

6.334 Lecture Notes

Intro to DC/AC

First Averaged Circuit rules



$$KCL \quad \sum_{\downarrow} i_{\downarrow} = 0$$

$$\frac{1}{T} \int \sum_{\downarrow} i_{\downarrow} dt = 0$$

$$\sum_{\downarrow} \frac{1}{T} \int i_{\downarrow} dt = 0$$

$$\boxed{\sum_{\downarrow} \langle i_{\downarrow} \rangle = 0}$$

KCL Applies to time-average currents (cons. charge)

The same is true for KVL $\sum_k \langle V_k \rangle = 0$

So for a power converter in PERIODIC STEADY STATE :

1. Average KCL $\sum_{\downarrow} \langle i_{\downarrow} \rangle = 0$

2. Average KVL $\sum_k \langle V_k \rangle = 0$

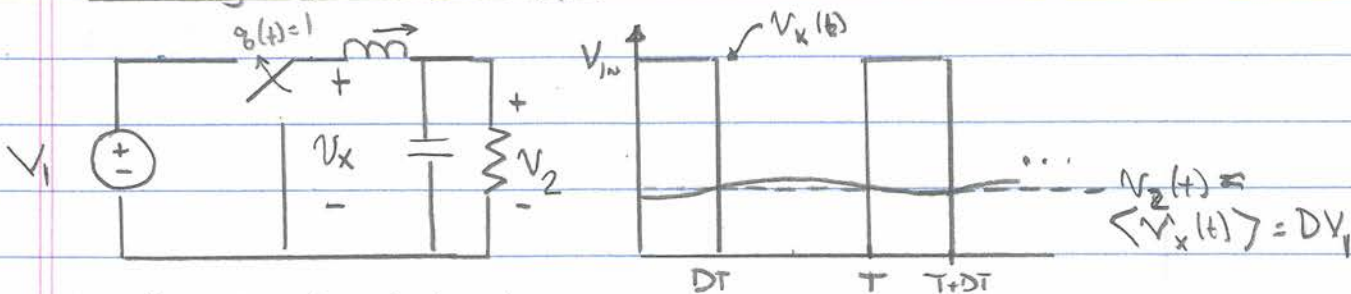
3. Capacitors in P.S.S. $\langle i_c \rangle = 0$

4. Inductors in P.S.S. $\langle V_L \rangle = 0$

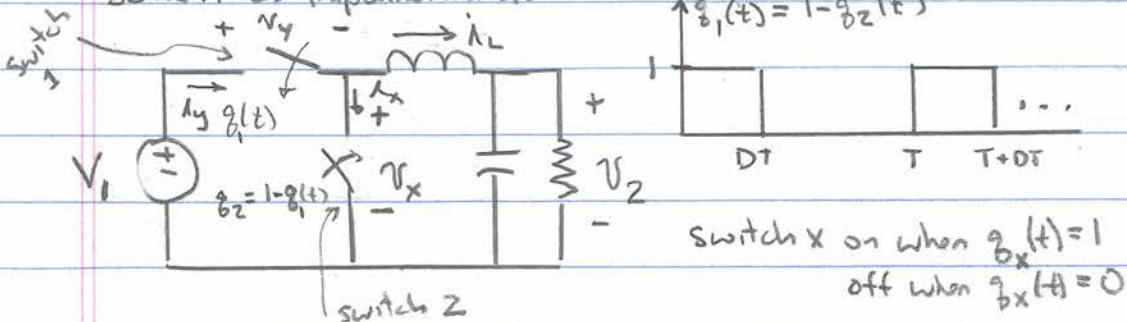
5. If system lossless $\langle P_{in} \rangle = \langle P_{out} \rangle$
(cons. of energy)

Review

Switching Regulator Example "Buck Converter"



Sometimes implemented as:

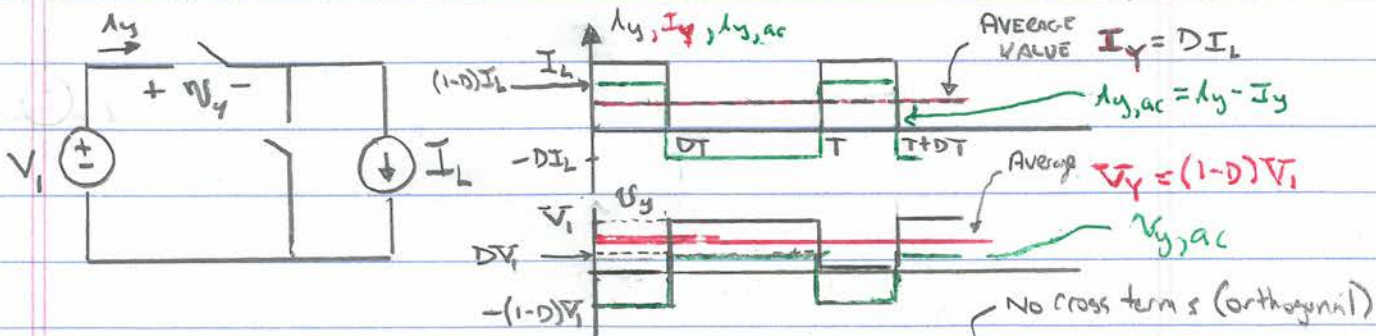


Assume L's, C's are very big : $v_o(t) \approx V_o$, $i_L(t) \approx I_L$

using average relations in p.s.s. $\langle v_L \rangle = \langle v_x \rangle - \langle v_2 \rangle$

$$\langle v_L \rangle = \frac{1}{T} [DT (V_1 - V_2) + (1-D)T (-V_2)] = 0 \Rightarrow \boxed{V_2 = DV_1}$$

ASIDE: WHAT DO SWITCH 1 + SWITCH 2 DO? LETS IGNORE INDUCTOR RIPPLE



$$\text{Ave Power into sw1: } \langle P_1 \rangle = \langle (v_1 + v_{2,ac})(I_Y + i_{Y,ac}) \rangle = \langle v_1 I_Y \rangle + \langle v_{2,ac} i_{Y,ac} \rangle$$

$$\langle P_1 \rangle = D(1-D)I_L V_1 + \{ D[-(1-D)^2 I_L V_1] + (1-D)[-D^2 I_L V_1] \}$$

Avg. Power into switch due to dc I_Y Avg. power into switch due to ac $i_{Y,ac}$

$$= \boxed{D(1-D)I_L V_1} - \boxed{D(1-D)I_L V_1} = 0$$

Switch S1 takes average power in from dc current, voltage and puts equal power out at ac current, voltage. Converts power (efficiently) from dc to ac waveforms! ("invertin", "switch")

Note: Switch S2 Does the opposite (converts power from ac waveforms to dc waveforms)! ("rectifying", "switch")

Co.334 Lecture Notes

Intro. to dc/dc

Consider input current:

L's, C's big, $i_L(t) \approx I_L$

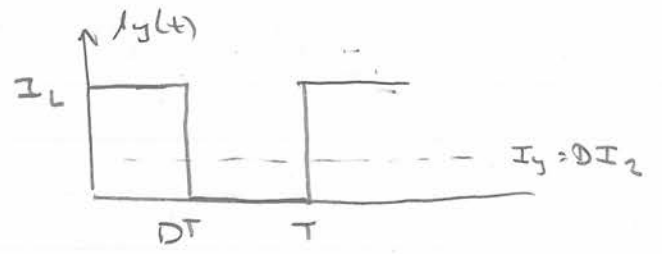
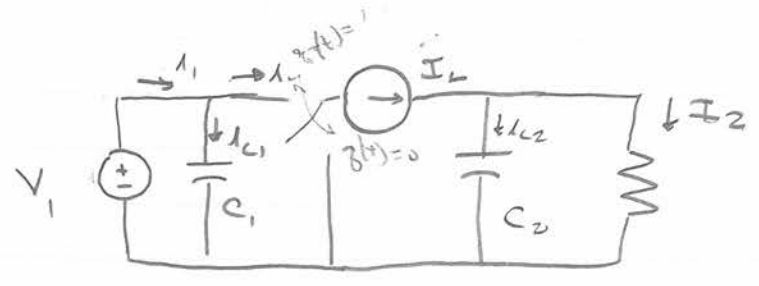
p.s.s. $\langle i_{c2} \rangle = 0 \therefore I_2 = I_L$

p.s.s. $\langle i_{c1} \rangle = 0 \therefore$

$$I_1 = \langle i_1 \rangle = \langle i_y \rangle = DI_2$$

$$\therefore \boxed{I_1 = DI_2}$$

Combining w/ previous result
 $DI_1 = I_2$

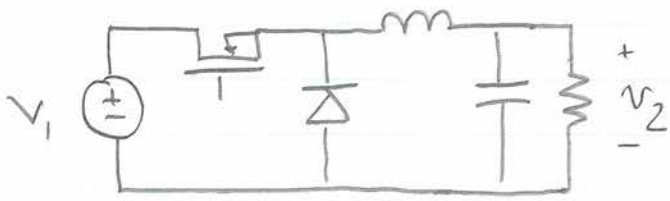


$$I_1 V_1 = I_2 V_2 \leftarrow \text{lossless system!}$$

Note: The trick is to be careful about when one is dealing with instantaneous variables, and when one is dealing with average variables!

e.g. at a given instant, $i_y(t) \neq \langle i_y(t) \rangle$

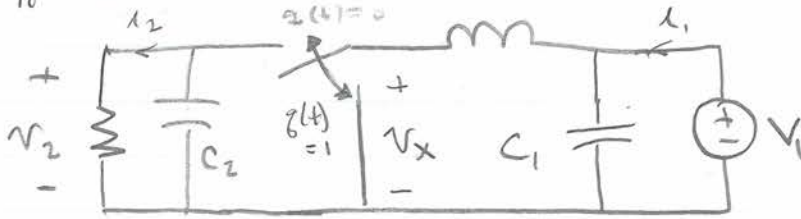
Switch implementation for this case, $V_1, V_2 > 0$



Power flows 1 \rightarrow 2

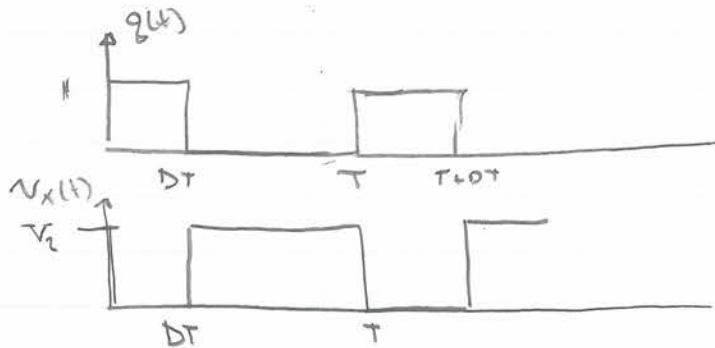
"Down" or "buck" converter. A type of "direct" converter because in one switch state, power flows directly from input to output

Suppose we switch source + resistor.



* note, redefine $g(t)=1$ as switch "down" position

If C's, L's big, same analysis:



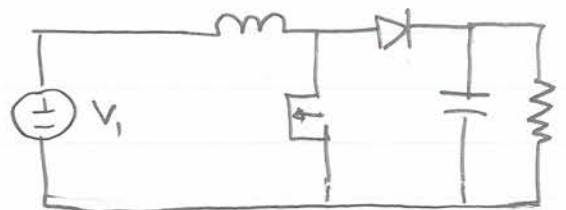
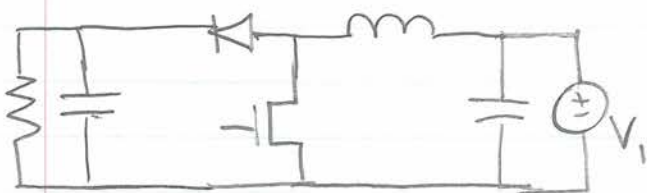
$$\langle V_L \rangle = 0 \therefore \langle V_x \rangle = (1-D)V_2 = V_1$$

$$\therefore \boxed{V_2 = \frac{V_1}{1-D}} \quad \text{AND} \quad \boxed{\frac{I_2}{1-D} = I_1}$$

If $V_1, V_2 > 0$, then power flows $2 \leftarrow 1$ AND $V_2 > V_1$

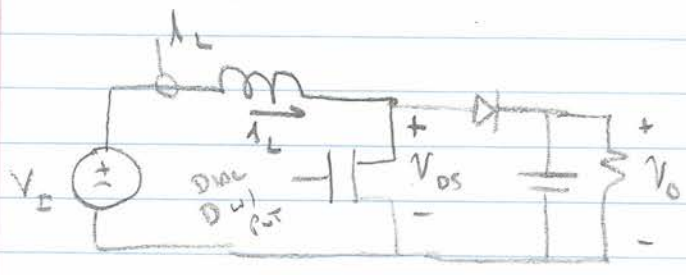
Boost converter:
(or "up" converter)

Sometimes draw $L \rightarrow R$ power flow
(but nothing fundamental about it).



★ SHW BOOST CONVERTER DEMO CIRCUIT

→ BUILT BY KATIE R. + SAURABNA DAS

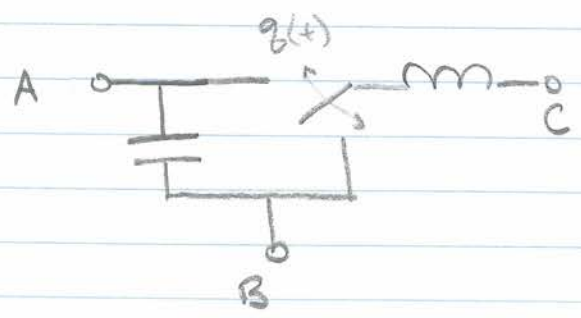


- SHOW:
1. V_{DS}
 2. i_L
 3. V_O on scope

Explain Boost Operation:

- Switch turns on, i_L rises + incrementally stores energy in L from V_I
- Switch turns off + this energy plus additional energy from V_I is transferred to output
- Steady state voltages are determined by $V_2 = \frac{V_1}{1-D}$

Either buck or boost can be viewed as a connection of a "canonical cell"



- "Direct" connection has B common
- one cannot tell power flow direction without knowing
 1. external networks
 2. switch implementation
 3. control

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