

Power Electronics Notes - D. Perreault

★★ RESONANT POWER CONVERSION

In many power converter applications, one converts between dc and high-frequency sinusoidal ac (either as an intermediate or final waveform). Applications include:

1. RF Power amplifiers for communications, radar, etc.
2. High frequency inverters for induction heating
3. "Resonant" dc/dc converters using high-frequency sinusoidal intermediate waveforms + energy storage
4. Electronic ballasts for lighting
5. Power converters using resonant energy storage/transformer structures (e.g. piezoelectric "electromechanical" transformers)

Here we consider topologies, designs + control methods that are suited to these applications. These applications share certain objectives:

1. High-frequency sinusoidal ac waveforms
2. A desire for high-efficiency power conversion.

But

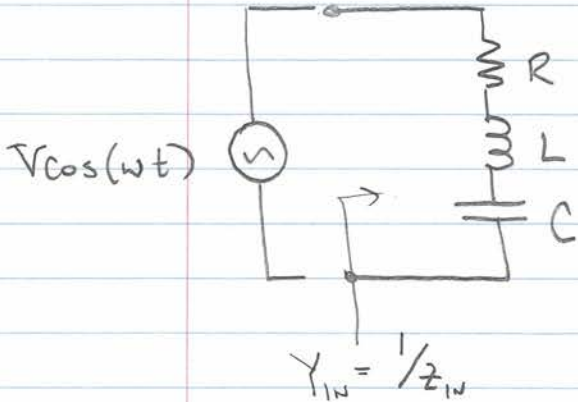
Different applications have different requirements:

1. Load characteristics (narrow, well-known range vs. wide load variations)
2. Need for or absence of regulation + control of output
3. high sinusoidal waveform purity (required or not)

NOTE: THIS YEAR, FIRST LECTURE COVERS ONLY RESONANT CIRCUITS REVIEW.

REVIEW OF RESONANT CIRCUITS

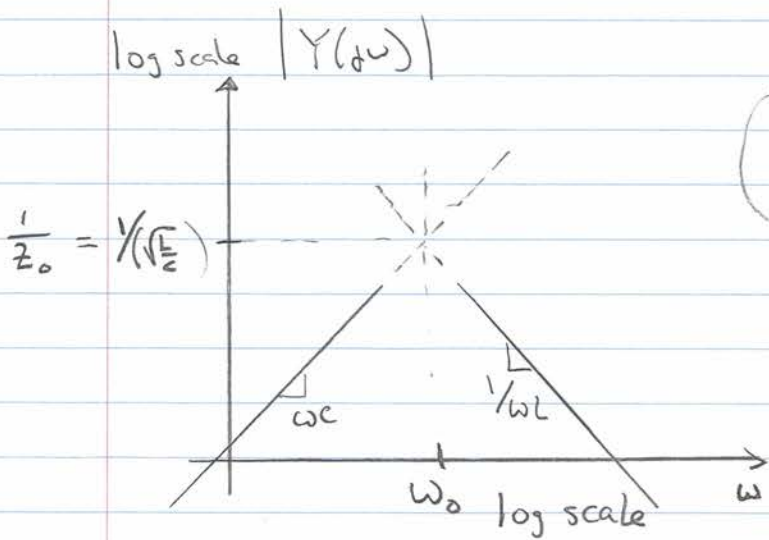
Consider a second-order series-resonant tank



$$Y_{IN} = \frac{1}{R + j\omega L + \frac{1}{j\omega C}} = \frac{1}{R + j(\omega L - \frac{1}{\omega C})}$$

$$|Y_{IN}| = \frac{1}{\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}}$$

$$\angle Y_{IN} = -\text{ATAN}\left(\frac{\omega L - \frac{1}{\omega C}}{R}\right)$$



(imaginary w/ opposite sign)

@ low frequency capacitor limits admittance $Y_{IN} \approx j\omega C$

@ high frequency inductor limits admittance $Y_{IN} \approx \frac{1}{j\omega L} = -\frac{j}{\omega L}$

@ some intermediate frequency the impedances of L, C are equal and opposite

$$j\omega L - \frac{j}{\omega C} = 0 \Rightarrow \omega = \omega_0 = \frac{1}{\sqrt{LC}}$$

ω_0 : "Undamped natural frequency"

@ ω_0 : $|Z_L| = \omega_0 L = \sqrt{\frac{L}{C}}$, $|Z_C| = \frac{1}{\omega_0 C} = \sqrt{\frac{L}{C}}$

$$Z_0 \triangleq \sqrt{\frac{L}{C}}$$

* -> NOTE $|V_C(\omega_0)| = \frac{|I_L|}{\omega C} = \sqrt{\frac{L}{C}} \cdot |I_L| = Z_0 |I_L| \Rightarrow Z_0$ relates $|V_C|$ to $|I_L|$ @ ω_0 !

"CHARACTERISTIC IMPEDANCE"

G.334 Lecture Notes

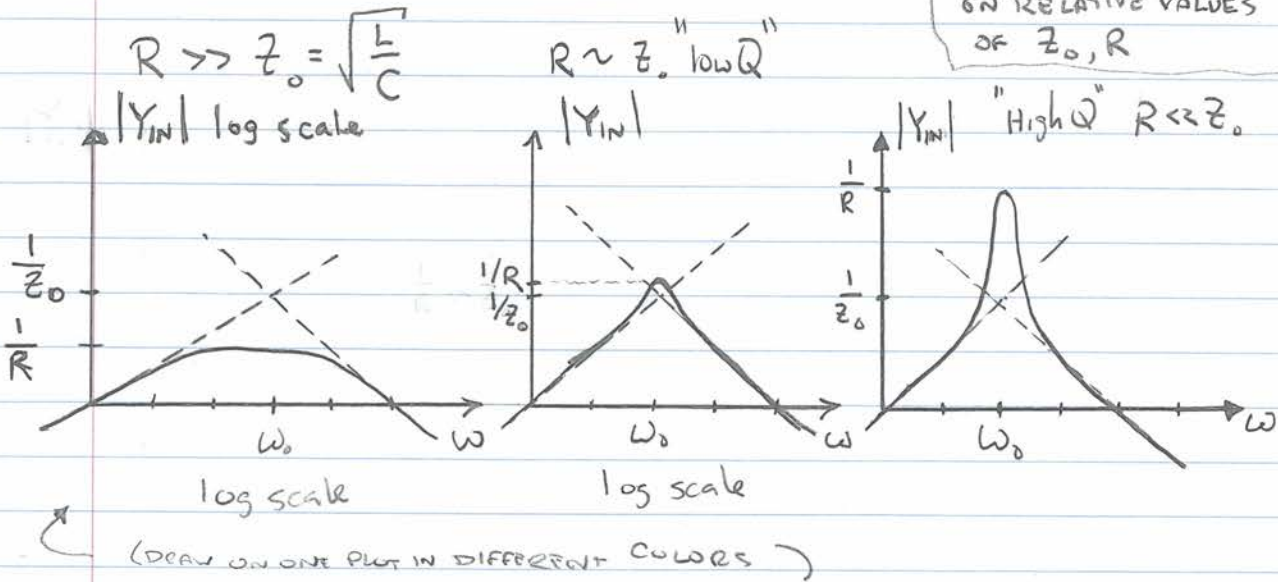
Resonant Power Conversion #1

what happens near $\omega = \omega_0$?

@ $\omega = \omega_0$ $Y_{IN} = \frac{1}{R}$ (L, C impedances cancel)

∴ Three possible cases

THE BEHAVIOR DEPENDS ON RELATIVE VALUES OF Z_0, R

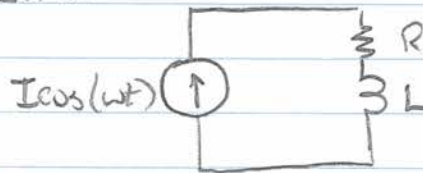


WE OFTEN DISCUSS THE "Q" or "quality factor" of a system. The quality factor is proportional to the peak ^(ac) energy stored to the energy dissipated in an ac cycle

$$Q \triangleq 2\pi \frac{\text{PEAK ENERGY STORED}}{\text{ENERGY DISSIPATED}}$$

example: a series RL circuit

$$E_{\text{STORED}} = \frac{1}{2} L I^2$$



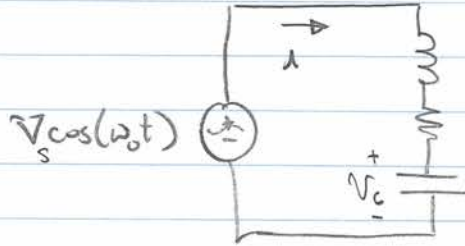
$$E_{\text{DISS}} = \left(\frac{1}{2} I^2 R\right) (T) = \left(\frac{1}{2} I^2 R\right) \cdot \frac{2\pi}{\omega} = \frac{\pi I^2 R}{\omega}$$

$$\Rightarrow Q = 2\pi \cdot \frac{L_0 I^2 \omega}{R I^2 2\pi} \Rightarrow Q = \frac{\omega L}{R}$$

lets consider the Q of the series LRC @ $\omega = \omega_0$

$$i(t) = \frac{V_s}{R} \cos(\omega_0 t)$$

From before @ $I = \frac{V}{R}$



$$E_{Diss} = \frac{\pi V_s^2}{\omega_0 R}$$

@ ω_0 i_L, V_c 90° out of phase $\therefore i_L, p_k$ @ $V_c = 0$.

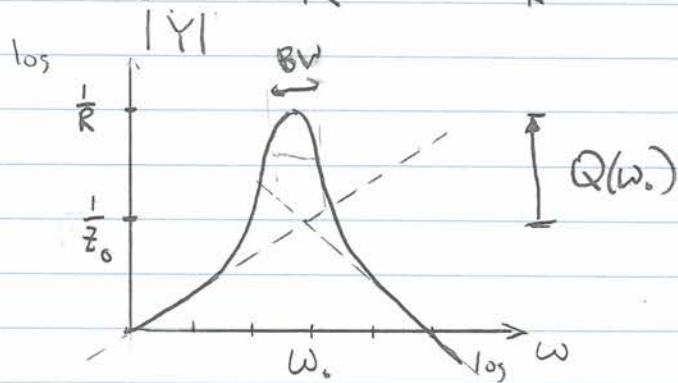
$$E_{Stored} = \frac{1}{2} L \left(\frac{V_s}{R} \right)^2 = \frac{1}{2} \frac{L V_s^2}{R^2}$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

ENERGY STORED
TO ENERGY LOST
@ $\omega = \omega_0 = Z_0/R$

$$\therefore Q(\omega_0) = 2\pi \frac{L V_s^2}{2R^2} \cdot \frac{\omega_0 R}{\pi V_s^2} = \frac{\omega_0 L}{R} = \frac{\sqrt{L/C}}{R} = \frac{Z_0}{R}$$

So, considering our plot:



- ① THE RESONANCE PEAKS UP THE ADMITTANCE (DUE TO L,C CANCELLATION) BY A FACTOR

$$Q(\omega_0) = \frac{Z_0}{R} !$$

- ② Consider the voltage gain from source voltage V_s to peak capacitor voltage $|V_c|$ at drive frequency $\omega = \omega_0$.

$$V_{c, pk} = \frac{I}{\omega_0 C} = \frac{V_s}{R \cdot \omega_0 C} = V_s \frac{Z_0}{R} = V_s \cdot Q(\omega_0)$$

\therefore for large Q (@ ω_0) we can get large voltage gain from resonance.

This is often used in practice (e.g. for "striking" the lamp in a lamp ballast.)

③ Consider the "Bandwidth" over which large resonant peaking occurs. We will consider the bandwidth (or frequency range) over which the power delivered to R is at least half that delivered at ω_0 ("half-power bandwidth")

@ $\omega_0, |I| = \frac{V_s}{R}$

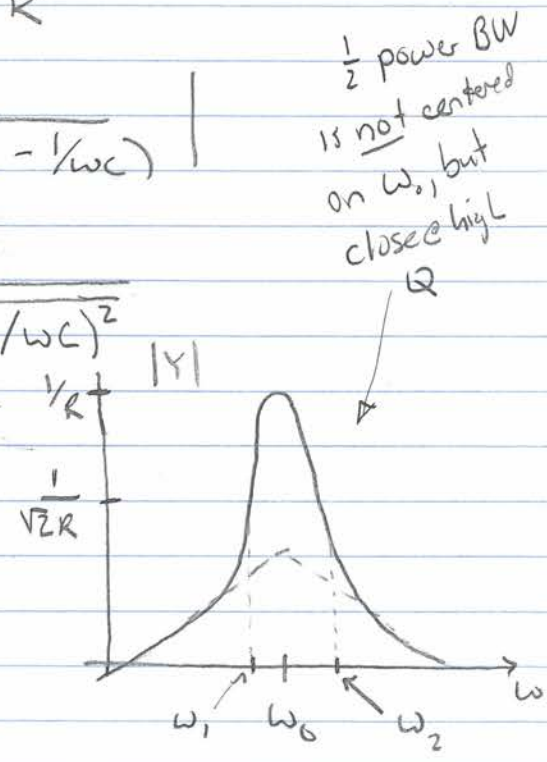
for half-power we get $|I| = \frac{V_s}{\sqrt{2}R}$

or $|Y| = \frac{1}{\sqrt{2}R} = \left| \frac{1}{R + j(\omega L - 1/\omega C)} \right|$

$\therefore \frac{1}{\sqrt{2}R} = \frac{1}{\sqrt{R^2 + (\omega L - 1/\omega C)^2}}$

$\therefore \left| \omega L - \frac{1}{\omega C} \right| = R$

happens @ two frequencies, $\omega_1 < \omega_0, \omega_2 > \omega_0$



@ $\omega_1: \omega_1 L - \frac{1}{\omega_1 C} = -R$

$\omega_1^2 LC + \omega_1 RC - 1 = 0$

$\omega_1 = \frac{-RC + \sqrt{(RC)^2 + 4LC}}{2LC} = -\frac{R}{2L} + \sqrt{\frac{1}{LC} + \left(\frac{R}{2L}\right)^2}$

@ $\omega_2: \omega_2 L - \frac{1}{\omega_2 C} = R \Rightarrow \omega_2^2 LC - \omega_2 RC - 1 = 0$

$\therefore \omega_2 = \frac{+RC + \sqrt{(RC)^2 + 4LC}}{2LC} = \sqrt{\frac{1}{LC} + \left(\frac{R}{2L}\right)^2} + \frac{R}{2L}$

Finding the half-power bandwidth $BW = \omega_2 - \omega_1$

$$\omega_2 - \omega_1 = R/L$$

Normalizing this to ω_0 , we get:

$$\frac{BW}{\omega_0} = \frac{R\sqrt{LC}}{L} = \frac{R}{\sqrt{L/C}} = \frac{R}{Z_0} = \frac{1}{Q(\omega_0)}$$

So we find that the half-power bandwidth (over which the power delivered to R is at least $1/2$ that at ω_0) normalized to ω_0 is $1/Q$!

\Rightarrow higher Q gives larger peaking over a narrower bandwidth

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