore 125 mm, stroke 110 mm,  $r_c=17$ , 3000 rev/min, and full load

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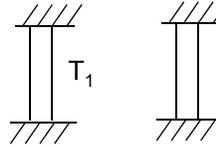
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# Thermal stress

Simple 1D example : column constrained at ends

Stress-strain relationship

$$\epsilon_x = [\sigma_x - \nu(\sigma_y + \sigma_z)]/E + \alpha(T_2 - T_1)$$



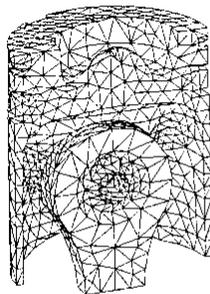
$T_2 > T_1$  induces compression stress

## REAL APPLICATION - FINITE ELEMENT ANALYSIS

- Complicated 3D geometry
- Solution to heat flow to get temperature distribution
- Compatibility condition for each element

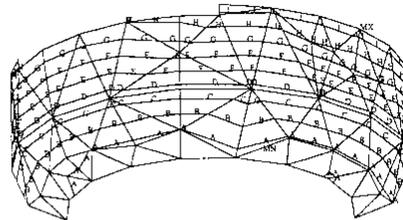
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### Example of Thermal Stress Analysis: Piston Design



Power Cylinder Design  
Variables and Their  
Effects on Piston  
Combustion Bowl Edge  
Stresses  
J. Castleman, SAE 932491

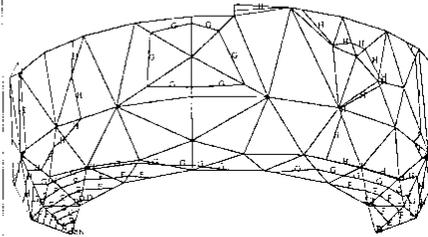
### Heat Transfer Analysis



```

ANR75 4 441
MAX 0 1503
13.55.08
PLAT NO 3
POST1 378155
STEP 4969
ITER 1
TEMP
SMN =297.253
SMX =356.124
YV =1
ZY =0.4
DIST=1.419
XZ =-2.154825
YF =-0.708471
ZF =2.751
VDP =2
PRECISE HIDDEN
A =712.2
B =-289.015
C =-20.849
D =-301.824
E =-511.479
F =-28.273
G =-531.548
H =-341.312
I =-351.157
    
```

### Thermal-Stress-Only Loading Structural Analysis



```

ANR75 4 441
MAX 6 1593
13.55.08
PLAT NO 5
POST1 378155
STEP 4969
ITER 1
TEMP
SMN =-8.84012
SMX =-1.602
YV =-1
ZY =0.4
DIST=1.419
XZ =-2.154825
YF =-0.708471
ZF =2.751
VDP =2
PRECISE HIDDEN
A =-74.008
B =-65.212
C =-26.127
D =-4.47422
E =-28.527
F =-39.631
G =-20.756
H =-11.611
I =-3.345
    
```

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## Heat Transfer Summary

1. Magnitude of heat transfer from the burned gas much greater than in any phase of cycle
2. Heat transfer is a significant performance loss and affects engine operation
  - Loss of available energy
  - Volumetric efficiency loss
  - Effect on knock in SI engine
  - Effect on mixture preparation in SI engine cold start
  - Effect on diesel engine cold start
3. Convective heat transfer depends on gas temperature, heat transfer coefficient, which depends on charge motion, and transfer area, which depends on flame/combustion chamber geometry
4. Radiative heat transfer is smaller than convective one, and it is only significant in diesel engines

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