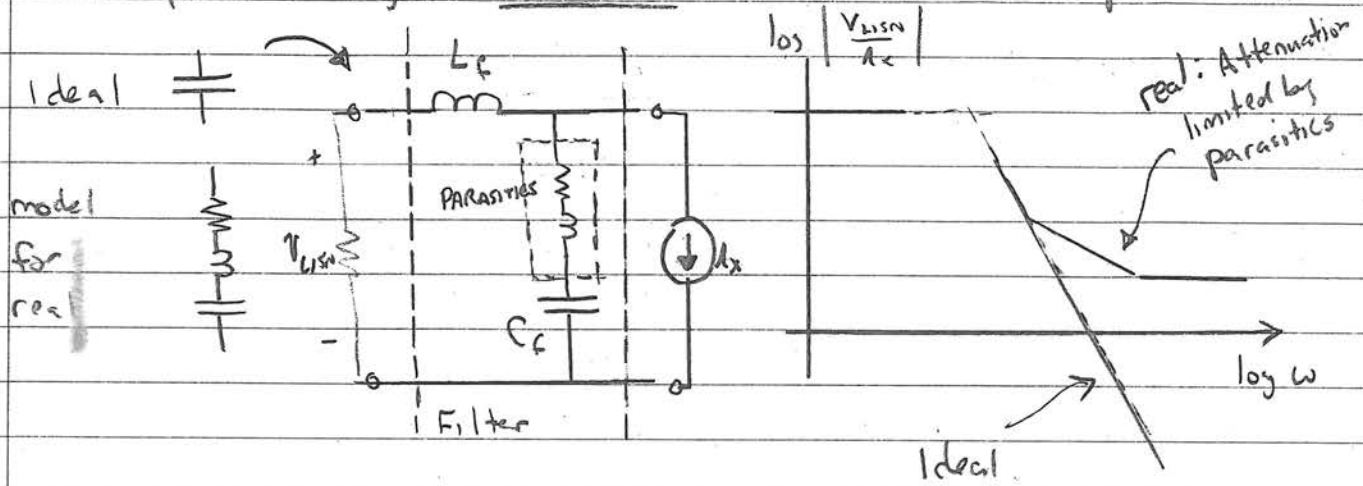


REVIEW : (VERY SHORT OR SKIP)

From last time, we saw that

① Component + Layout PARASITICS often limit filter performance



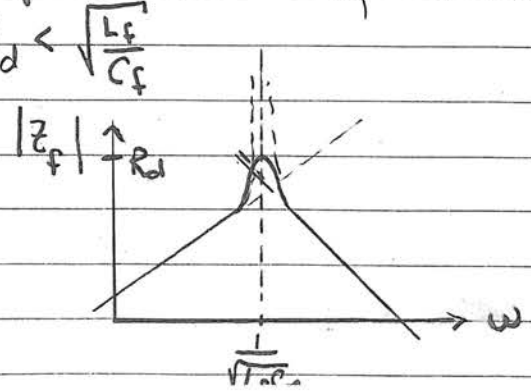
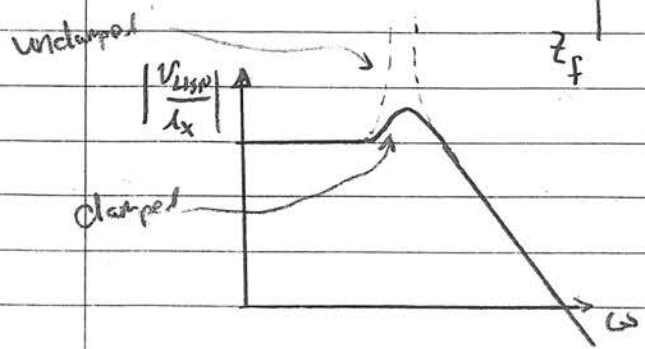
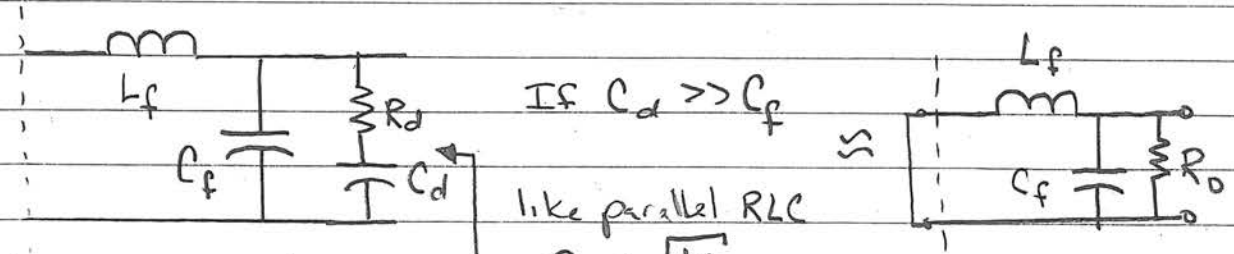
Inductor parasitic capacitance and parasitic L's, C's due to circuit layout can also limit performance

⇒ example of how layout capacitance across  $L_f$  was a major issue in one consulting design.

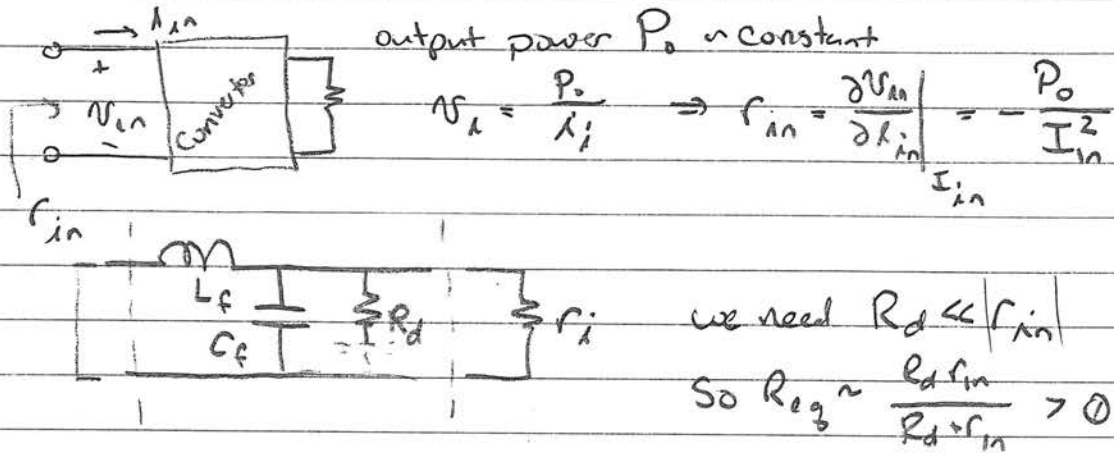
② Filter Damping is important

→ damp corner frequency of LC

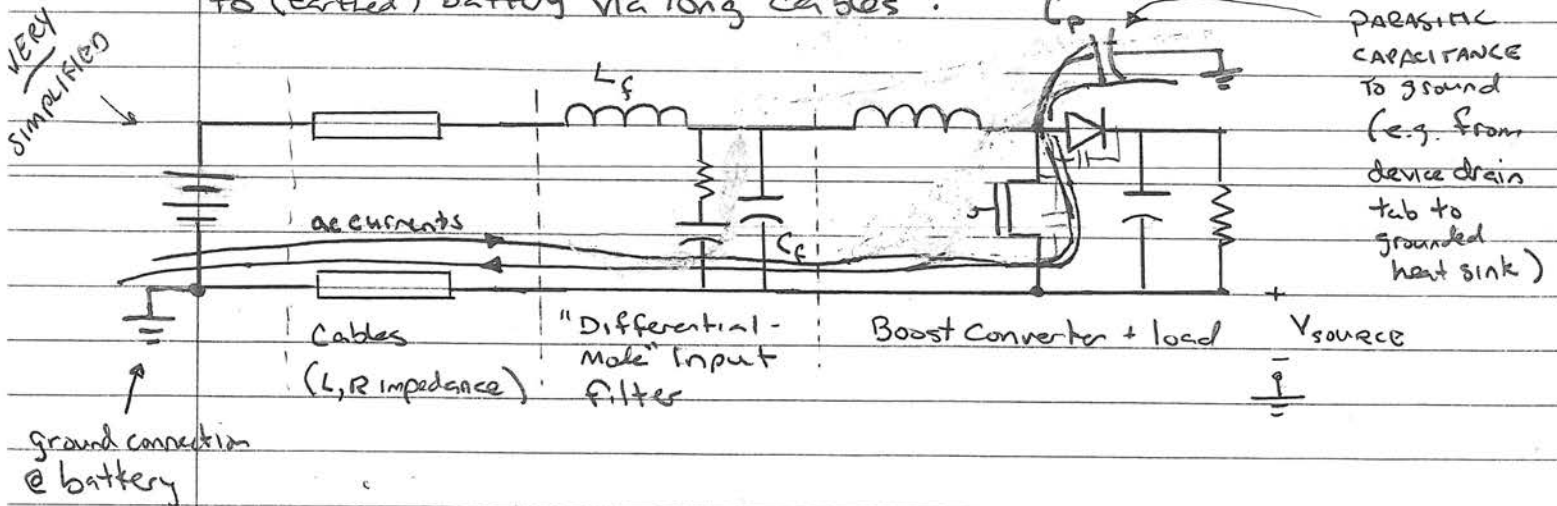
e.g. overdamping method:



Input filters often need extra damping, because closed-loop converters provide incremental "negative resistance" that tends to destabilize the input filter:



Simple example to introduce notion of common-mode + differential mode noise: Filtered boost converter connected to (Earthed) battery via long cables:



- First describe input currents without parasitic capacitance (well filtered by  $L_f, C_f$ ) and little high-frequency "bounce" in  $V_s$
- With parasitic capacitance  $C_p$ , the lower cable (return) sees high-frequency current, and  $V_{source}$  "bounces" substantially from ground at high frequency,

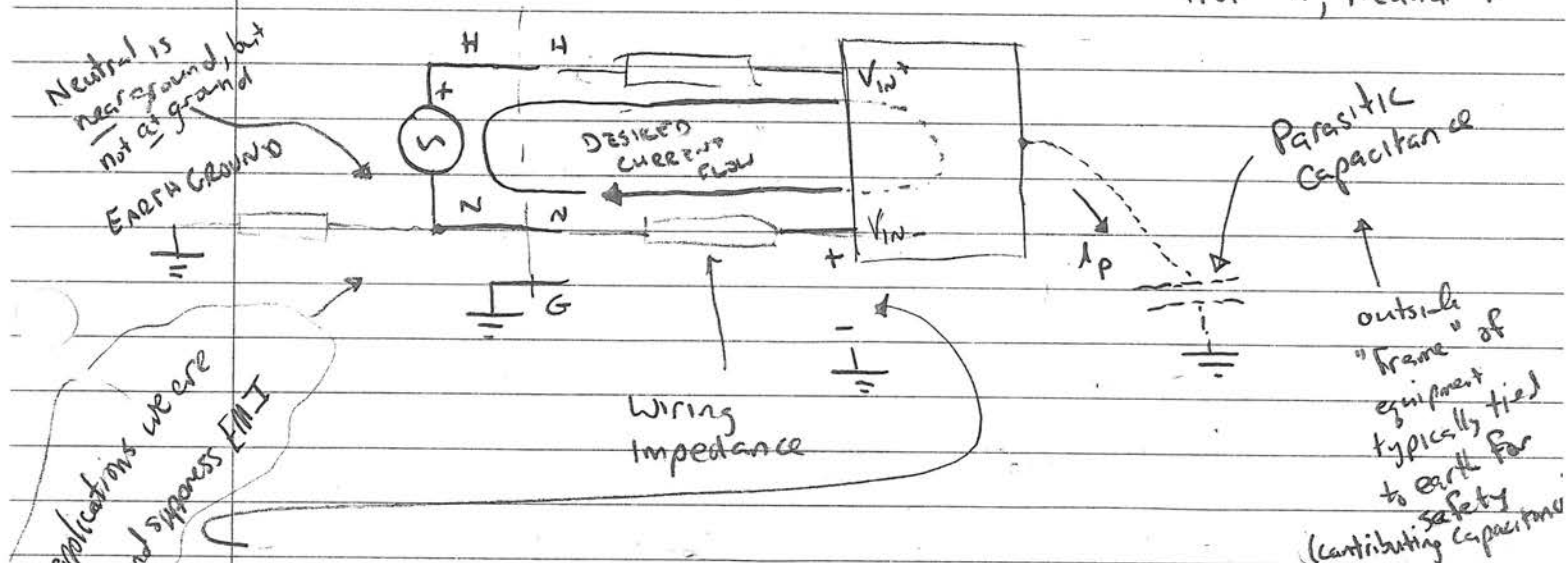
6.334 Lecture Notes

EMI Filters #3: CM + DM

COMMON MODE + DIFFERENTIAL MODE :

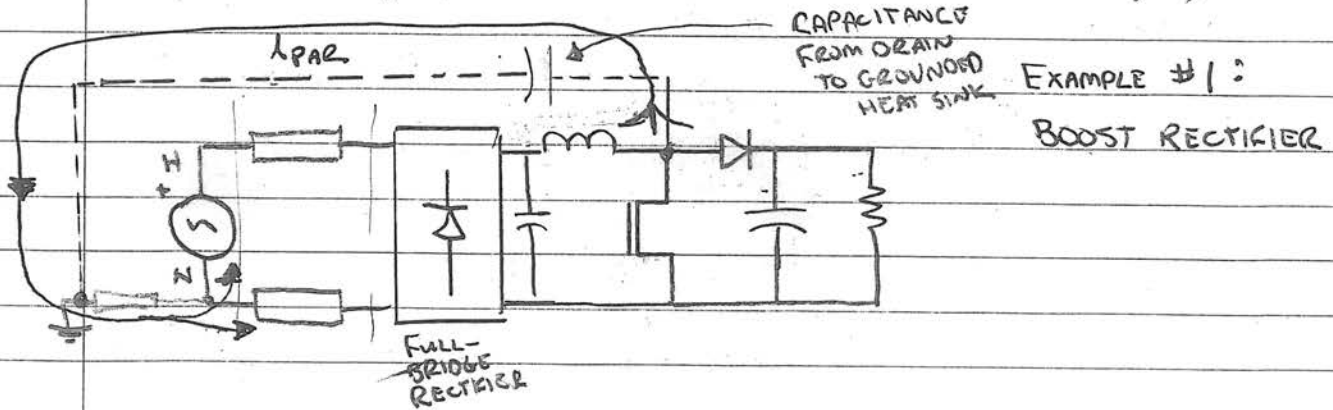
The filter strategies shown thus far are appropriate when all circuits are well connected to earth ground and supplied from a ground referenced input. However, this is not exactly the case in many applications!

e.g. Systems connected to the ac line : Converter connected to "Hot" H, "Neutral" N



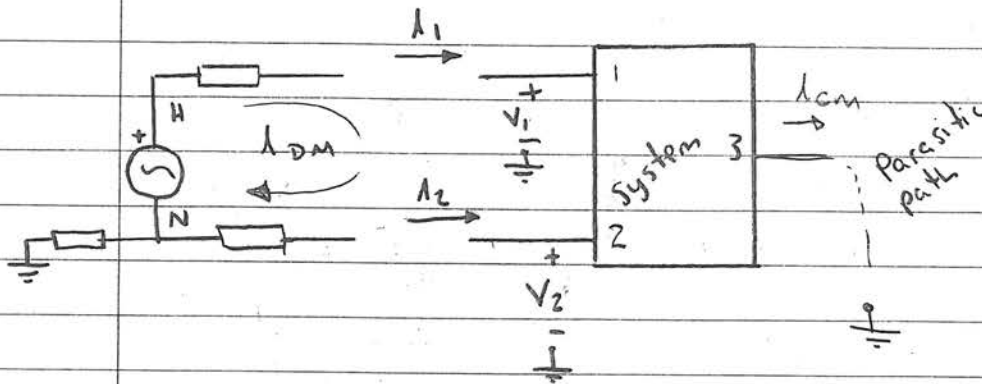
note: in ac-line applications we are required to measure and suppress EMI in both Hot + Neutral!

- We can have voltage differences between  $V_{in-}$  (Connected to N) and gnd (and  $V_{in+}$  and gnd)
- Thus current can flow through parasitic impedances (e.g. capacitance) back through earth ground, and return along paths we don't desire (not via H, N)



CM Example #2: MOTOR DRIVES often have a high capacitance from the windings (driven by converter) to the grounded frame.

How can we describe the different voltages and currents?



$$\left\{ \begin{array}{l} \text{differential-mode current} \\ \text{Common-mode current} \end{array} \right. \left. \begin{array}{l} i_{DM} = \frac{i_1 - i_2}{2} \\ i_{CM} = i_1 + i_2 \end{array} \right\} \therefore \begin{array}{l} i_1 = i_{DM} + \frac{1}{2} i_{CM} \\ i_2 = -i_{DM} + \frac{1}{2} i_{CM} \end{array}$$

The differential-mode current flows into terminal 1 and back out terminal 2 (as expected). The common-mode current flows equally into terminals 1, 2, and returns through the parasitic path (via "terminal 3")

We can also specify common + differential-mode voltages

$$\left\{ \begin{array}{l} \text{differential-mode voltage} \\ \text{Common-mode voltage} \end{array} \right. \left. \begin{array}{l} v_{DM} = v_1 - v_2 \\ v_{CM} = \frac{v_1 + v_2}{2} \end{array} \right\} \begin{array}{l} v_1 = v_{CM} + \frac{1}{2} v_{DM} \\ v_2 = v_{CM} - \frac{1}{2} v_{DM} \end{array}$$

These definitions are useful, since we use different techniques to solve common-mode + differential mode noise problems.

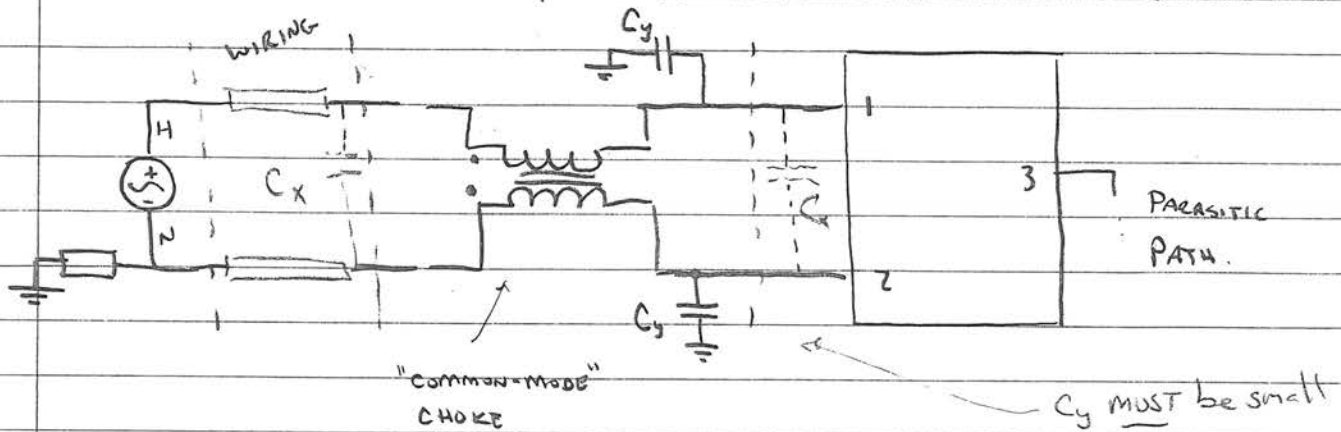
⇒ Why? e.g. placing a capacitor from 1-2 ("differentially") will not suppress common-mode current or voltage ripple at all! Other methods prevail.

6.334 Lecture Notes

EMI Filters #3: CM + DM

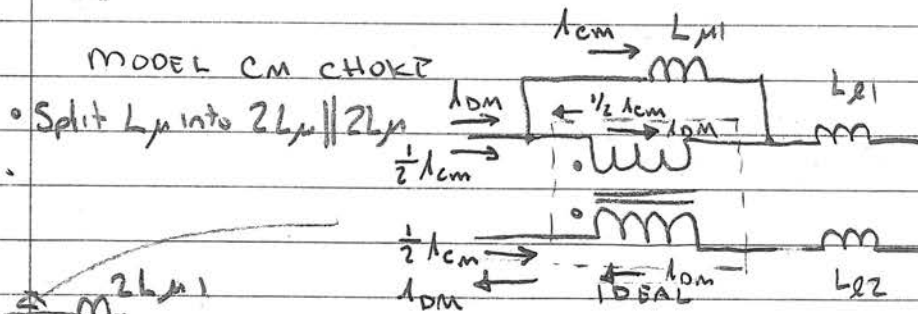
WE ARE REQUIRED TO NOT INJECT COMMON OR DIFFERENTIAL-MODE CURRENT BACK INTO THE LINE.

CONSIDER A MEANS TO SUPPRESS COMMON-MODE CURRENT (from line wiring)

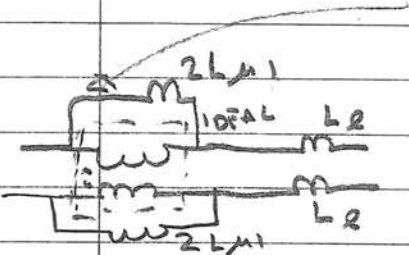


Common-mode choke is a transformer that tries to suppress common-mode currents (current "into one dot must flow out the other")

MODEL CM CHOKE



• Split  $L_p$  into  $2L_p \parallel 2L_p$



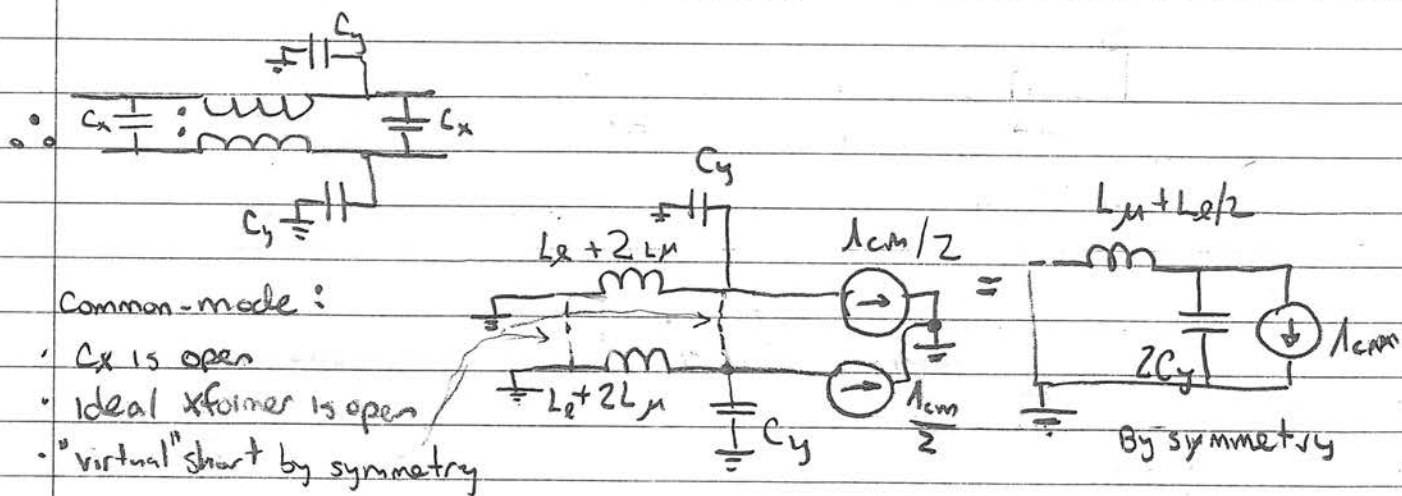
- Differential-mode current flows through ideal transformer, small leakage inductances
- Common-mode current must flow through BIG magnetizing inductance  $L_\mu$ . Core size/energy storage does not depend on  $I_{DM}$  (big @ high power), only on  $I_{CM}$ , which we always want to be small!



- So a common mode choke presents a very high impedance to common mode current flow. We get large inductance to CM from a small core, since CM currents are small.
- This is important, since we are only allowed to add tiny ( $< 10\text{nF}$ ) common-mode capacitors  $C_y$  to ground (to keep  $I_{cm}$  from flowing out to the line.) This is due to safety "leakage" current limits

To suppress Differential-mode currents, we can add large differential mode capacitors as described previously. (use "X" capacitors for ac-line applications)

The leakage inductances from the common-mode choke can form some or all of the differential-mode filter inductance



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