

Power Electronics Notes - D. Perreault

★ Control Design Example

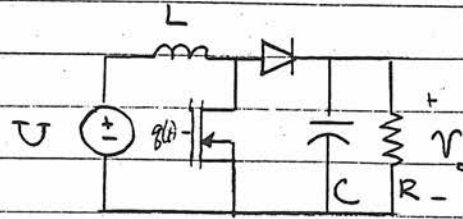
Boost Converter

$L = 10 \mu H$ $C = 50 \mu F$

$f_{sw} = 100 KHz$ $V_{o,ref} = 24 V$

$U_{nom} = 9V$, $8V < U < 10V$

$2 \Omega < R < 10 \Omega$



Start with switched equations of state:

$$\begin{cases} \frac{dI_L}{dt} = \frac{U}{L} g(t) + \frac{(U - V_o)}{L} (1 - g(t)) \\ \frac{dV_o}{dt} = -\frac{1}{RC} V_o g(t) + \left[\frac{1}{C} I_L - \frac{1}{RC} V_o \right] (1 - g(t)) \end{cases}$$

AVG.

State-space averaging with $\bar{x} = \frac{1}{T} \int_{t-T}^t x(\tau) d\tau$ results in nonlinear averaged model

$$\begin{cases} \frac{d\bar{I}_L}{dt} \approx \frac{1}{L} \bar{U} - \frac{1}{L} \bar{V} d' \\ \frac{d\bar{V}_o}{dt} \approx -\frac{1}{RC} \bar{V}_o + \frac{1}{C} \bar{I}_L d' \end{cases}$$

Linearize

Linearization about op point. U, I_L, V_o, D yields LTI linearized model of incremental dynamics

$$\begin{cases} \frac{d\tilde{I}_L}{dt} = \frac{1}{L} \tilde{U} - \frac{D'}{L} \tilde{V}_o + \frac{V_o}{L} \tilde{d} \\ \frac{d\tilde{V}_o}{dt} = -\frac{1}{RC} \tilde{V}_o + \frac{D'}{C} \tilde{I}_L - \frac{I_L}{C} \tilde{d} \end{cases}$$

$U = 9, V = 24, D = 0.625$
 $I_L = 25.6 A, R = 2.5 \Omega, C = 50 \mu F$
 $L = 10 \mu H$

$\tilde{V}_o / \tilde{d} = \frac{-512, 000 s + 1.8 \times 10^8}{s^2 + 80000 s + 2.81 \times 10^8}$

Zero @ $s = 35,156 \rightarrow$ explain!

LTI analysis

Using Laplace transform & Identity $\frac{V_o}{R} = D' I_L$

$$H(s) = \frac{\tilde{V}_o(s)}{\tilde{d}(s)} = \frac{-s \frac{V_o}{RC D'} + \frac{V_o D'}{LC}}{s^2 + \frac{1}{RC} s + \frac{D'^2}{LC}}$$

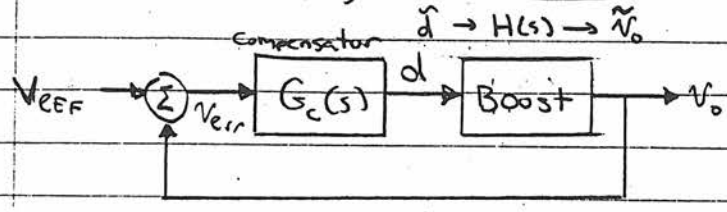
poles @ $s = -4000 \pm j16,279$
 period $\approx 0.4 ms$

Transfer Function depends on op. pt.

SEE TRANSIENT IN EX/2

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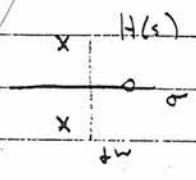
Back to original goal: Control!



Explain source of RHP zero

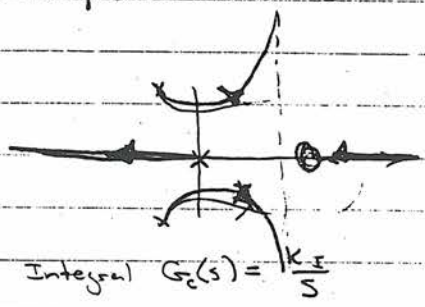
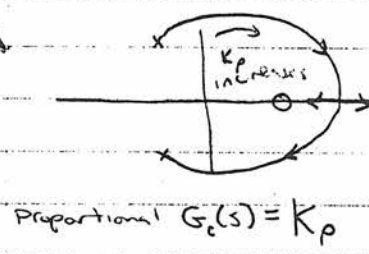
Looking at our transfer function, we have

1. 2 lightly-damped poles in LHP
2. 1 RHP zero



Note sign in numerator of H(s)

This is tricky, because the poles tend to move to the RHP under feedback:



→ So we must pick control gains that are not too high for stability.

Also, the poles move with operating point! (variations in U, R for example)

→ look at slide for variations of poles with R.

(problem becomes more difficult at light load...)

* → could use a damping leg ~~to~~ !! (neat trick)

must design controller valid over all operating points

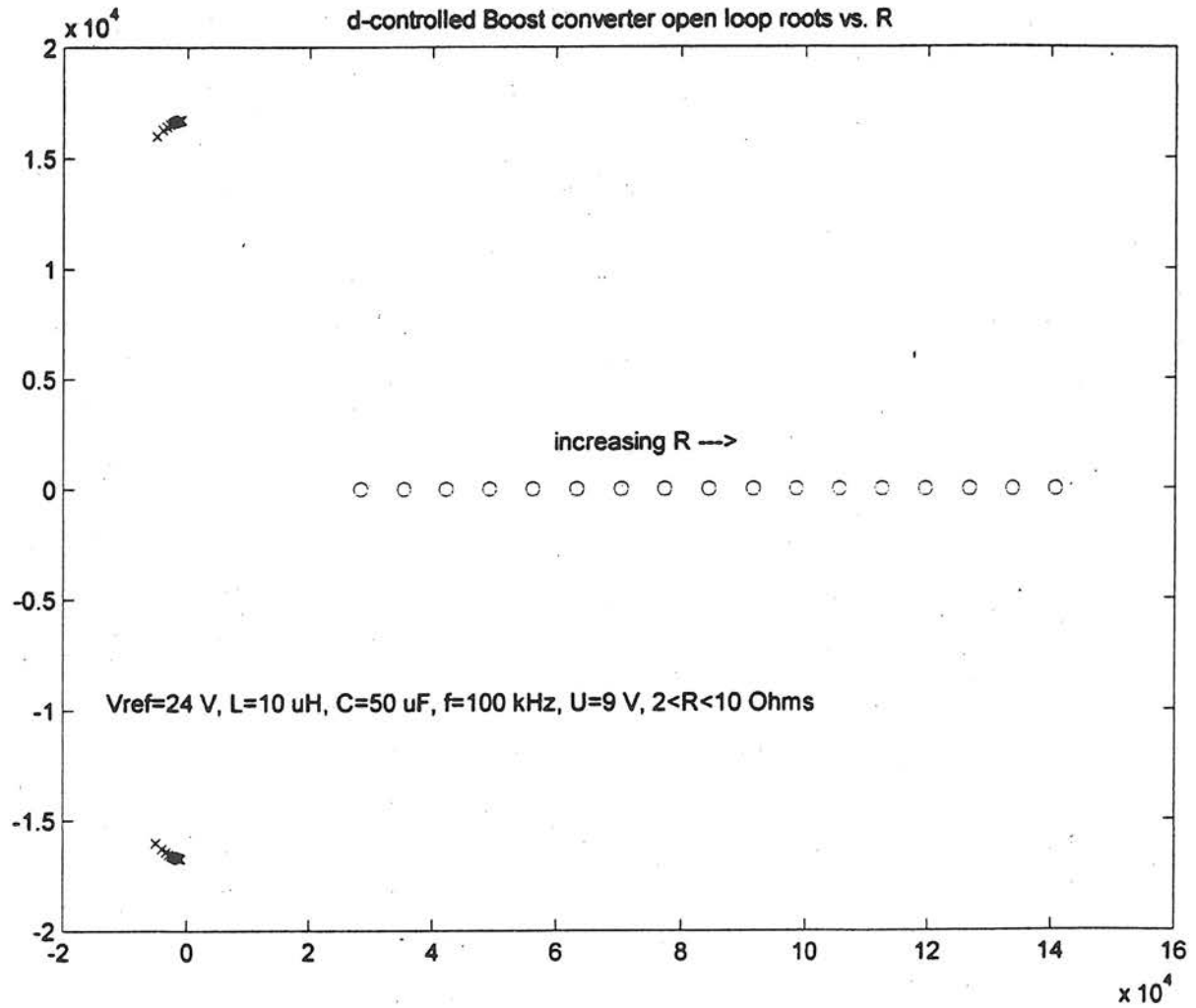
→ look at simple integral controller design

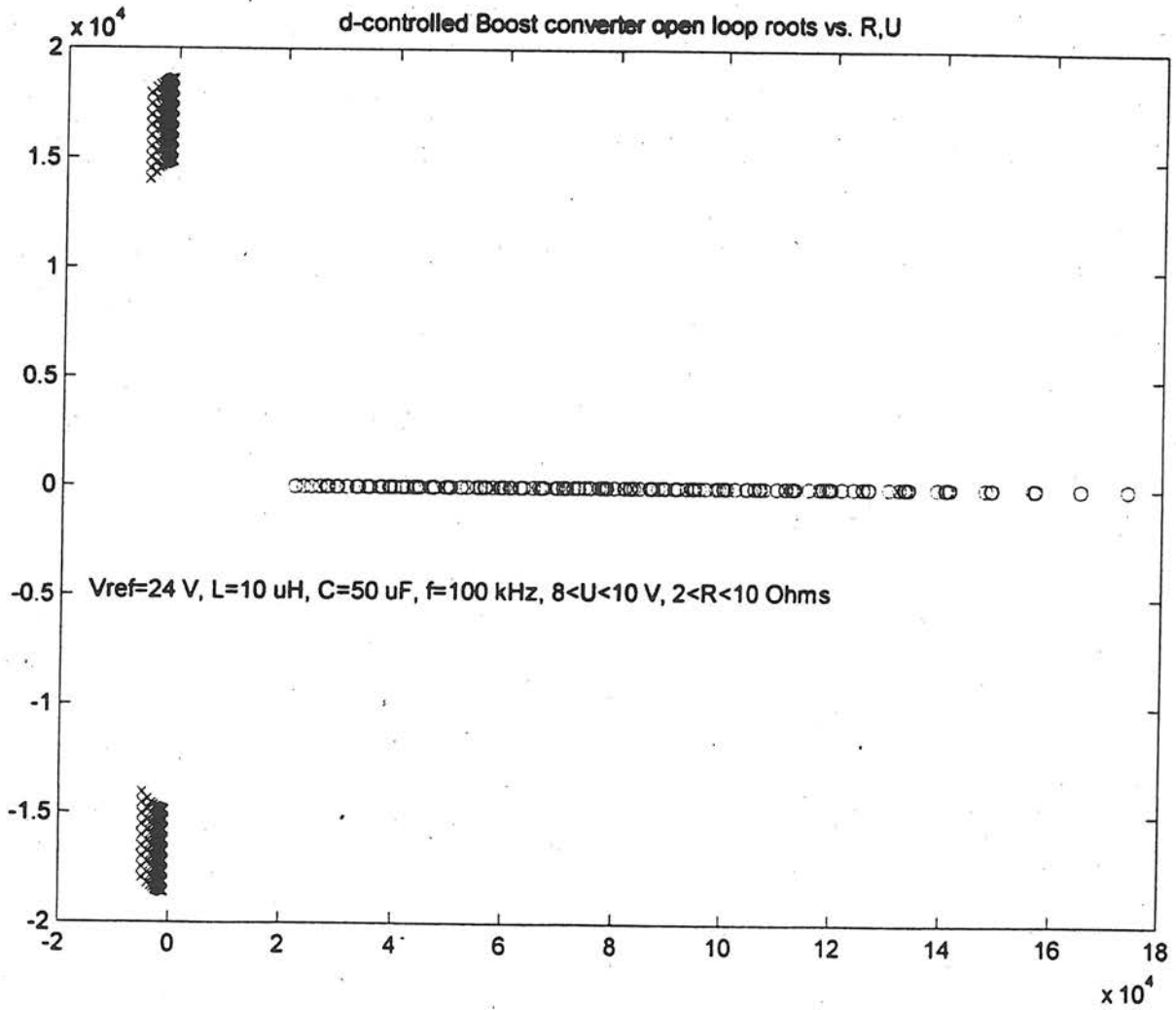
→ note: technically only small signal dynamics are determined, but power converters are forgiving in this respect.

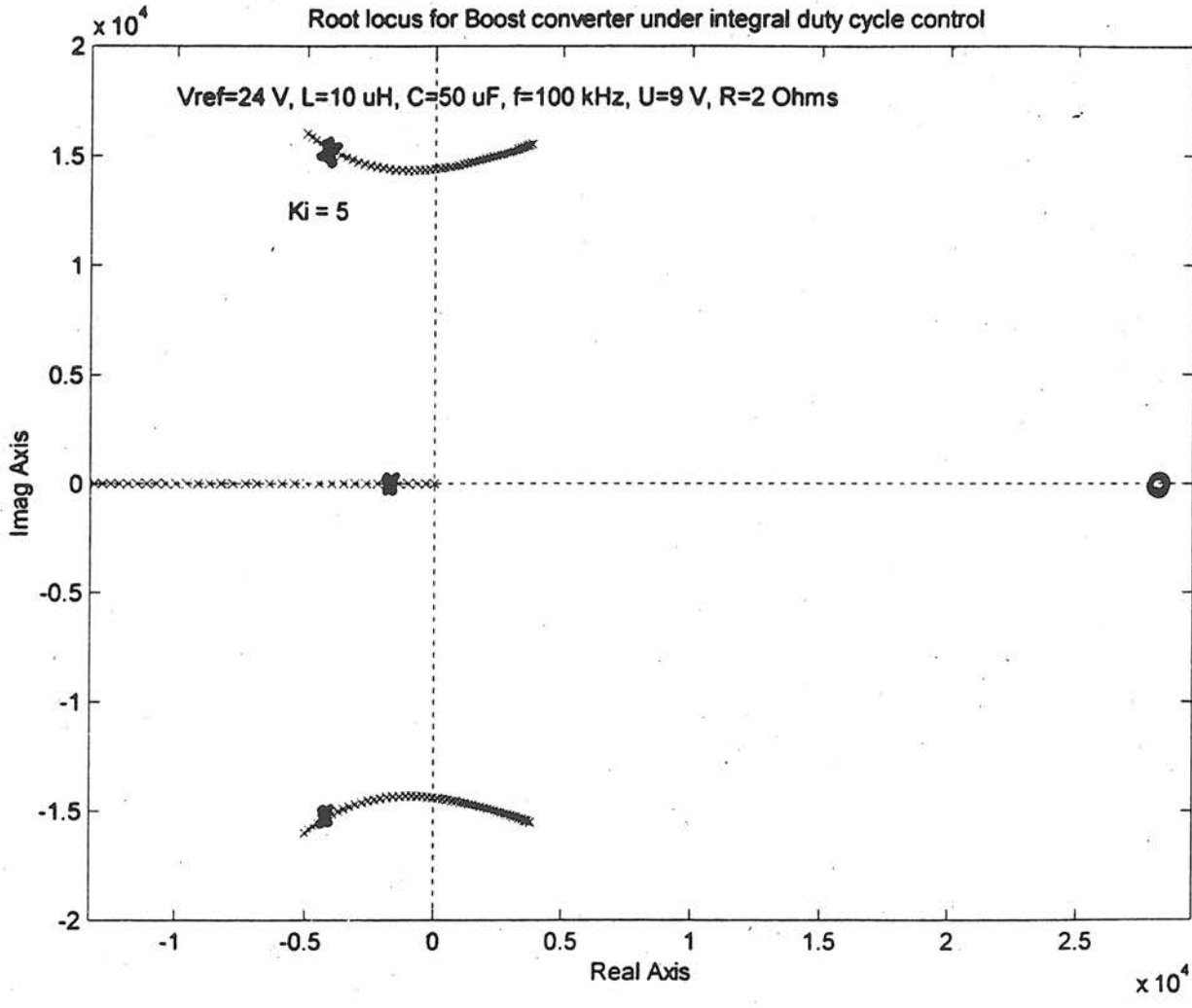
Note: This controller may not be ok in practice due to lightly-damped poles (noise sensitive, transient perf. etc.)

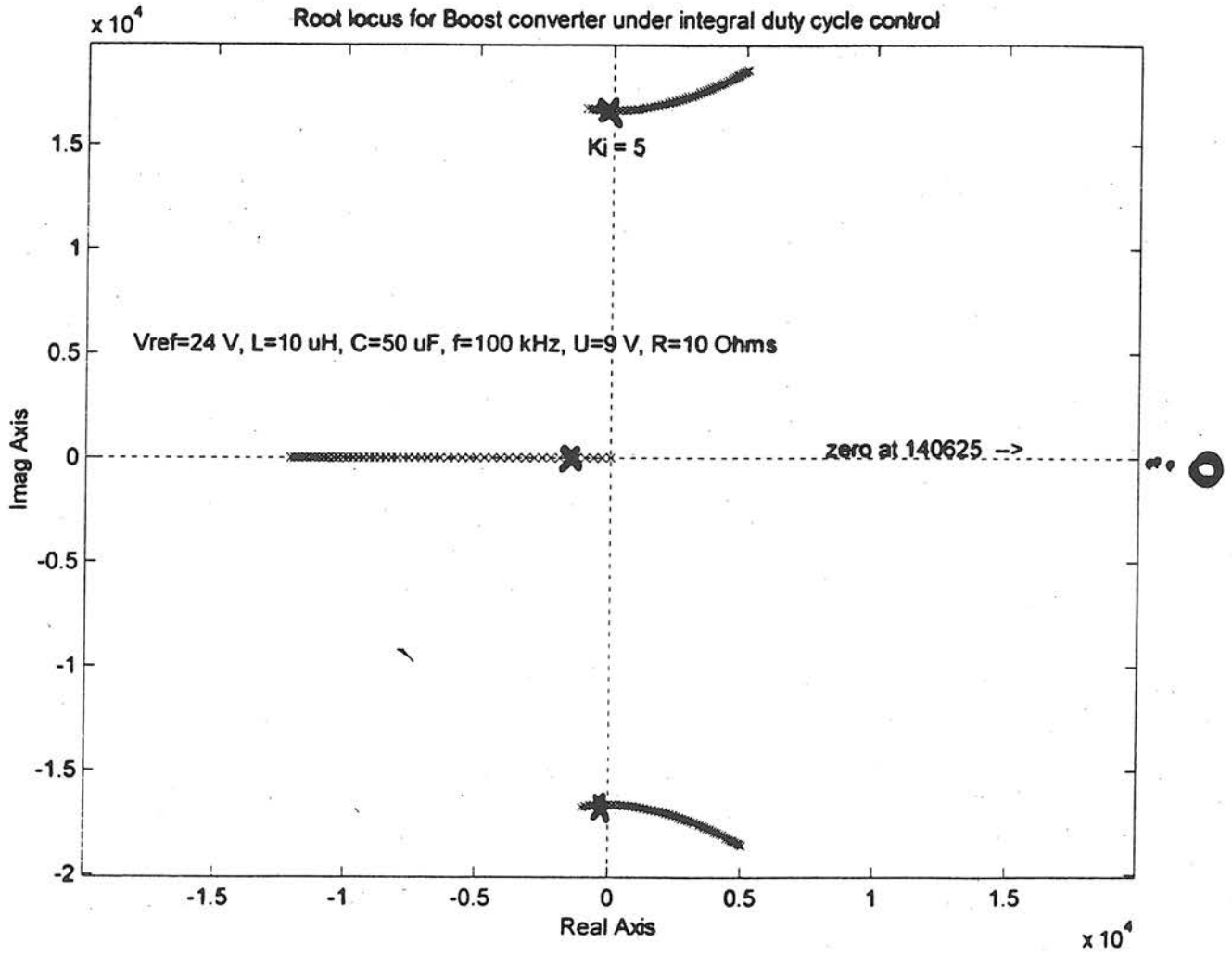
go to current mode control!

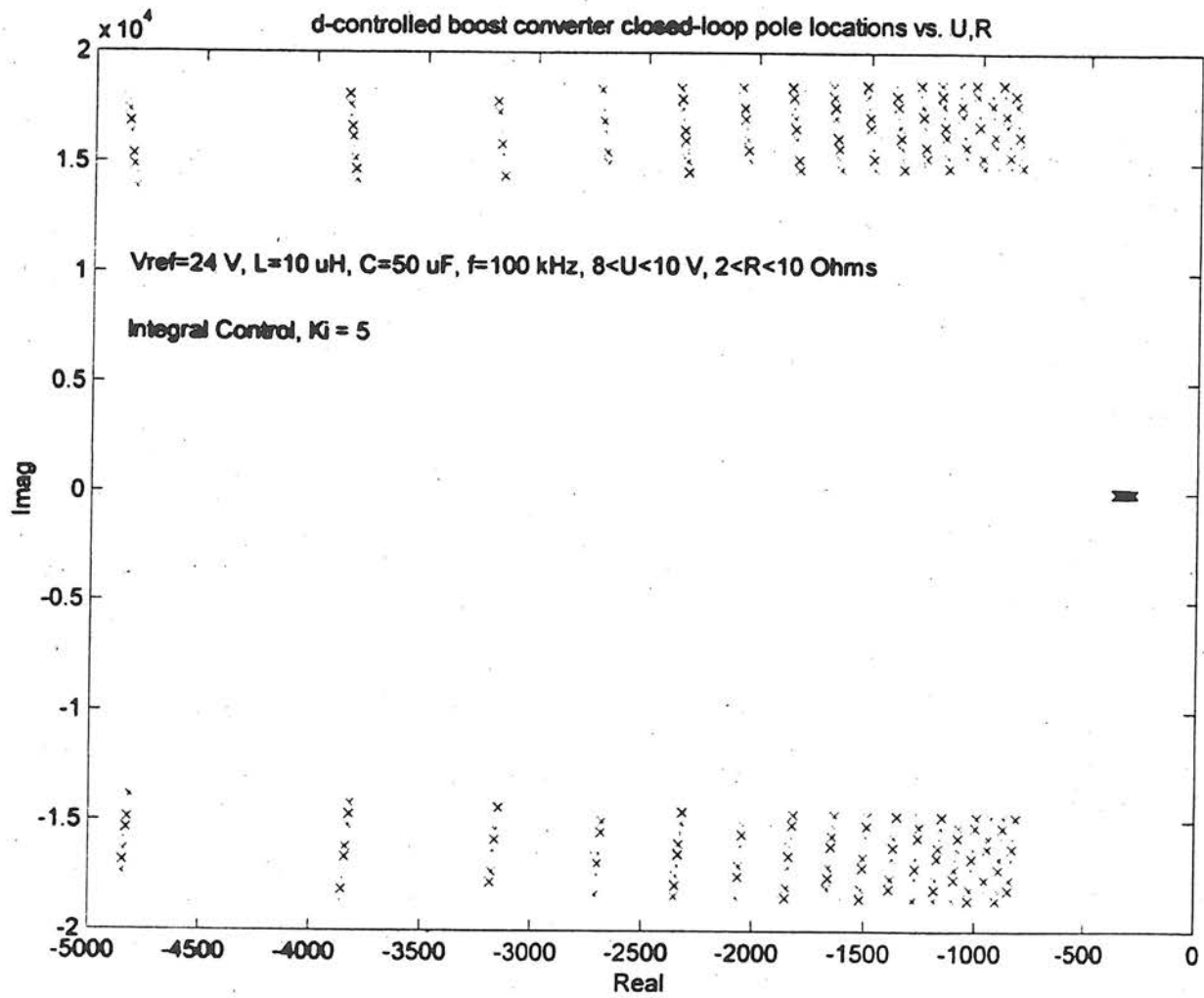
main prob is RHP zero!



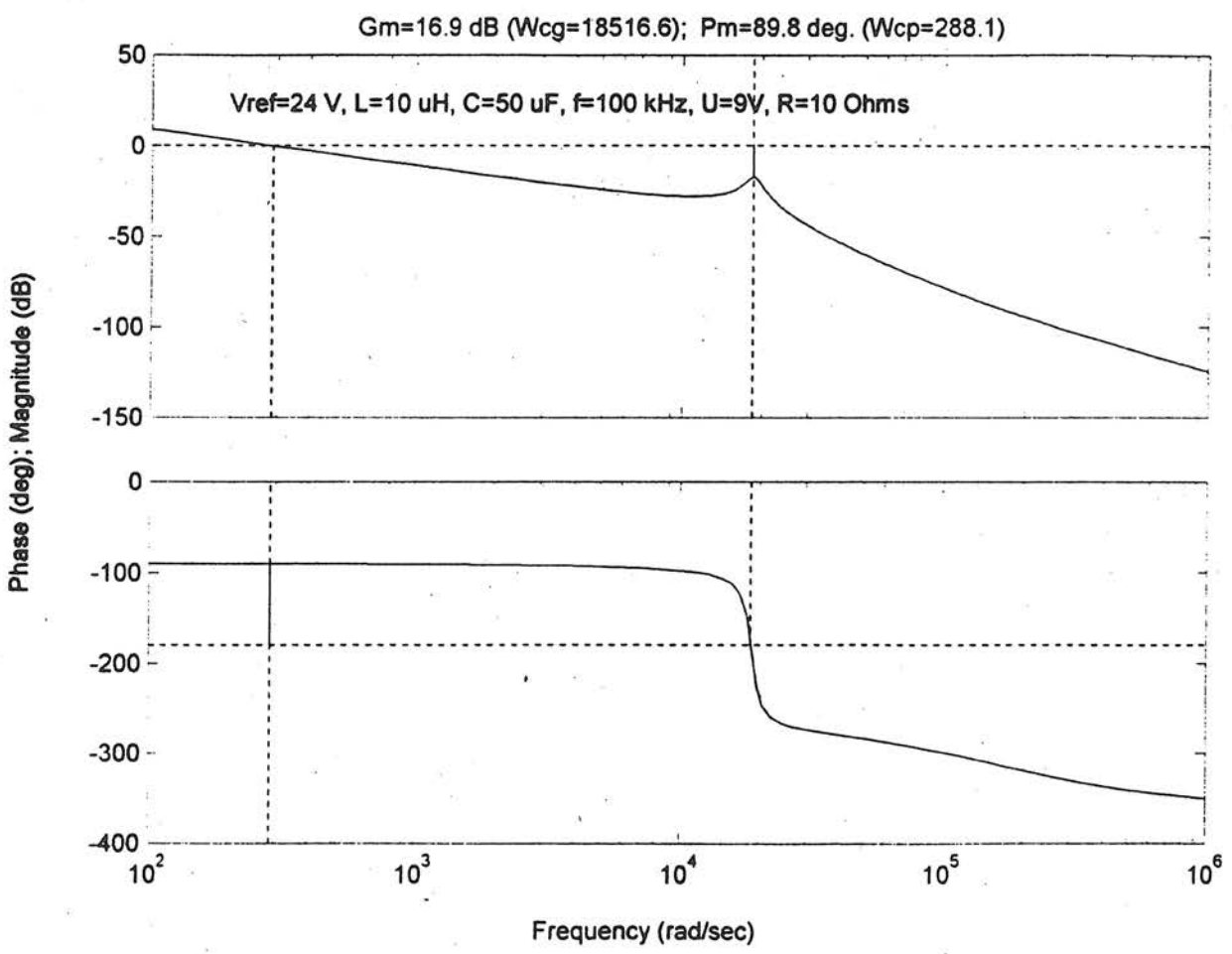








Bode Diagrams

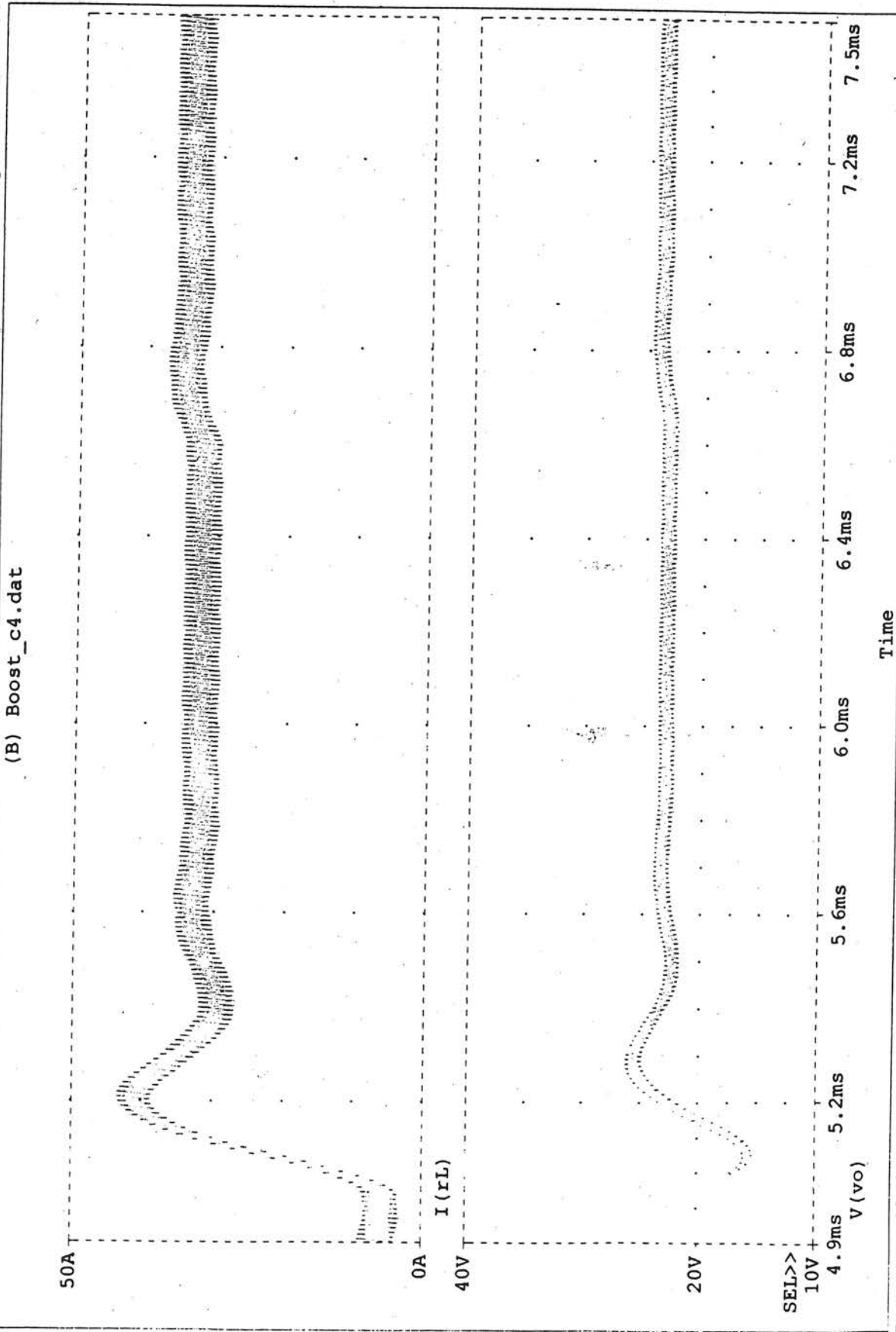


* C:\MSimEv_8\Projects\Boost_c4.sch

Temperature: 27.0

Date/Time run: 04/01/99 23:21:54

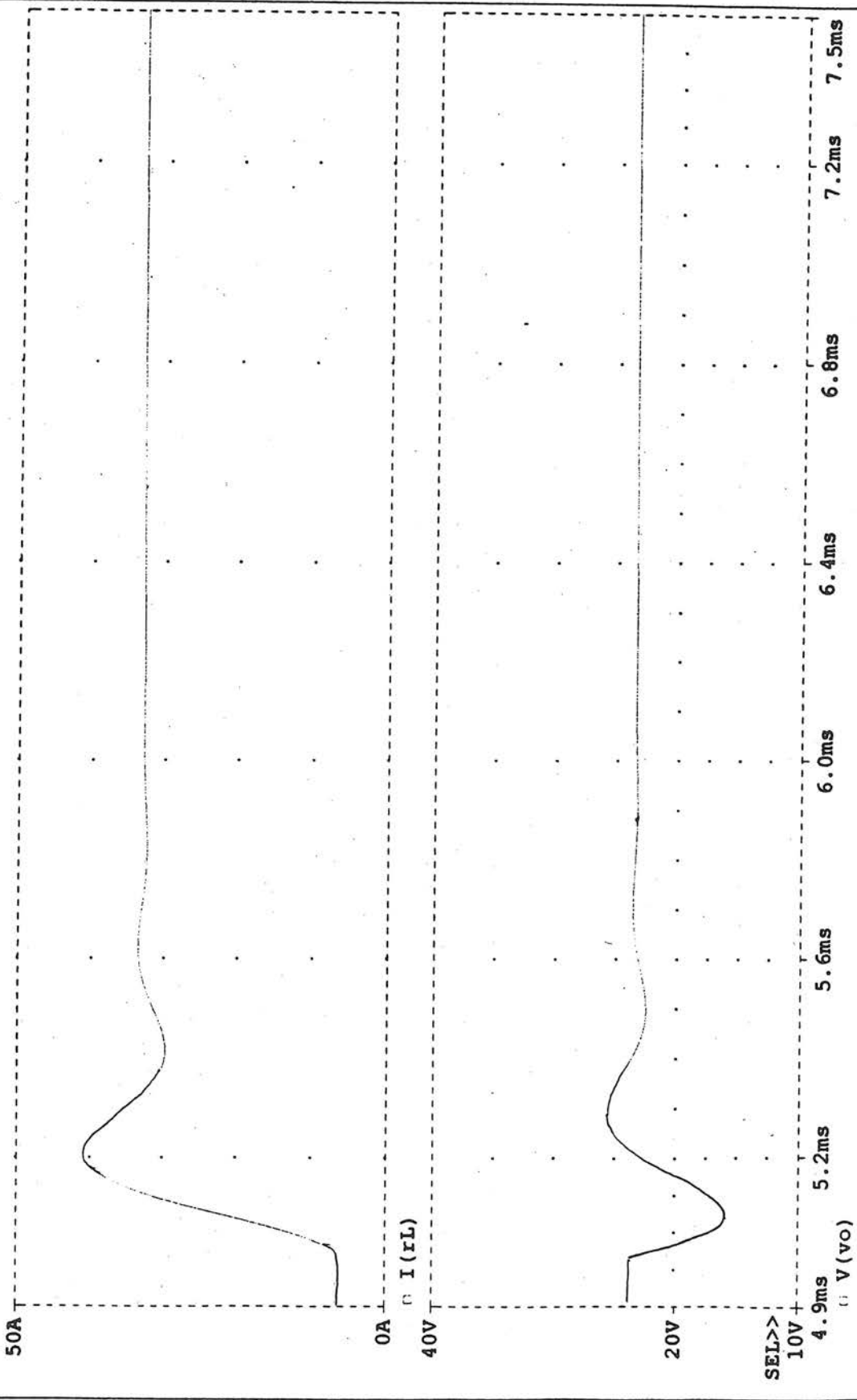
(B) Boost_c4.dat



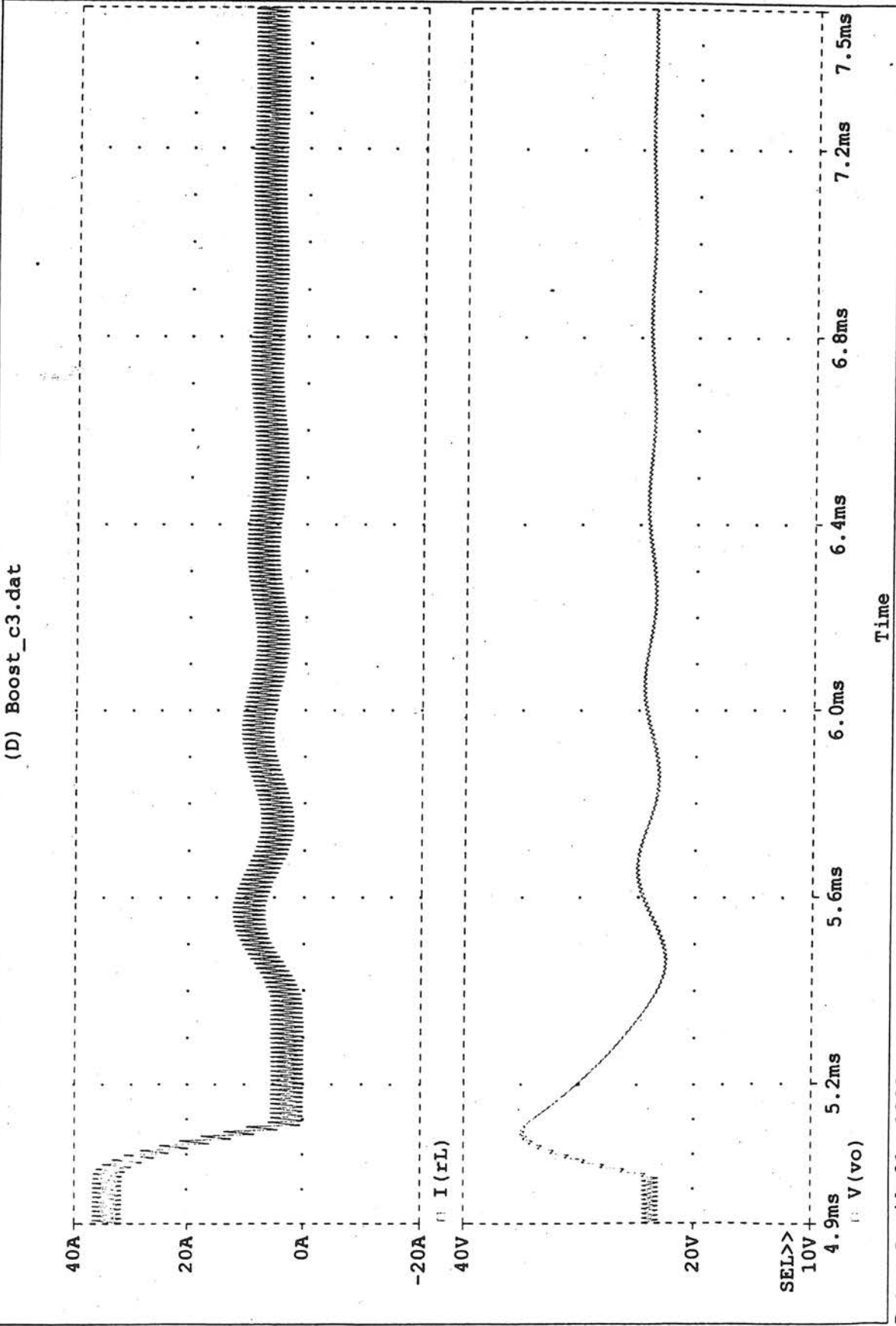
SEL>>
10V +
4.9ms 5.2ms 5.6ms 6.0ms 6.4ms 6.8ms 7.2ms 7.5ms
V(vo)

Time

(A) BOOST_AVG_Switch_c2.dat



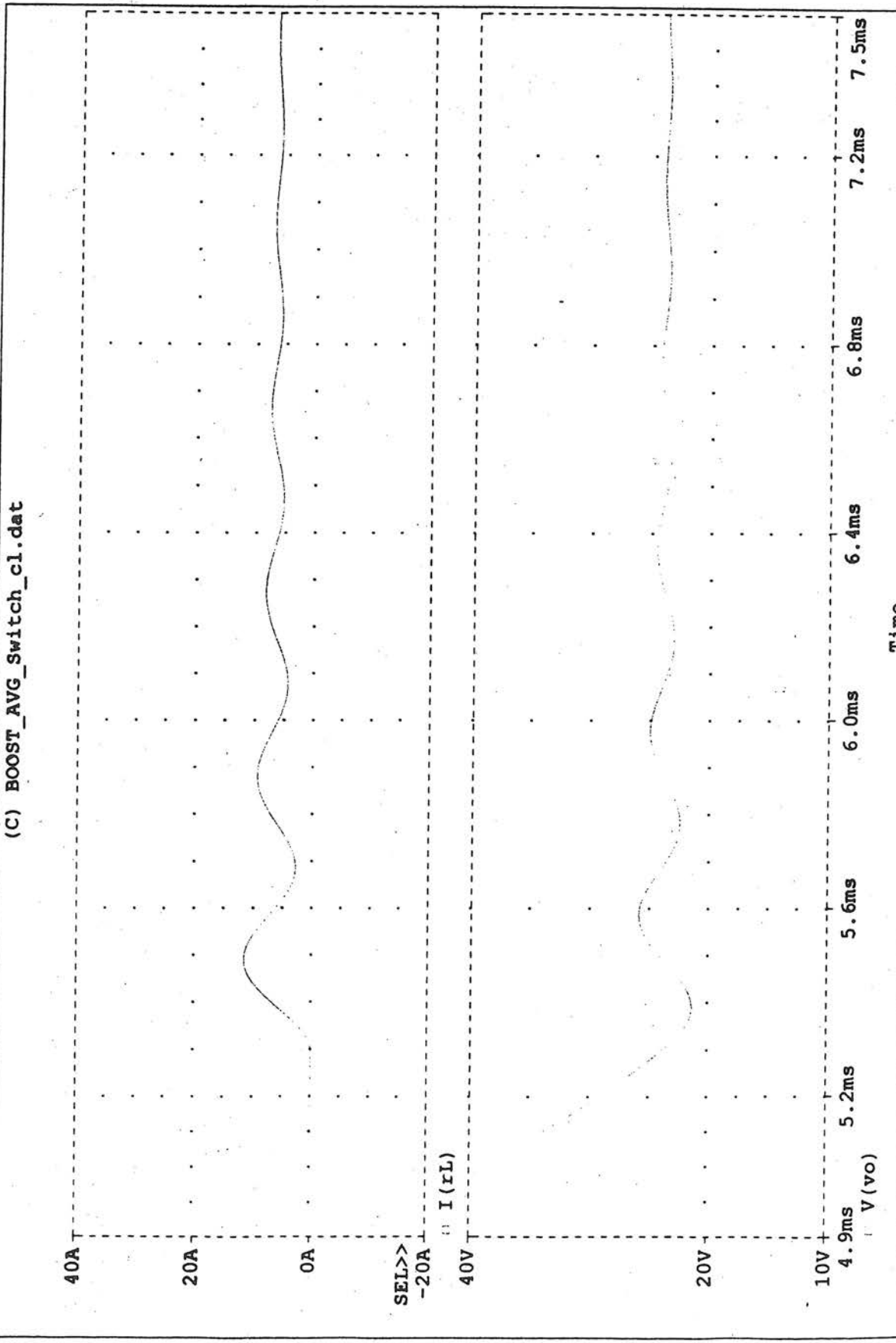
Time



Date/Time run: 04/01/99 22:36:37 * C:\MSimEv_8\Projects\BOOST_AVG_Switch_cl.sch

Temperature: 27.0

(C) BOOST_AVG_Switch_cl.dat



Time

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