6.622 Power Electronics

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Lecture 18 - Inverters 2

From last time:



- 1. We can synthesize pulsing voltages +, 0, over time
- 2. Filter to get desired output waveform (e.g. sinusoid)

3. Switching frequency limitations are often a practical constraint

 \Rightarrow Show inverter module from a toyota prius as example

To reduce filtering requirements, we often use waveform symmetrics to reduce unwanted content.

$$f(t) = \frac{b_0}{2} + \sum_{n=1}^a a_n \sin(n\omega_0 t) + b_n \cos(n\omega_0 t)$$
$$a_n = \frac{2}{T} \int_{\langle T \rangle} f(t) \sin(n\omega_0 t) dt, b_n = \frac{2}{T} \int_{\langle T \rangle} f(t) \cos(n\omega_0 t) dt$$

- For odd/even waves, synthesize odd/even patterns
- for half-wave symmetric outputs $f(t) = -f(t \frac{T}{2})$ synthesize half-wave symmetric pulse patterns $(a_{2k}, b_{2k} \text{ harmonics do not exist!})$

$$f_{hws}(t) = \frac{f(t) - f(t - \frac{T}{2})}{2}; f_{hwr}(t) = \frac{f(t) + f(t - \frac{T}{2})}{2}; f(t) = f_{hws} + f_{hwr}$$

We have seen that by control of the width of one pulse per half cycle (and each device switching on/off once per full cycle) we can

- Maintain half-wave symmetry (no even harmonics)
- eliminate triple-n harmonics (especially 3rd harmonic)

• keep odd symmetry (no cosine components)

Why? With only odd components, nth harmonic amplitude is:



Positive area of $f(t)sin(2\omega t)$ cancels negative area \therefore integral = 0!

 \Rightarrow we can introduce <u>more</u> notices in each half cycle (for <u>more switching transitions in each cycle</u>) so that higher harmonics (e.g. 5th are cancelled) while <u>not</u> disturbing the nullling of the 3rd. (see one example, next page)

In general: Harmonic elimination / programmed PWM

- Can eliminate one odd harmonic for each pulse per half cycle (and each switching transition per ac cycle)
- More harmonics eliminated, the higher the net device switching frequency
- Precise timing measured (μP)

 \rightarrow As more lower-order harmonics are eliminated, high-order harmonics actually increase, but these are more easily filtered!



Note: see classic papers for more on this area:

- H. S. Patel and R. G. Hoft "Generalized Techniques of Harmonic Elimination and Voltage Control in Thyristor Inverters: Part I — Harmonic Elimination Techniques"
- H. S. Patel and R. G. Hoft "Generalized Techniques of Harmonic Elimination and Voltage Control in Thyristor Inverters: Part II — Voltage Control Techniques"

Harmonic Cancellation 1

Add up time-shifted waveforms to cancel desired harmonic component(s)

If $\mathbf{x}(\mathbf{t}) = \Sigma A_n \sin(n\omega_0 t + \Phi_n)$ $\therefore x(t-t_1) = \Sigma A_n \sin(n\omega_0(t-t_1) + \Phi_n)$ = $\Sigma A_n \sin(n\omega_0 t + \Phi_n - n\omega_0 t_1) (\Phi_n - n\omega_0 t_1 = \Phi'_n)$

If we time-shift to change the fundamental by an angle $\Delta \Theta_T = -\omega_0 t_1$, we shift the nth harmonic by an angle $\Delta \Phi_n = n \Delta \Phi_1$



- Shift fundamentals by $36^{\circ} (\pm 18^{\circ})$
- Shifts 5th harmonic by $180^{\circ} (\pm 90^{\circ})$



By adding waveforms time shifted so that their 5th harmonics are 180° out of phase, the 5th harmonic is cancelled in the summed waveform!

<u>Harmonic cancellation</u> and <u>harmonic elimination</u> can also be applied in other forms of power converters. For example, in dc-dc conversion, we have a desired frequency (dc) and undesired components (all ac ripple). We can suppress these, reducing ripple content + increasing fundamental ripple frequency.



With 2 converters, <u>fundamental</u> ripple

- 1. Frequency doubles!
- 2. Also, p-p current ripple (net) is <u>half</u> that of a single high-power unit.

We can <u>interleave</u> N identical converters by phase-shifting them by $\Delta t = \frac{T}{N}(\omega_1 = \frac{2\pi}{N})$. The net ripple

frequency in the input and output waveforms will ideally be at N times the individual switching frequency! \rightarrow This trick is very widely used, including in the converters for most PC power supplies feeding the final low voltage to the microprocessor

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