

Using K_T and K_Q for design

*these notes are landscape
as plots are usually shown in
that mode*

we have seen in general the development of the Wageningen B series. The performance curves are available either in chart form or can be generated from polynomials:

▶ regression coeff. $Re=2 \cdot 10^6$

▶ polynomial representation

use in design

A typical design problem calls for designing a propeller that will provide the required thrust at a given speed of advance. These parameters result from applying thrust deduction and wake fraction to resistance and ship velocity respectively. Design will imply selecting a P/D from a B-series plot that will maximize open water efficiency.

For now we will arbitrarily pick a number of blades and expanded area ratio. Later we will address the criteria in their selection. Reviewing the non-dimensional forms of the parameters associated with thrust and speed:

$$K_T = \frac{T}{\rho \cdot n^2 \cdot D^4} \quad J = \frac{V_A}{n \cdot D}$$

we have independent variables n and D . Normally one of these is determined by other criteria, e.g. maximum diameter by hull form, or n by the propulsion train design, so we will look at two cases, one in which D is fixed - determine n , and the other where n is fixed determine D

case 1 given: V_A, T, D find n and P/D for maximum efficiency

only thing unknown is n , eliminate ... from ratio of K_T and J

$$\frac{K_t}{J^2} = \frac{T}{\rho \cdot n^2 \cdot D^4} \cdot \frac{n^2 \cdot D^2}{V_A^2} = \frac{T}{\rho \cdot D^2 \cdot V_A^2}$$

this says that propeller (full scale and model) must match this ratio which is a constant determined by T, V_A, D and ρ

$$K_t \text{ over } J \text{ sq} := \frac{T}{\rho \cdot D^2 \cdot V_A^2}$$

we can plot a curve of K_T vs J^2 and determine the points (values of J) for which K_T vs J for a given P/D match.

the design point for a particular propeller (B.n.nn) i.e. n is determined from the value of J that satisfies: $K_t(J) = \text{constant} \cdot J^2$

for example, let $K_{t_over_J_sq} := 0.544$

what n i.e. J will satisfy the relationship for a B 5.75 propeller with P/D -1.0


$$K_{t_design}(J) := K_{t_over_J_sq} \cdot J^2$$

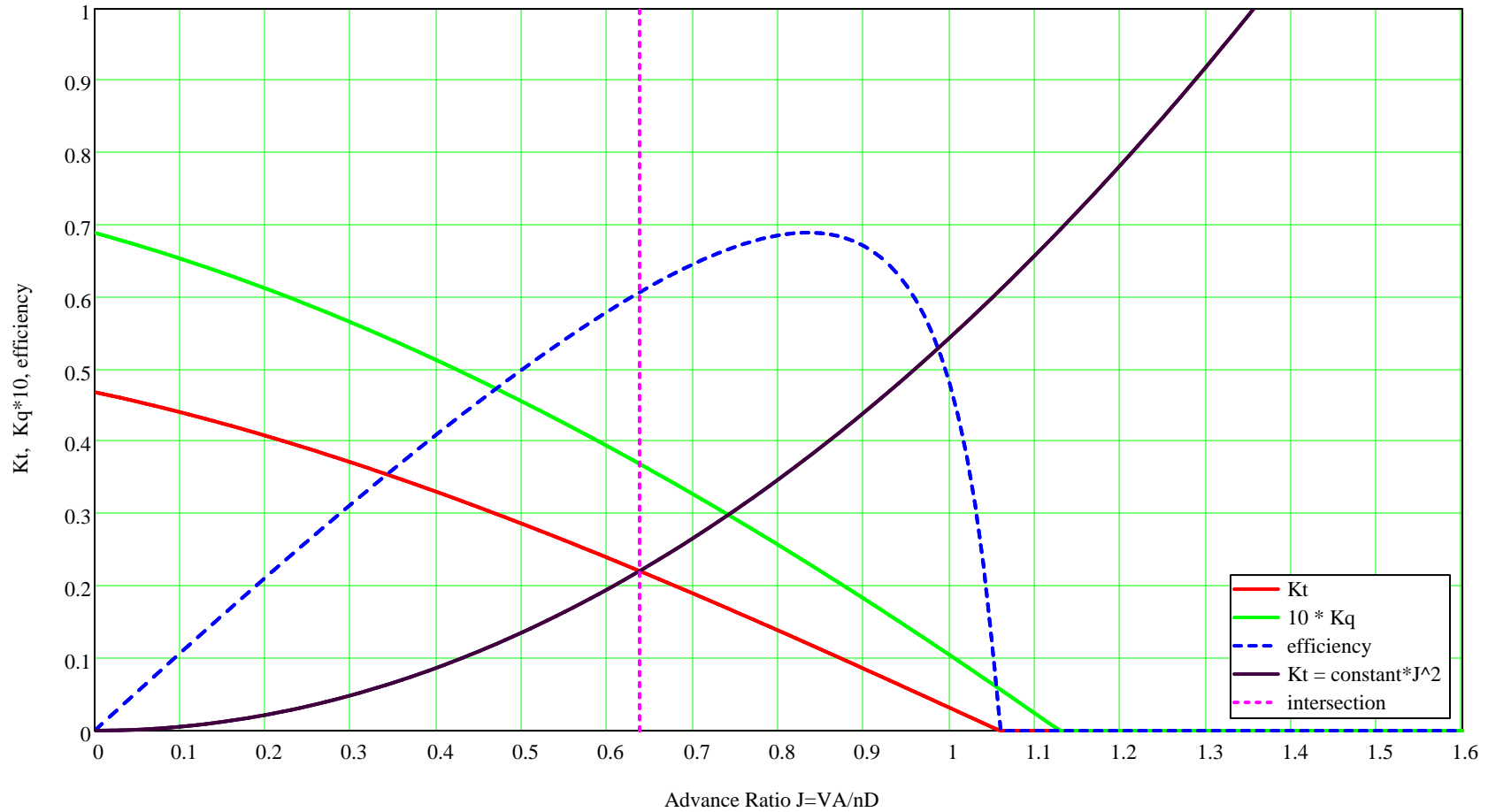
select using B_series

$$z := 5$$

$$EAR := 0.75$$

$$P_over_D := 1.0$$

 determine intersection



intersection occurs at

$$JJ = 0.64$$

so ...

$$n = \frac{V_A}{JJ \cdot D}$$

where V_A and D are known as described above

selection of the optimum n for this B z.EAR propeller is a matter of comparing similar curves for a range of P/D and choosing the maximum open water efficiency η_o

B series

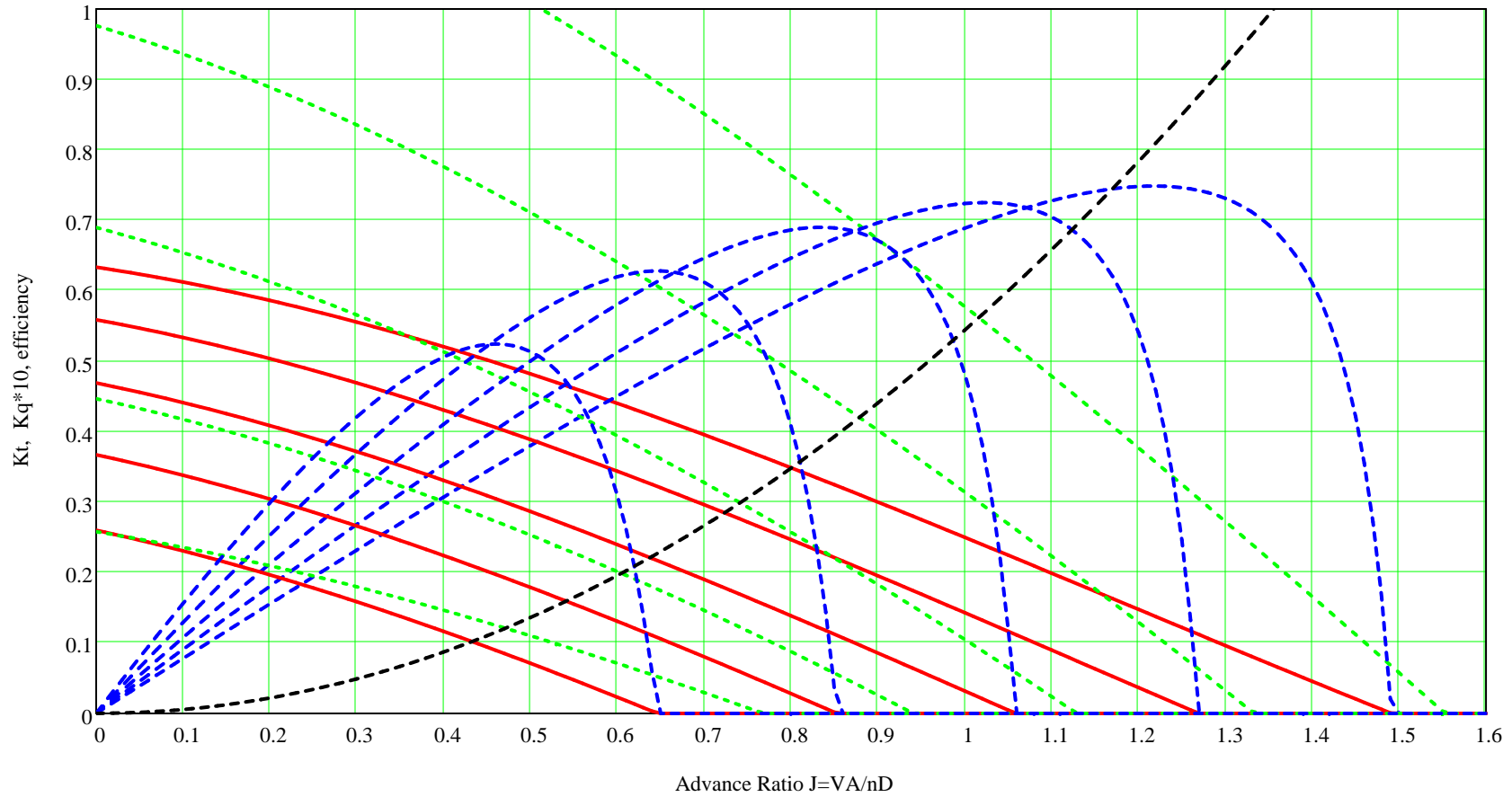
$z = 5$

EAR = 0.75

say

$P_{over D} :=$

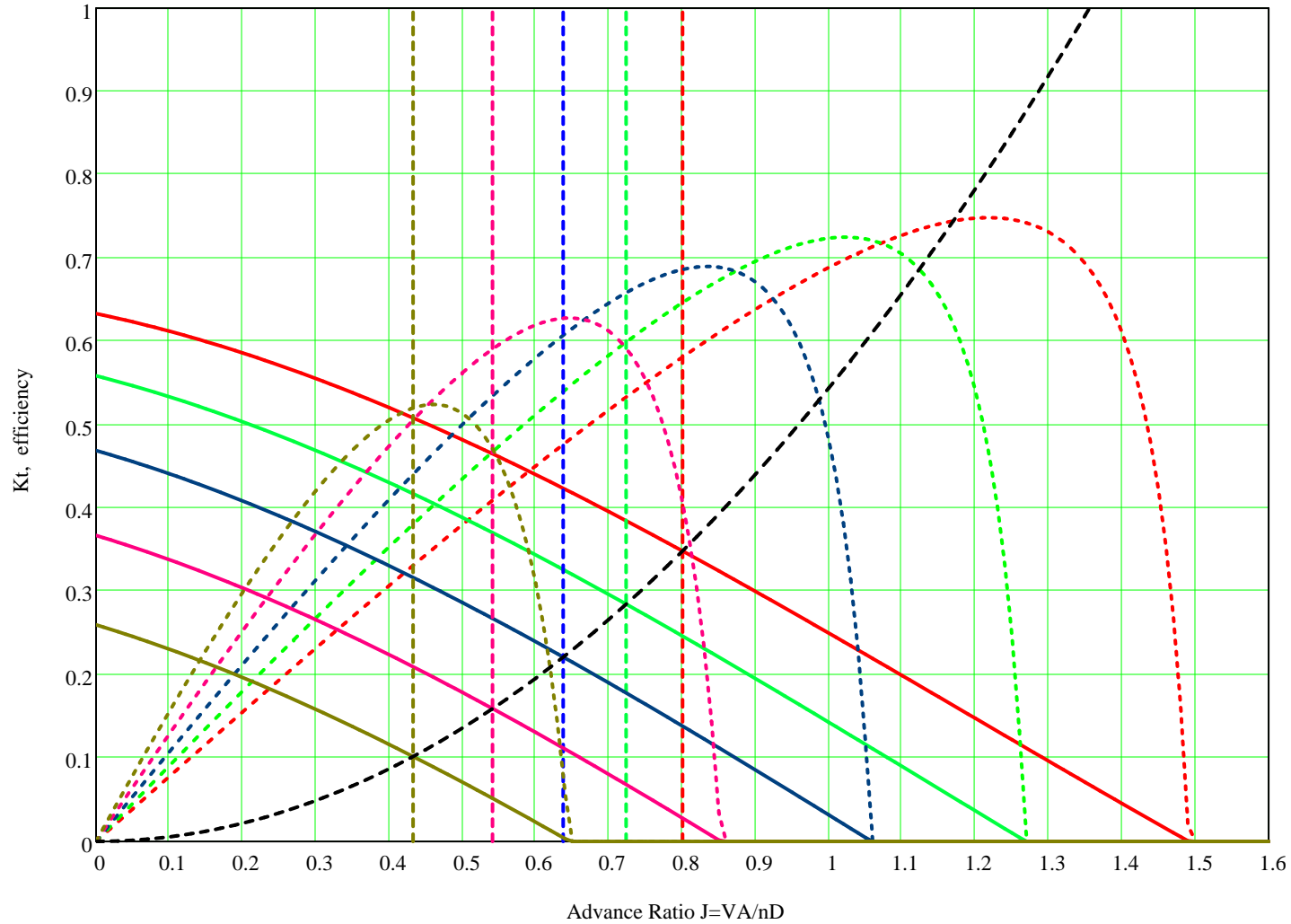
(1.4
1.2
1.0
0.8
0.6)



busy plot of K_t , K_q , η_o and $K_t = \text{constant} \cdot J^2$. see breakdown below. P/D not labeled but $\sim J$ at $K_t = 0$

intersection solution

plot with only Kt but vertical lines at J for $Kt/J^2 = Kt$ to show points which satisfy the design requirements



P/D = 0.6

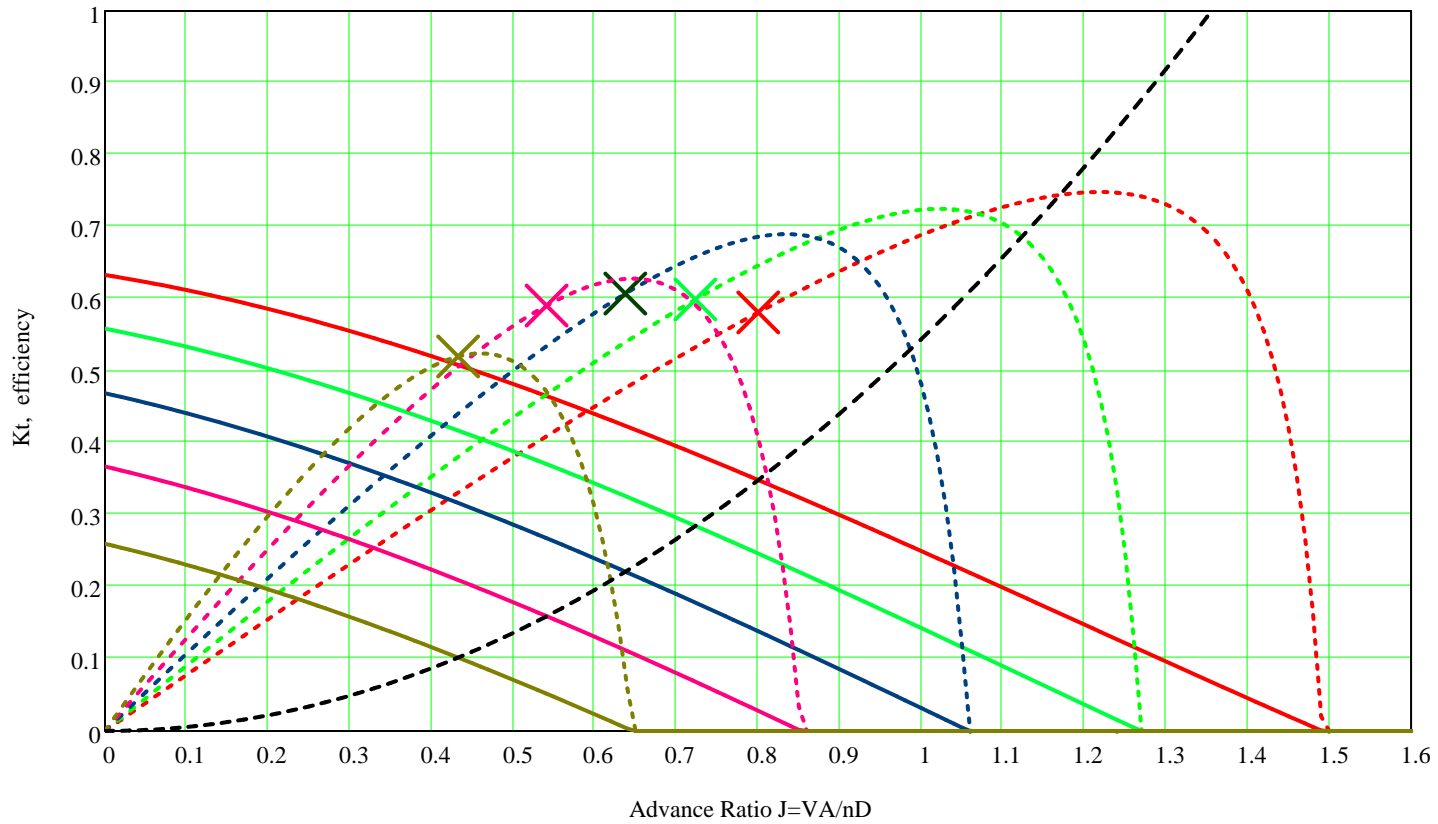
P/D = 0.8

P/D = 1.0

P/D = 1.2

P/D = 1.4

note the η_0 at each J intersection and select the maximum (P/D curves not well labeled, P/D ~ = J at $K_T=0$. left to right lowest to highest)



Plot for P/D = $P_{over_D}^T = (1.4 \ 1.2 \ 1 \ 0.8 \ 0.6)$ calculated using regression relationships

this case appears to have maximum at $J_{ans} = 0.64$ $P_{over_D_ans} = 1$ $\eta(J_{ans}, EAR, z, P_{over_D_ans}) = 0.61$

so ...
$$n = \frac{V_A}{J_{ans} \cdot D}$$
 where V_A and D are known as described above

case 2 given: V_A, T, n find P/D and D for maximum efficiency

only thing unknown is D , eliminate ... from ratio of K_T and J

$$\frac{K_t}{J^4} = \frac{T}{\rho \cdot n^2 \cdot D^4} \cdot \frac{n^4 \cdot D^4}{V_A^4} = \frac{T}{\rho} \cdot \frac{n^2}{V_A^4}$$

this says that propeller (full scale and model) must match this ratio which is a constant determined by T , V_A , n and ρ

$$K_{t_over_J_4} := \frac{T}{\rho \cdot D^2 \cdot V_A^2}$$

we can plot a curve of K_T vs J^4 and determine the points (values of J) for which K_T vs J for a given P/D match.

for example, let $K_{t_over_J_4} := 0.544$

$$K_{t_design}(J) := K_{t_over_J_4} \cdot J^4$$

select using B_series

$$z := 5$$

$$EAR := 0.75$$

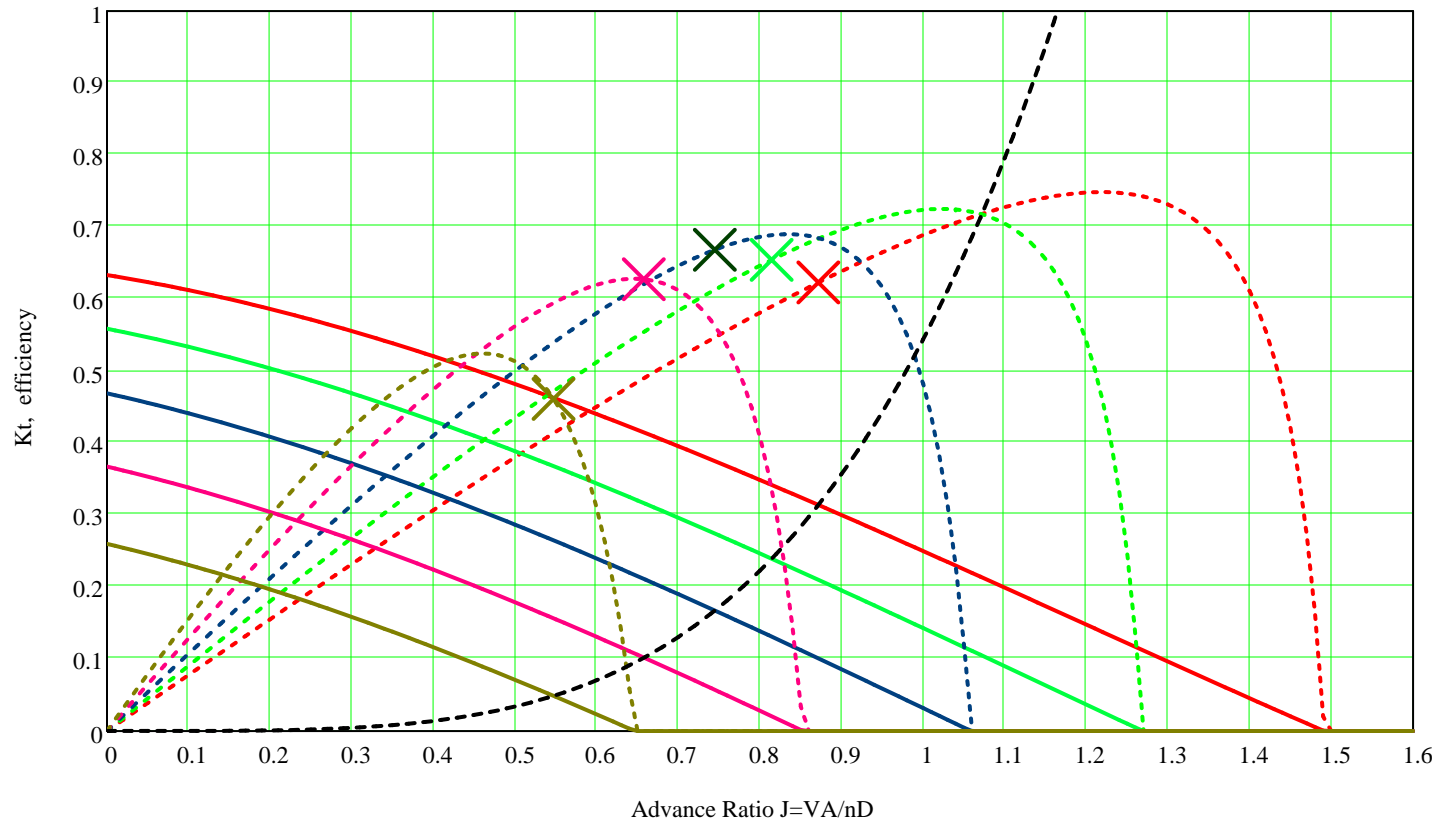
the design point for a particular propeller (B.n.nn) i.e. n is determined from the value of J that satisfies:

$$K_t(J) = \text{constant} \cdot J^4$$

since the process is identical to case 1, only the final result is shown

 intersection solution

note the η_0 at each J intersection and select the maximum (P/D curves not well labeled, P/D \sim J at $K_T=0$. left to right lowest to highest)



Plot for P/D = $P_{over_D}^T = (1.4 \ 1.2 \ 1 \ 0.8 \ 0.6)$ calculated using regression relationships

this case appears to have maximum at $J_{ans} = 0.74$ $P_{over_D_ans} = 1$ $\eta(J_{ans}, EAR, z, P_{over_D_ans}) = 0.67$

and ... $D = \frac{V_A}{J_{ans} \cdot n}$ where V_A and n are known as described above