

## Lecture 26 - Control 2

## 1 Control Design Example

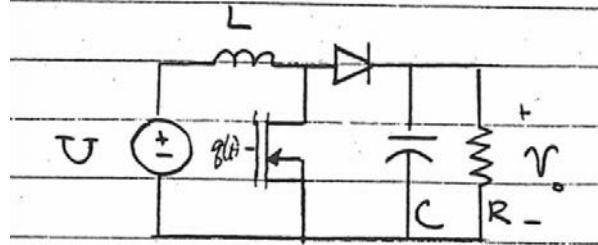
Boost converter

$$L = 10\mu H, C = 50\mu F$$

$$f_s w = 100kHz, V_{0,ref} = 24V$$

$$U_{nom} = 9V, 8V < U < 10V$$

$$2\Omega < R < 10\Omega$$



Start with switched equations of state:

$$\begin{cases} \frac{di_L}{dt} = \frac{u}{L}q(t) + \frac{(u-v_0)}{L}(1-q(t)) \\ \frac{dv_0}{dt} = -\frac{1}{RC}v_0q(t) + \left(\frac{1}{C}i_L - \frac{1}{RC}v_0\right)(1-q(t)) \end{cases}$$

State space averaging with  $\bar{x} = \frac{1}{T} \int_{t-T}^t x(\tau) d\tau$  results in nonlinear averaged model

$$\begin{cases} \frac{d\bar{i}_L}{dt} = \frac{\bar{u}}{L} + \frac{\bar{v}}{L}d' \\ \frac{d\bar{v}_0}{dt} = -\frac{1}{RC}\bar{v}_0 + \frac{1}{C}\bar{i}_Ld' \end{cases}$$

Linearization about op. point.  $U, I_L, V_0, D$  yields LTI linearized model of incremental dynamics

$$\begin{cases} \frac{d\tilde{i}_L}{dt} = \frac{\tilde{u}}{L} - \frac{D'\tilde{v}_0}{L} + \frac{V_0\tilde{d}}{L} \\ \frac{d\tilde{v}_0}{dt} = -\frac{1}{RC}\tilde{v}_0 + \frac{D'\tilde{i}_L}{C} - \frac{I_L\tilde{d}}{C} \end{cases}$$

Using Laplace transform and identity  $\frac{V_0}{R} = D'I_L$ 

$$H(s) = \frac{v_0(s)}{\tilde{d}(s)} = \frac{-s \frac{V_0}{RC D'} + \frac{V_0 D'}{LC}}{s^2 + \frac{1}{RC}s + \frac{D'^2}{LC}}$$

Transfer function depends on op. point.

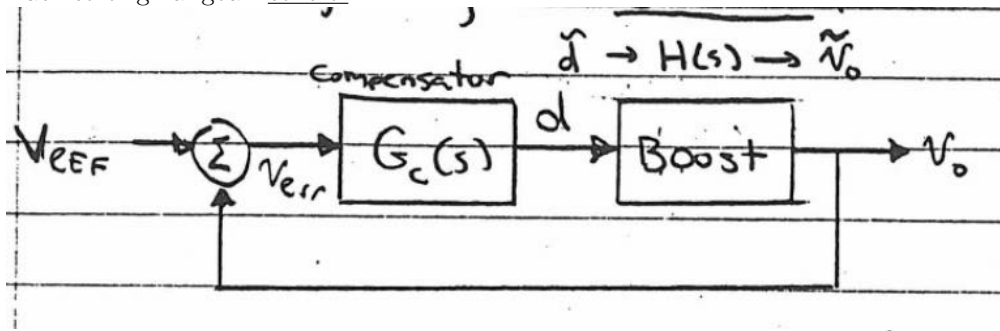
$$@ u = 9, V = 24, D = 0.625$$

$$I_L \approx 25.6A, R = 2.5\Omega, C = 50\mu F, L = 50\mu H$$

$$\frac{\tilde{v}_0}{\tilde{d}} = \frac{-512000s + 1.8 \times 10^{10}}{s^2 + 8000s + 2.81 \times 10^8}$$

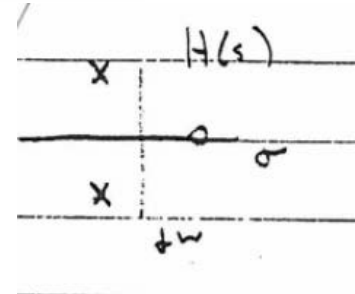
zero at  $s = 35,156$ Poles at  $s = -4000 \pm j16279$ period  $\approx 0.4ms$

Back to original goal: control!

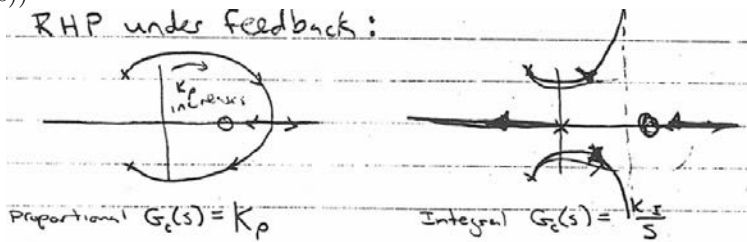


Looking at our transfer function, we have

1. 2 lightly-damped poles in LHP
2. 1 RHP zero



This is tricky, because the poles tend to move to the RHP under feedback: (Note sign in numerator of H(s))



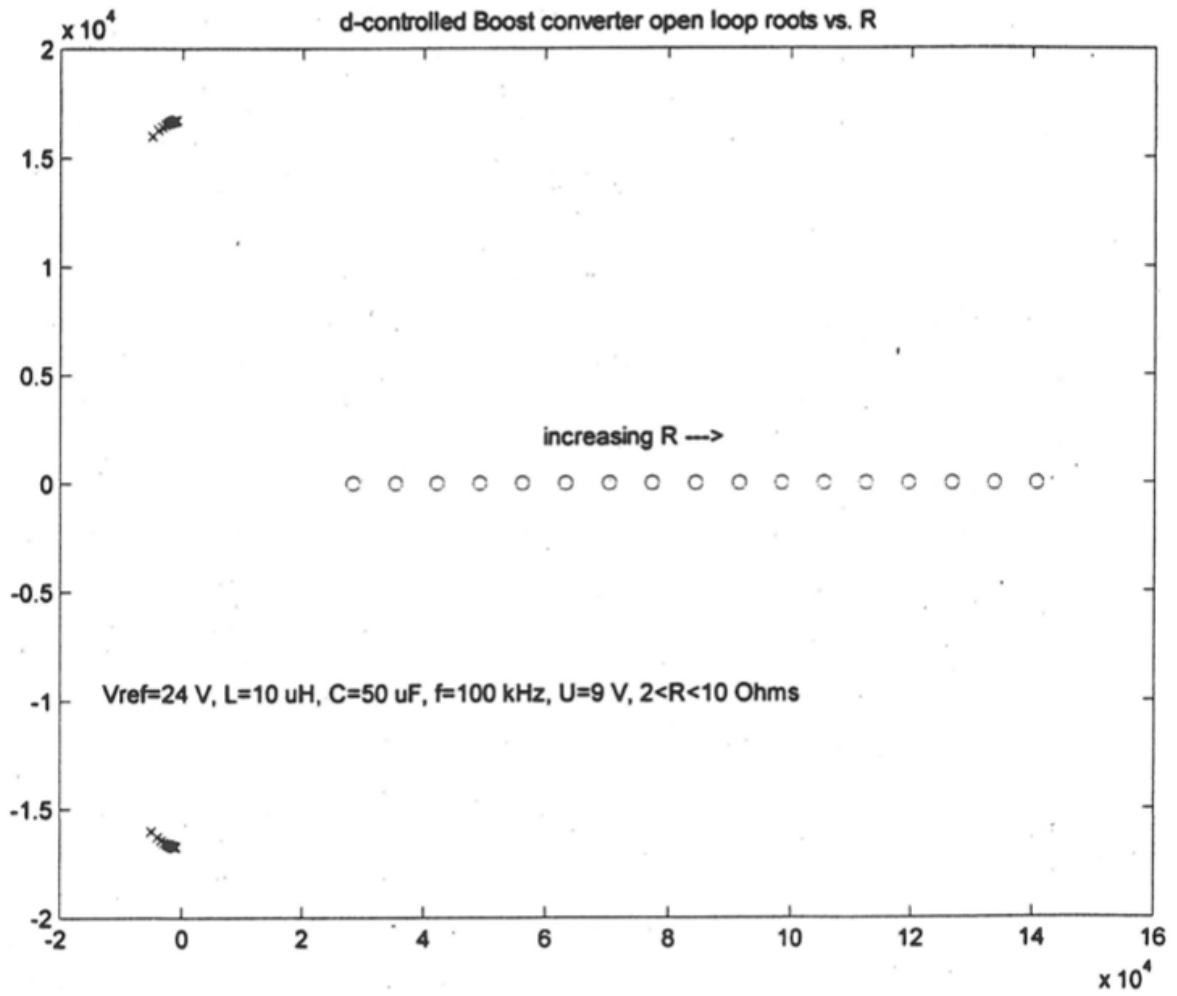
→ So, we must pick control gains that are not too high for stability.  
Also, the poles move with operating point! (variations in U, R for example)

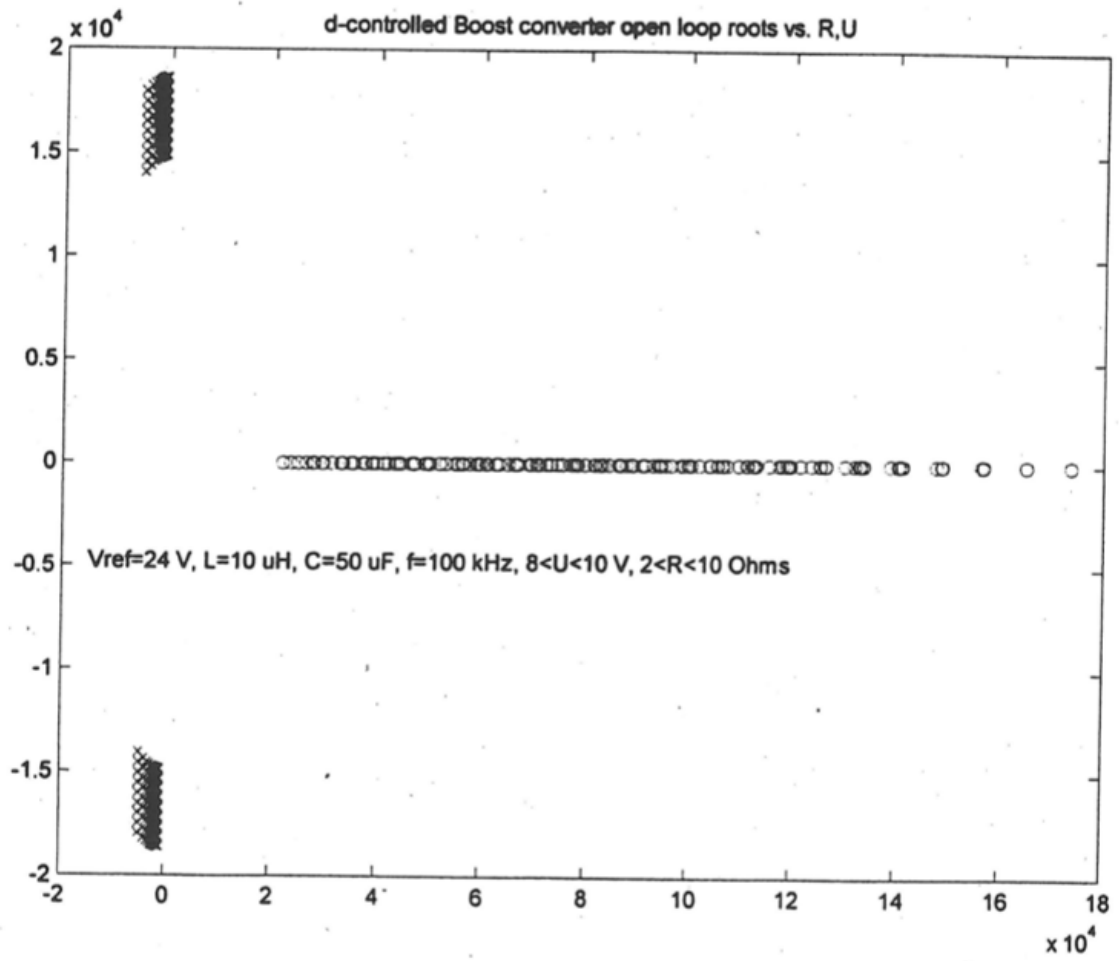
- Look at slide for variations of poles with R (problem becomes more difficult at light load...)
- Could use a damping leg !! (neat trick)

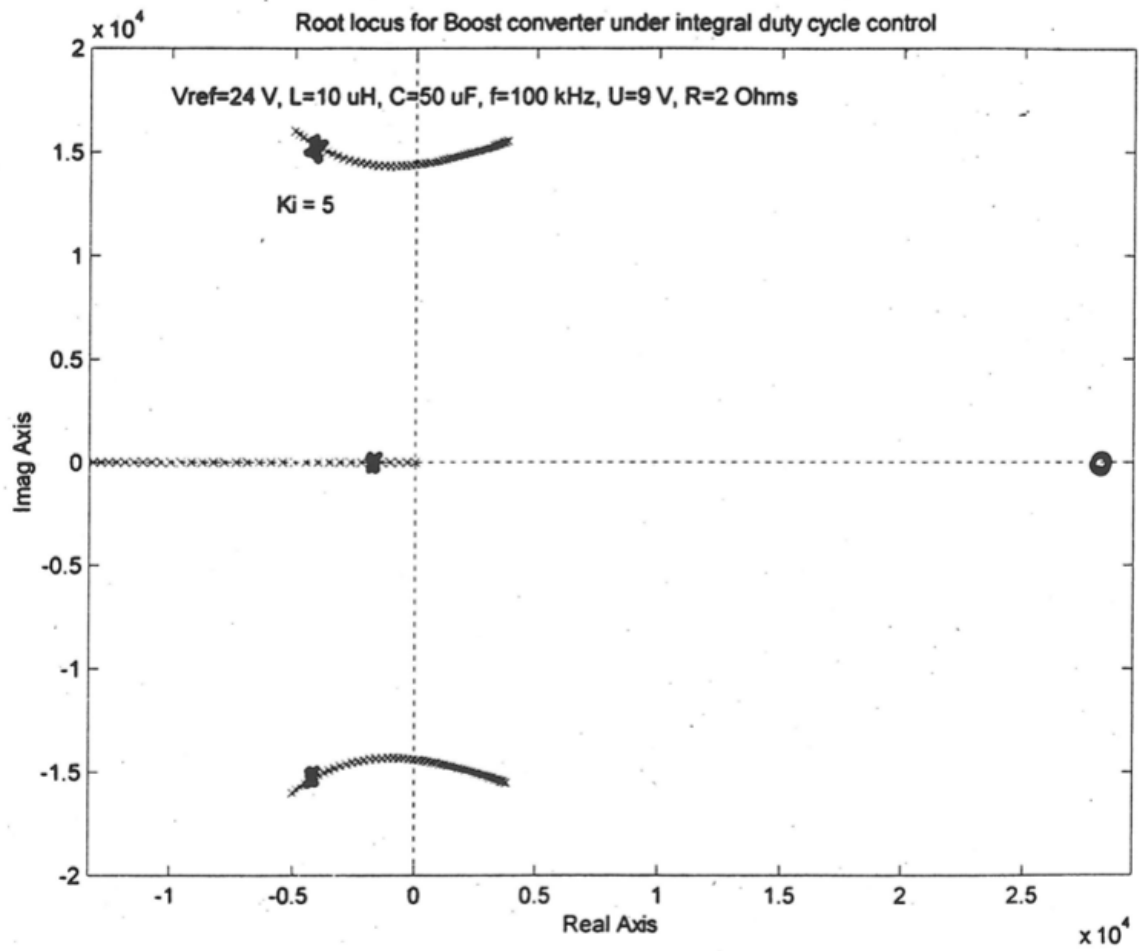
Must design controller valid over all operating points

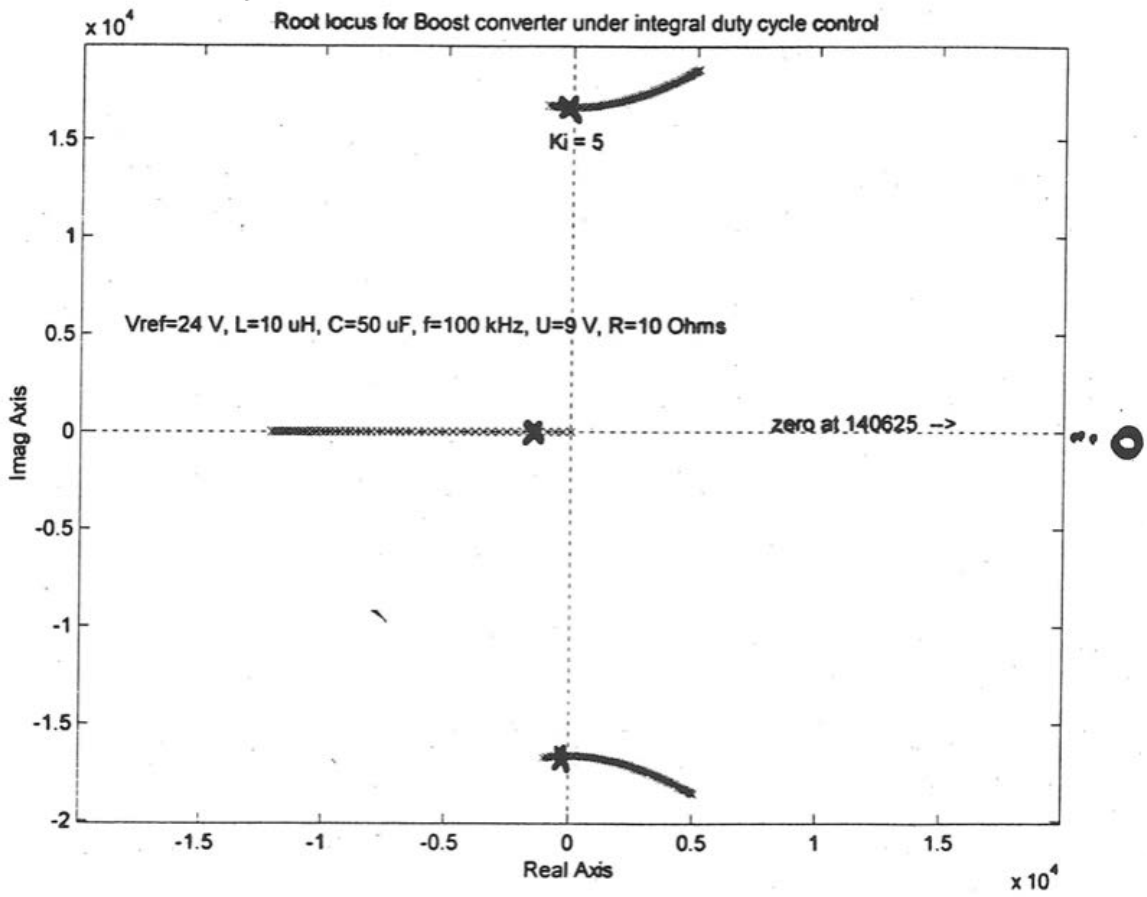
- Look at simple integral controller design
- Note: technically only small signal dynamics are determined, but power converters are forgiving in this respect.

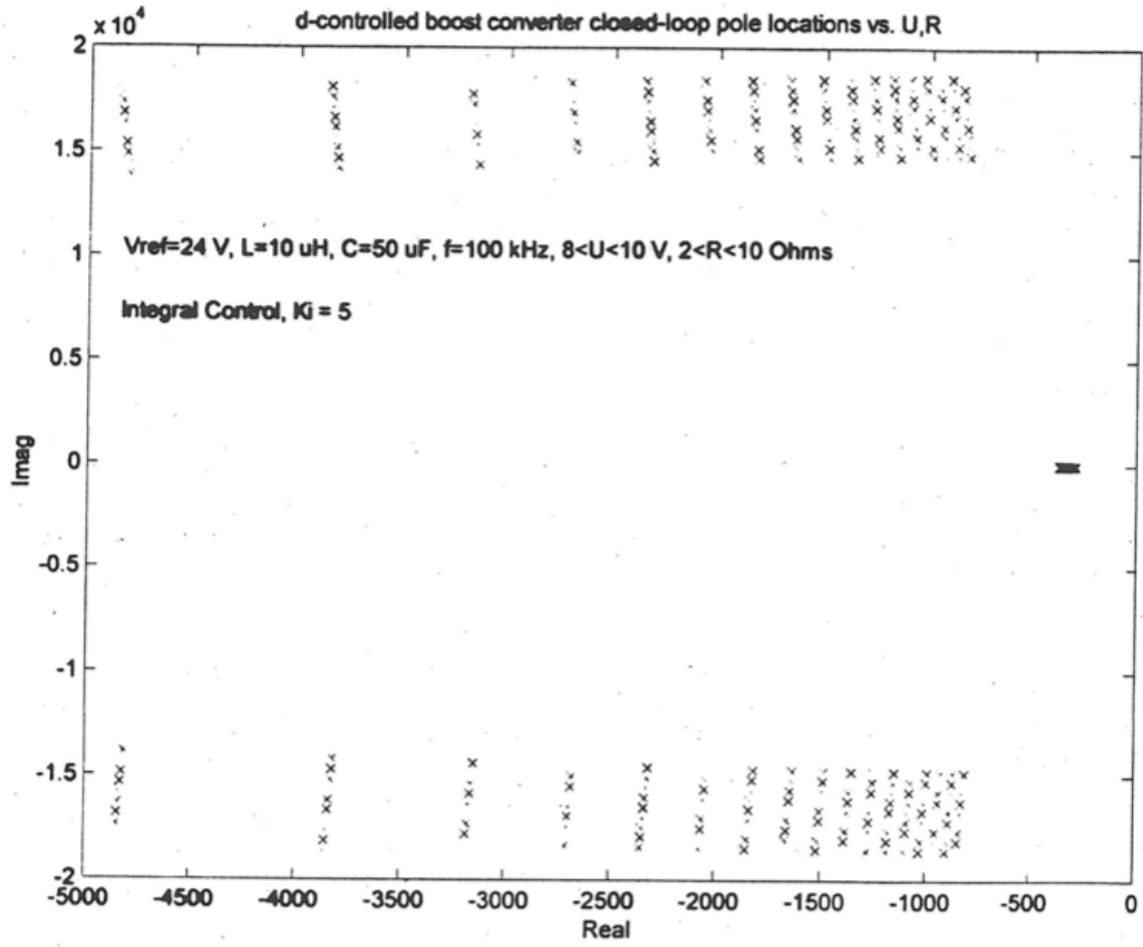
Note: This controller may not be ok in practice due to lightly-damped poles (noise sensitive, transient perf, etc), main pro is RHP zero!! → go to the current-mode control!!







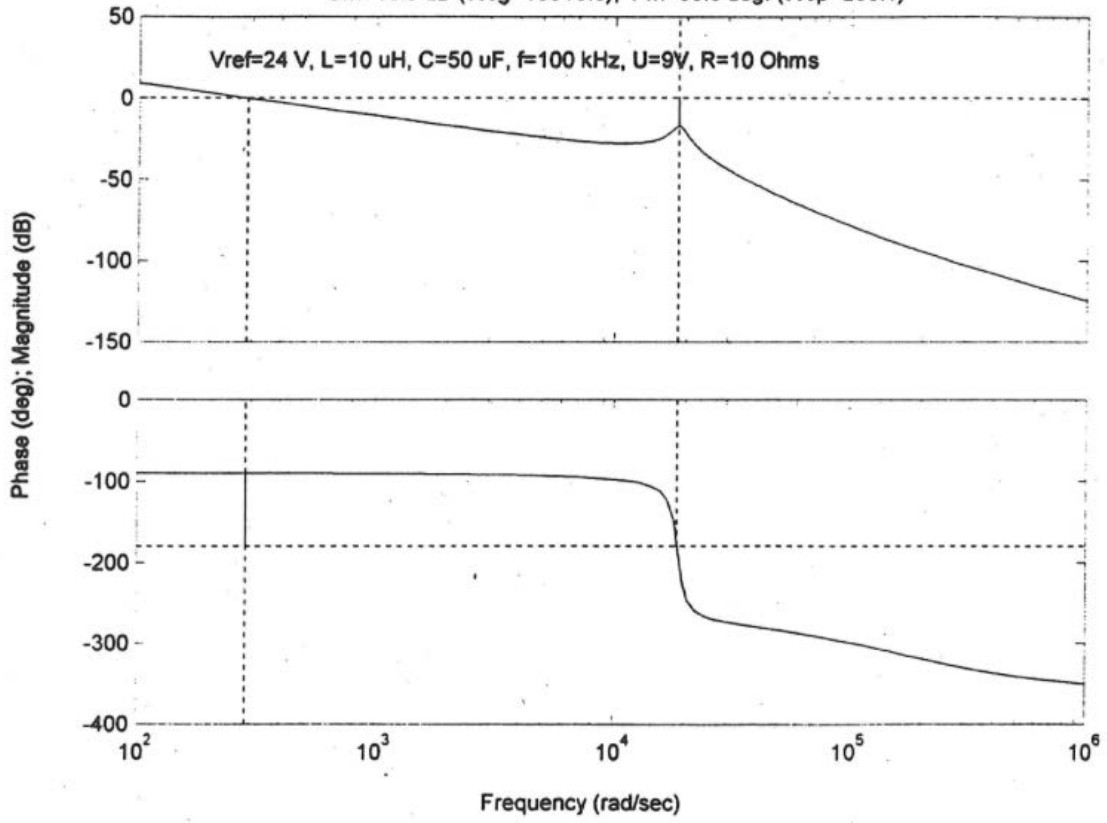




### Bode Diagrams

Gm=16.9 dB (Wcg=18516.6); Pm=89.8 deg. (Wcp=288.1)

Vref=24 V, L=10 uH, C=50 uF, f=100 kHz, U=9V, R=10 Ohms



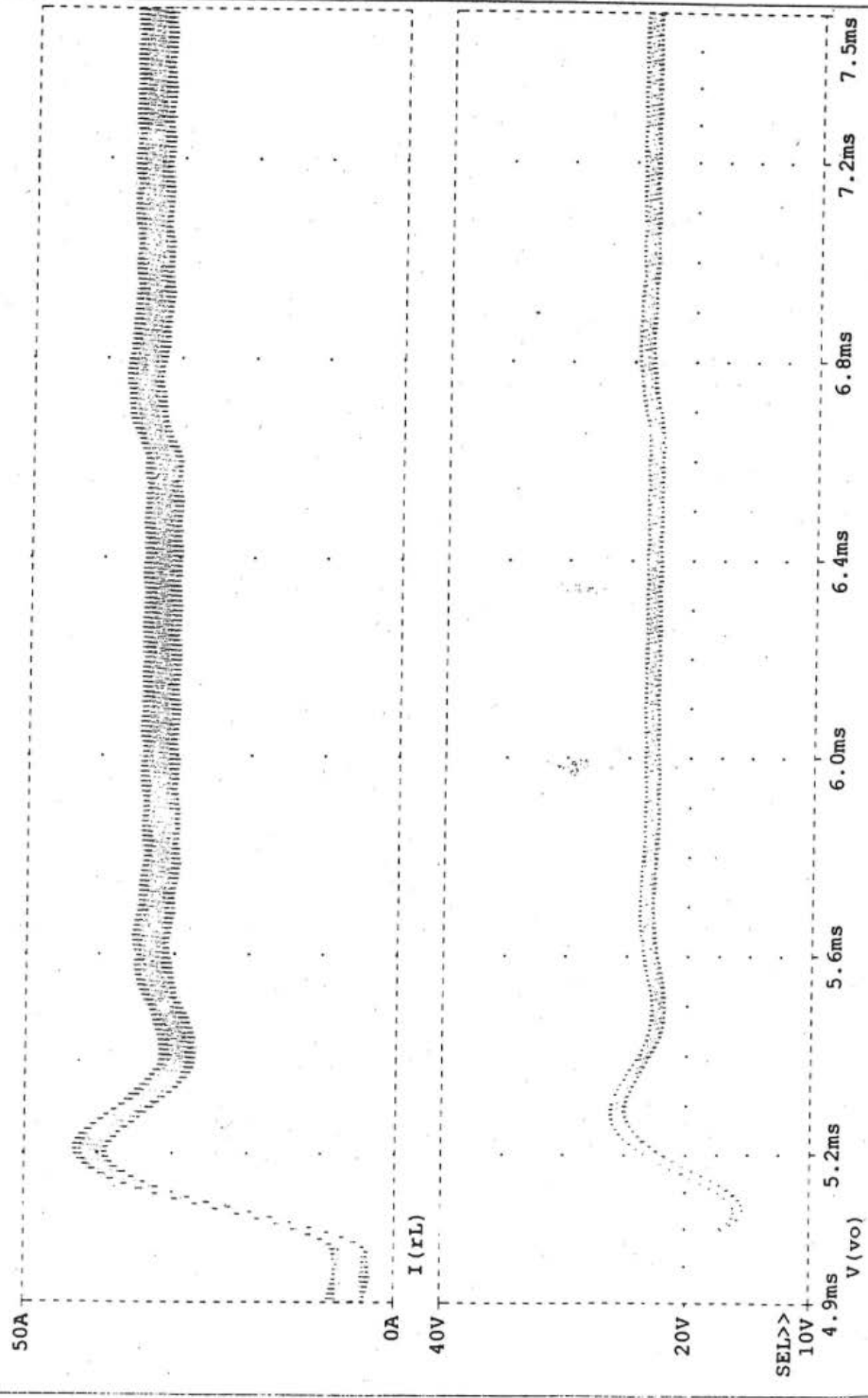


\* C:\MSimEv\_8\Projects\Boost\_c4.sch

Temperature: 27.0

Date/Time run: 04/01/99 23:21:54

(B) Boost\_c4.dat



Time

Date: April 01, 1999

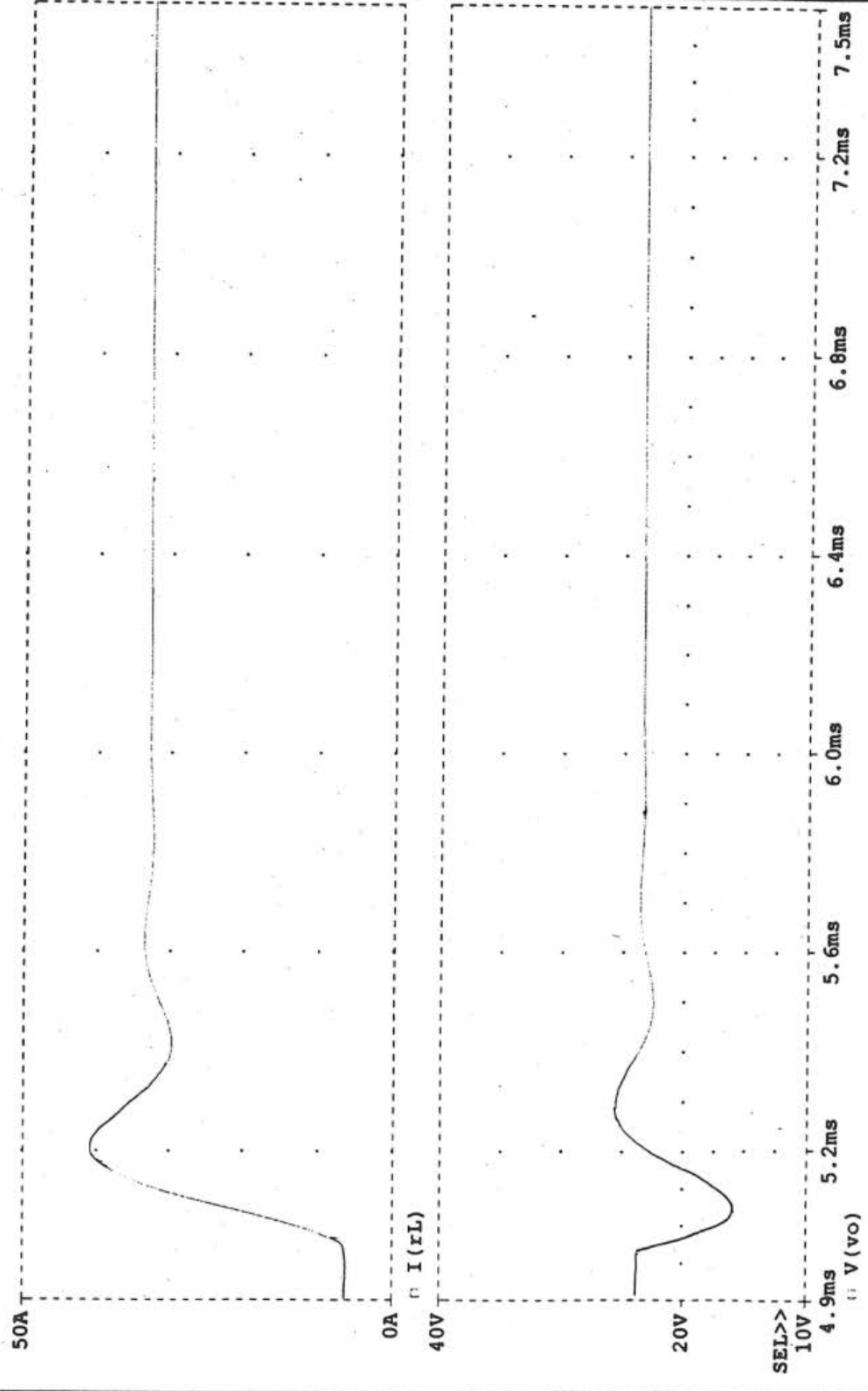
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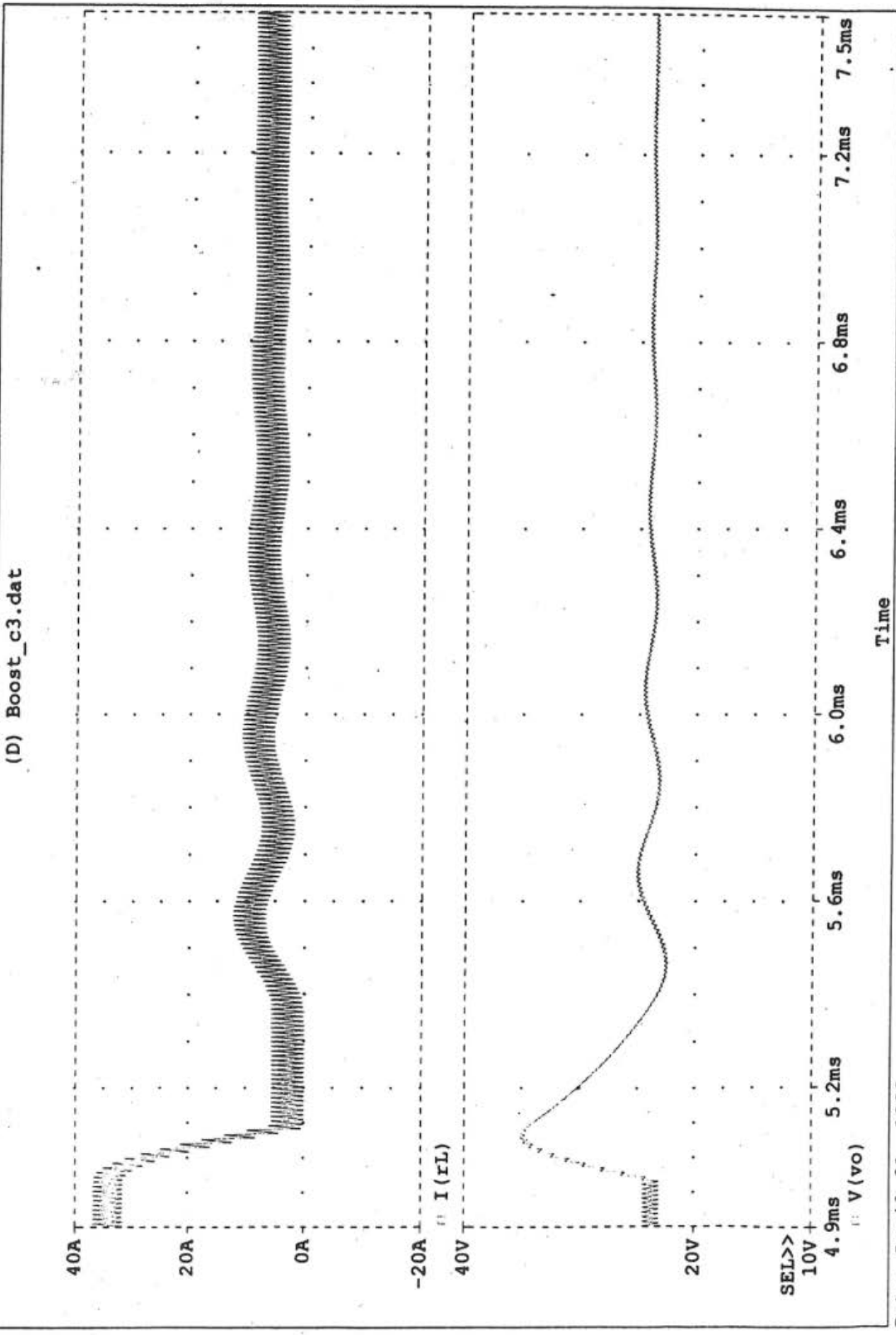
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Date/Time run: 04/01/99 23:12:43 \* C:\MSimEv\_8\Projects\BOOST\_AVG\_Switch\_c2.sch

Temperature: 27.0

(A) BOOST\_AVG\_Switch\_c2.dat



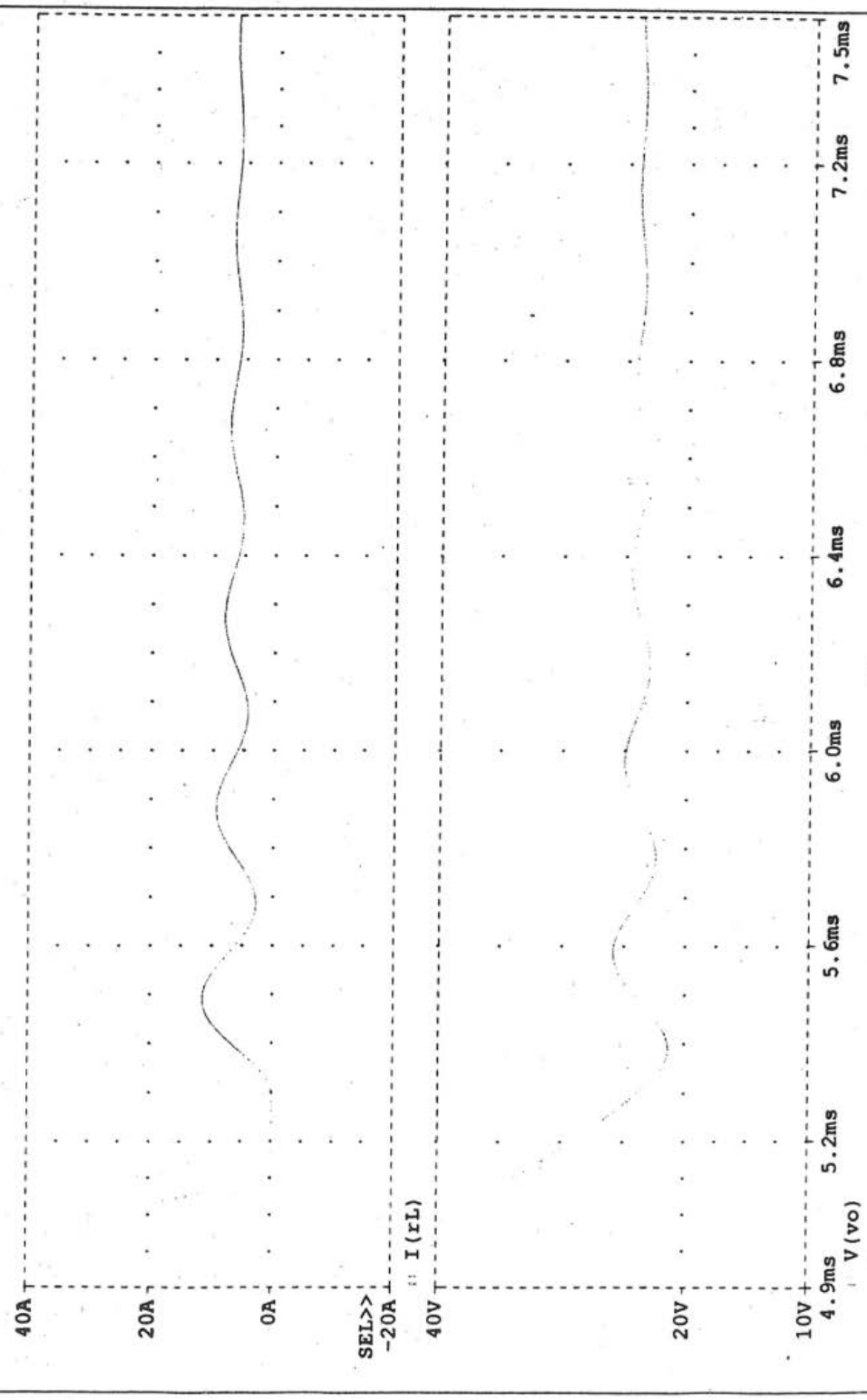


\* C:\MSimEv\_8\Projects\BOOST\_AVG\_Switch\_cl.sch

Temperature: 27.0

Date/Time run: 04/01/99 22:36:37

(C) BOOST\_AVG\_Switch\_cl.dat



Time

Date: April 01, 1999

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Time: 23:56:46

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