

# Introduction to EES - 2

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**2.60/2.62/10.390 Fundamentals of Advanced Energy Conversion**

Spring 2020

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Credits: Adapted from the presentations created by Xiaoyu Wu and Aniket Patankar for 2.60

# Examples for Today

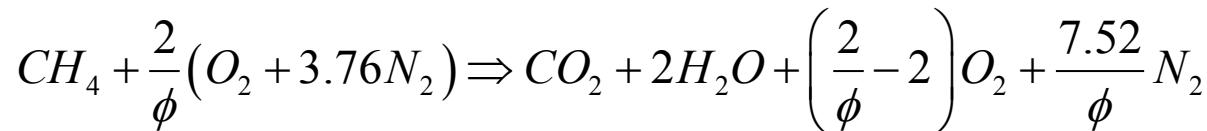
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1. Adiabatic Flame Temperature
2. Throttling, Joule-Thomson effect
3. Chemical Equilibrium

# Example 1: Adiabatic Flame Temperature

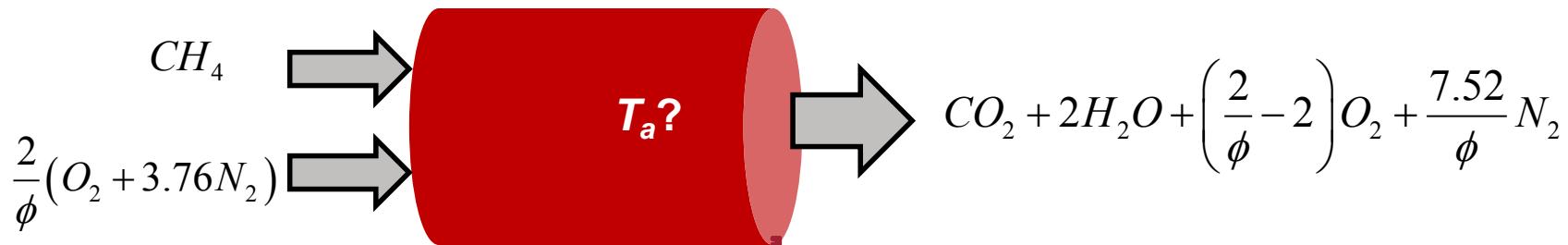
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- What's the adiabatic temperature  $T_a$  of lean burning when the equivalence ratio  $\phi$  changes ( $\phi < 1$ )



$$T_0 = 298 \text{ K}$$

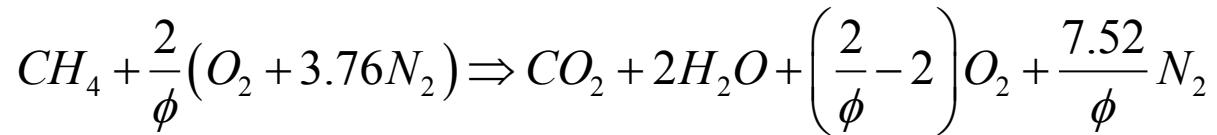
$$P_0 = 1 \text{ bar}$$



# Equations

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Assume: Only forward reaction occurs; constant pressure



Adiabatic condition:

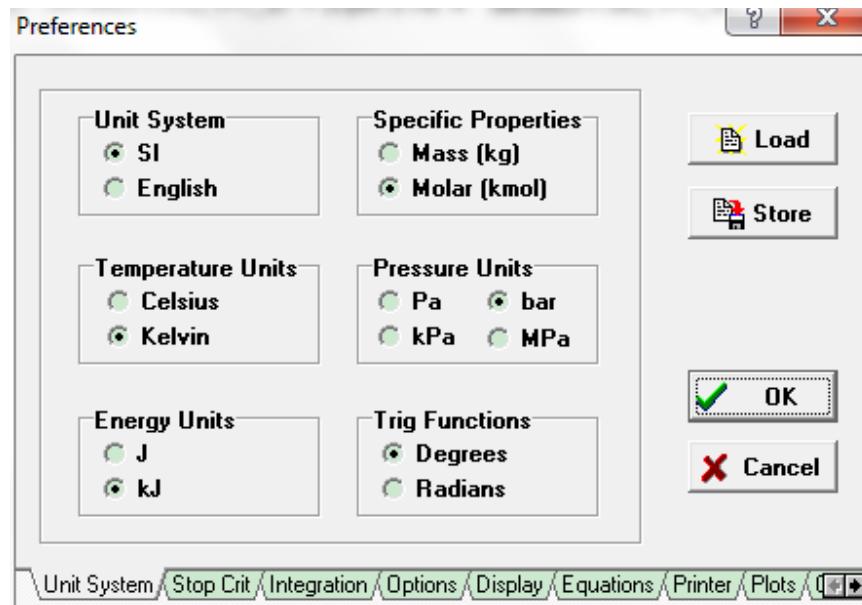
$$H_{reactnats}(T_0, P_0) = H_{products}(T_a, P_0)$$

# Before writing code – Set the Units right!

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**Options → Unit Systems:** Set the unit system.

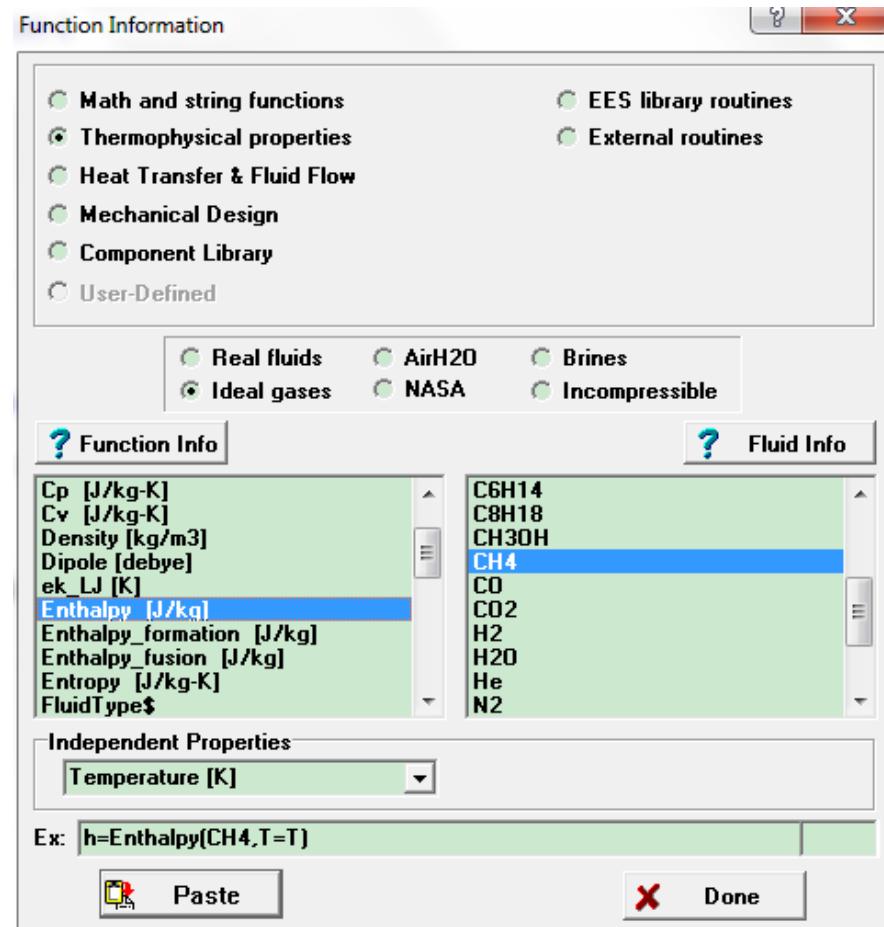
Recommended – T in Kelvin, Specific properties per unit mole



# Property Functions

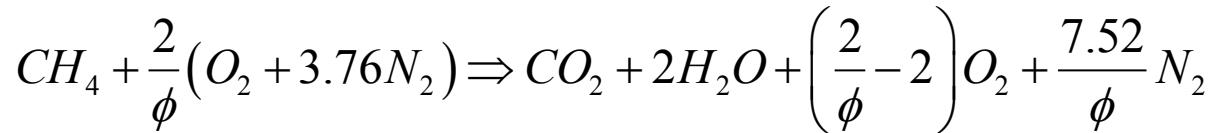
## Options → Function Information

- Thermophysical properties
- Ideal gases/Real gas
- Then Paste



# Equations

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"1) enthalpy of reactants"

$$T_o = 298$$

$$h_R = ENTHALPY(CH4,T=T_o) + 2/\phi * ENTHALPY(O2,T=T_o) + 2/\phi * 3.76 * ENTHALPY(N2,T=T_o)$$

"2) enthalpy of products"

$$h_P = 1 * ENTHALPY(CO2,T=T_a) + 2 * ENTHALPY(H2O,T=T_a) + (2/\phi - 2) * ENTHALPY(O2,T=T_a) + 2/\phi * 3.76 * ENTHALPY(N2,T=T_a)$$

"3) energy balance"

$$h_R = h_P$$

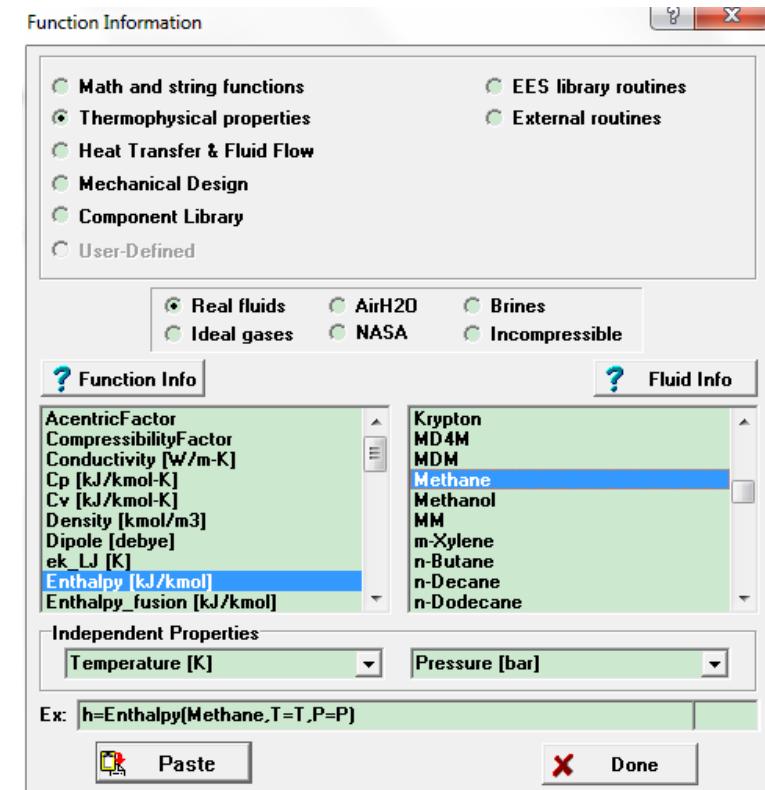
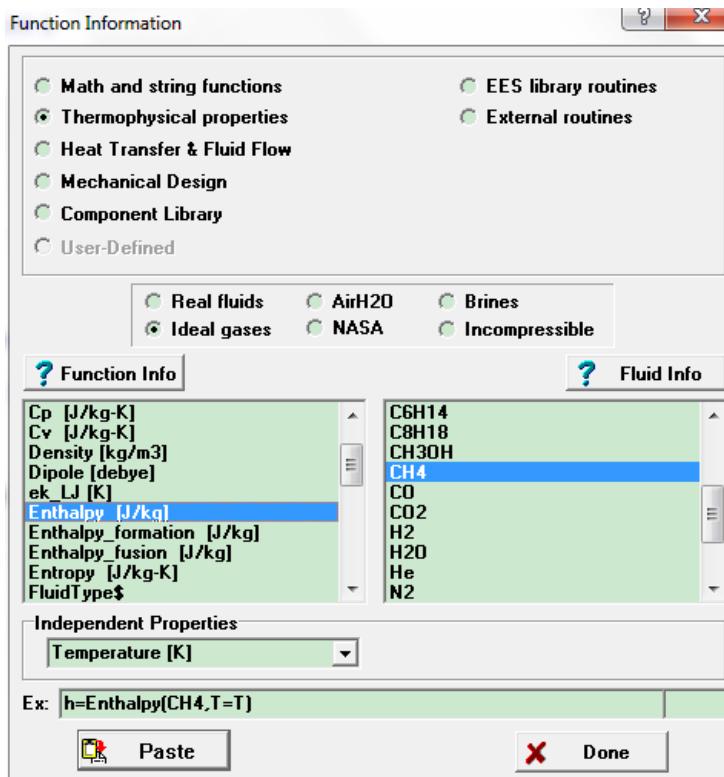
Why pressure isn't required?

ENTHALPY *per unit mole* in above formulation.

# Ideal gas vs Real fluids

## Differences:

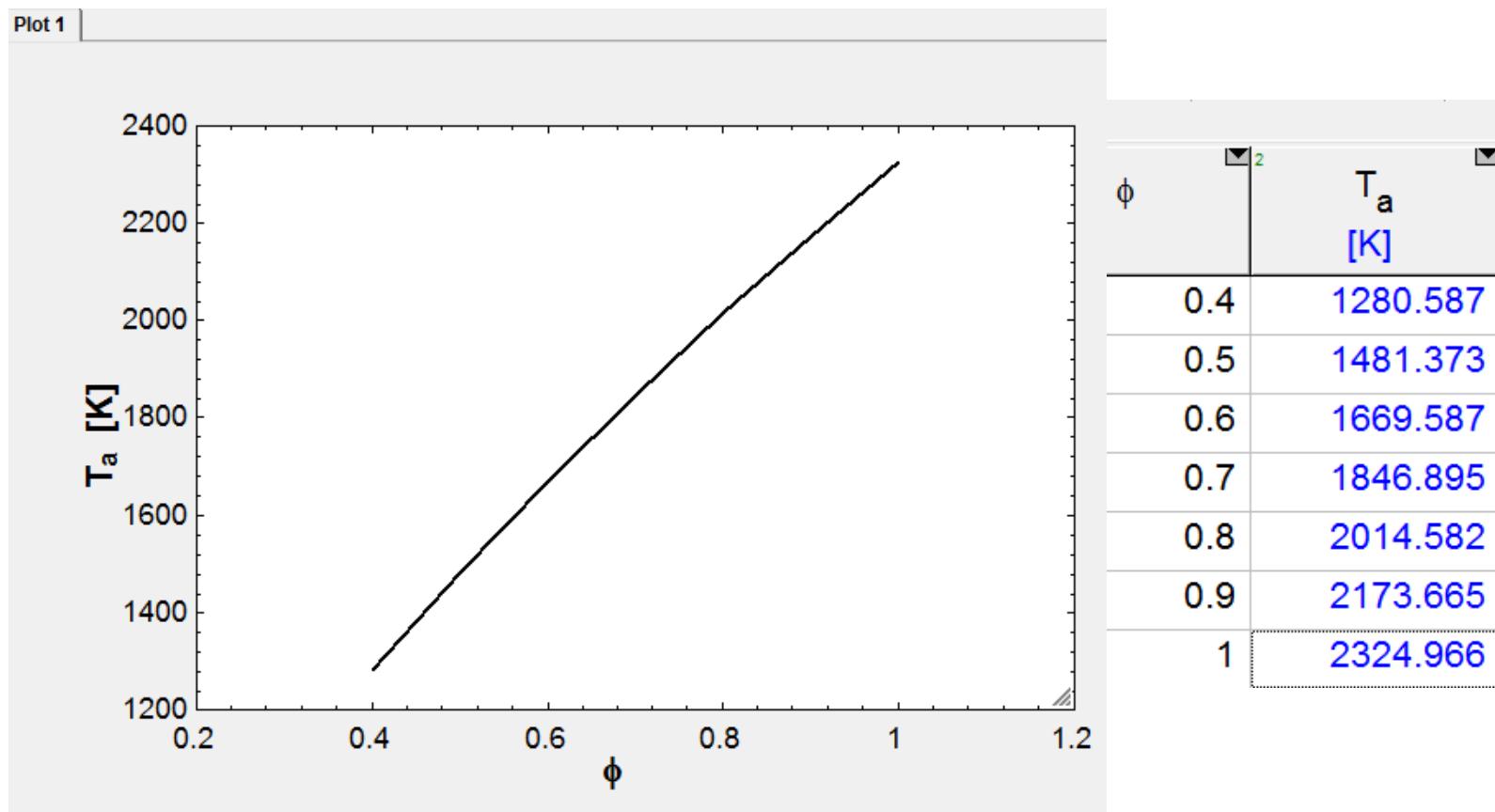
- Number of parameters required
- Name of fluid
- Reference values



# Parametric Table and Plot

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- Tables → New Parametric Table



# Throwback to the notes

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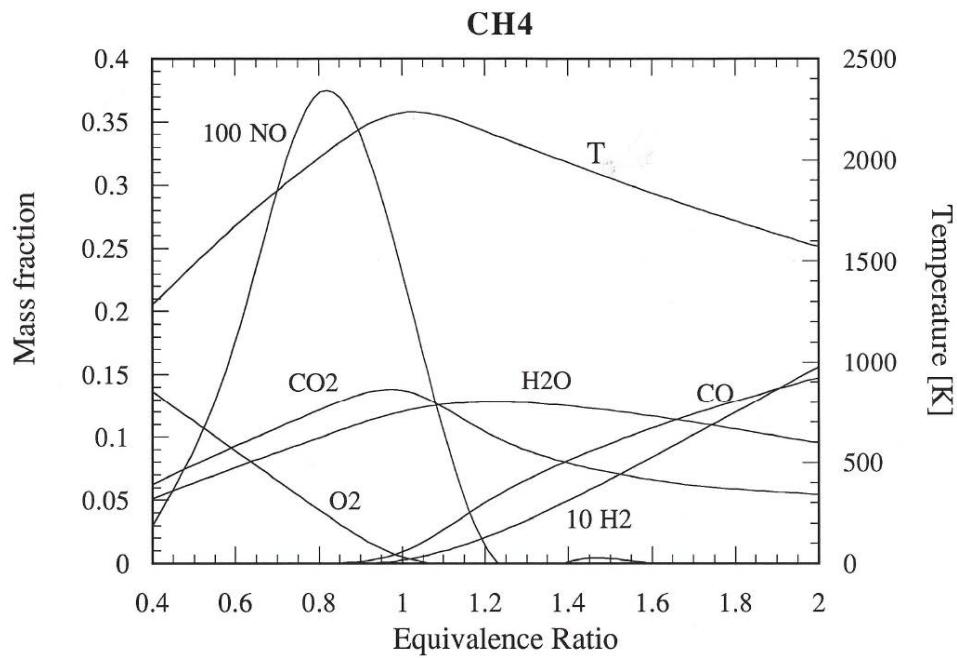
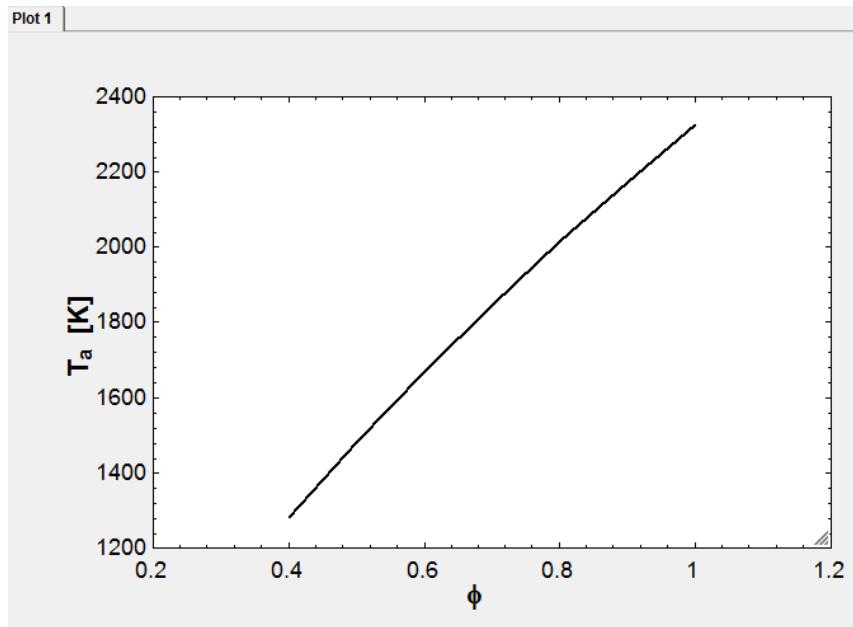


Figure from Chapter 3, 2.60 Spring 2020

## Example 2 – Joule-Thomson Inversion

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ISENTHALPIC expansion across a throttle valve can lead to an increase or decrease in temperature depending on conditions before throttling.

This effect is captured in terms of the Joule-Thomson coefficient defined below.

$$\mu_{JT} = \left( \frac{\partial T}{\partial P} \right)_H = \frac{V}{C_p} (\alpha T - 1)$$

(credits: Wikipedia.  $\alpha$  is the coefficient of thermal expansion)

[https://en.wikipedia.org/wiki/Joule–Thomson\\_effect](https://en.wikipedia.org/wiki/Joule–Thomson_effect)

# The Joule-Thomson Inversion Curve

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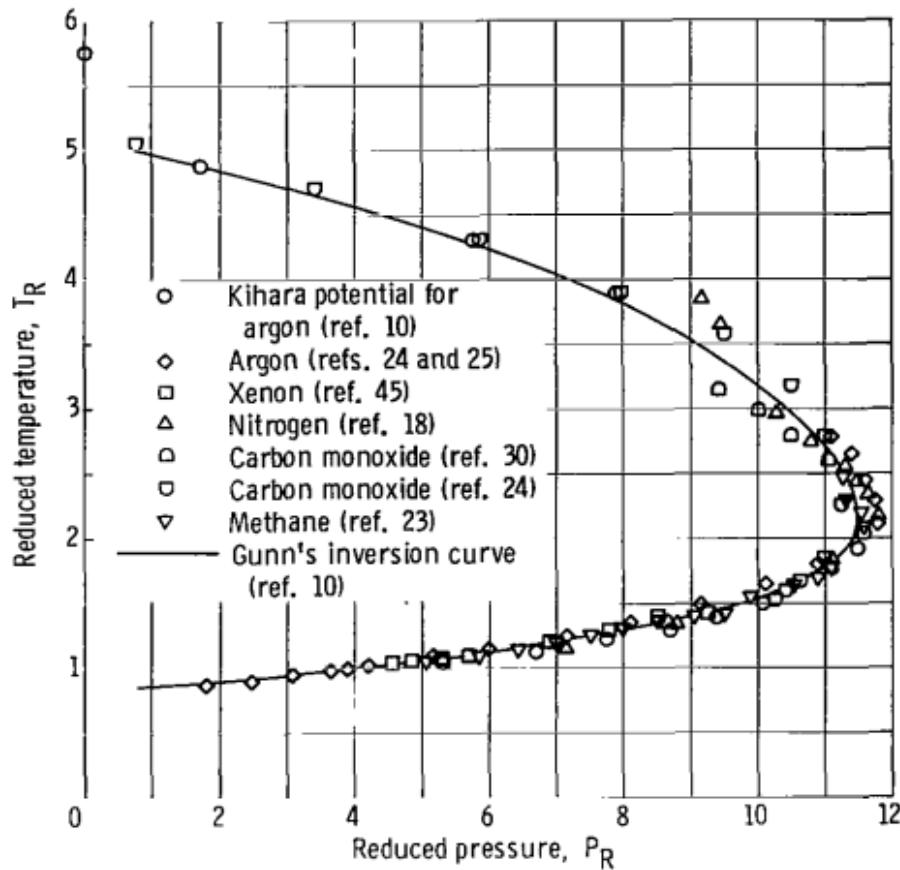


Figure courtesy of NASA.

Figure 1. - Generalized reduced inversion curve for several corresponding states fluids as determined by Gunn, Chueh, Prausnitz (ref. 10).

# Application to refrigeration and liquefaction: Linde-Hampson Cycle

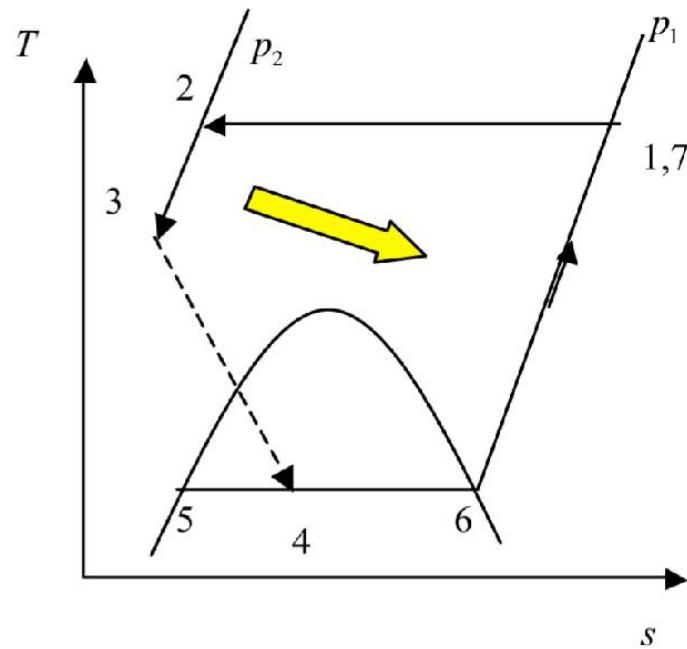
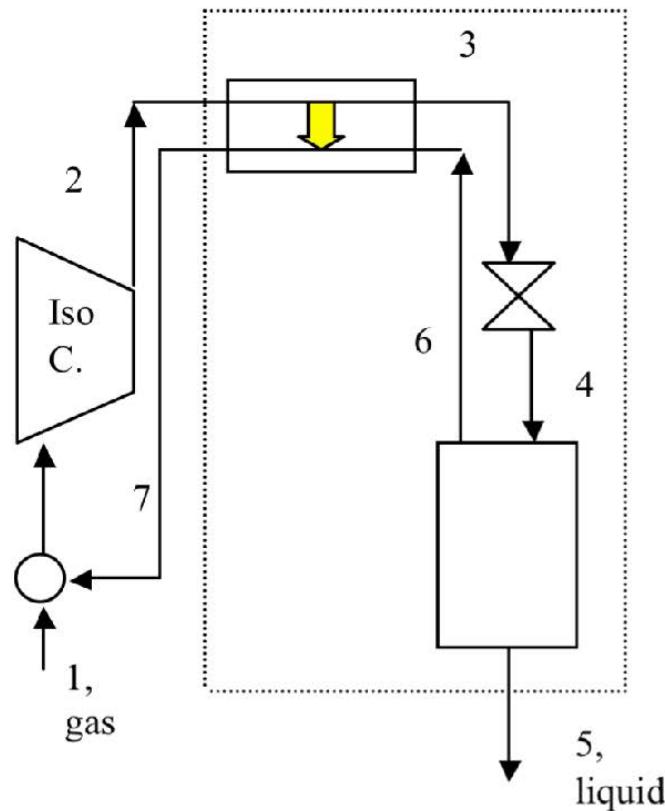


Figure from lecture 3, 2.60 Spring 2020

# EES for Joule-Thomson Inversion

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P1 = 135.6 [bar]

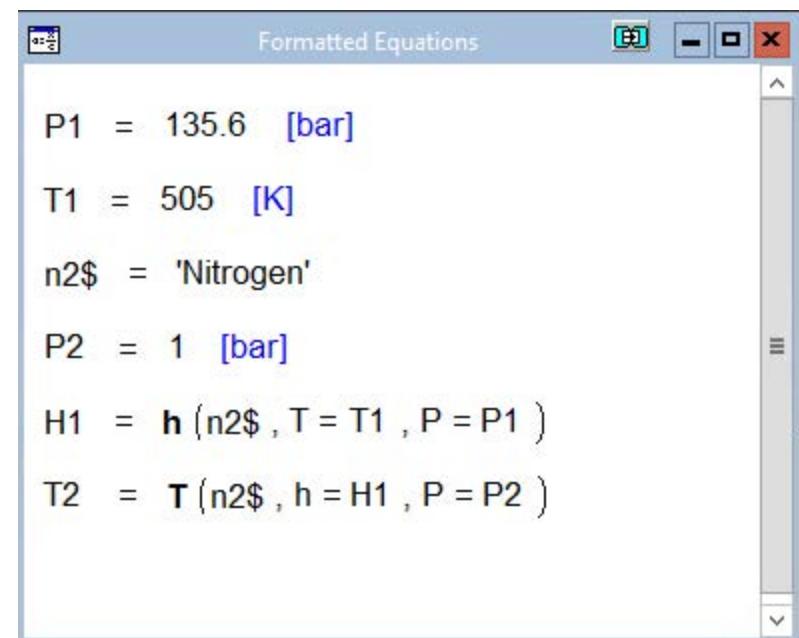
T1 = 505 [K]

n2\$ = 'Nitrogen'

P2 = 1 [bar]

H1 = **enthalpy**(n2\$, T=T1, P=P1)

T2 = **temperature**(n2\$, h=H1, P=P2)



The screenshot shows the 'Formatted Equations' window of the EES software. The window title is 'Formatted Equations'. Inside, there are six equations listed:

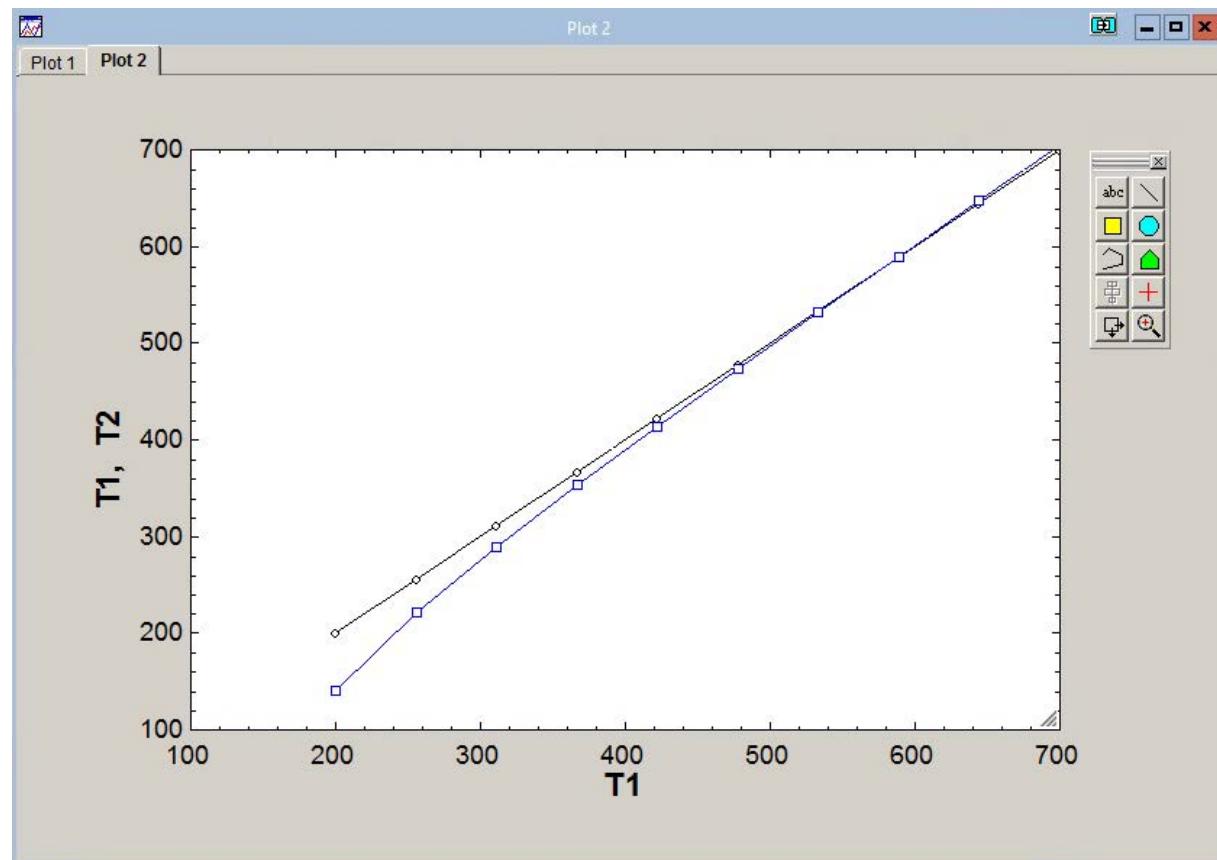
- P1 = 135.6 [bar]
- T1 = 505 [K]
- n2\$ = 'Nitrogen'
- P2 = 1 [bar]
- H1 = h (n2\$ , T = T1 , P = P1 )
- T2 = T (n2\$ , h = H1 , P = P2 )

# Joule-Thomson Inversion of Nitrogen

Table 1    Table 2

1.10

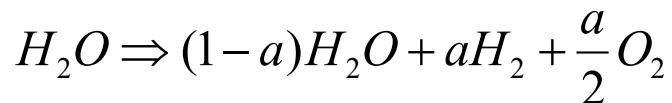
	T1	T2
Run 1	200	140.6
Run 2	255.6	221.2
Run 3	311.1	289.5
Run 4	366.7	352.8
Run 5	422.2	413.8
Run 6	477.8	473.2
Run 7	533.3	531.8
Run 8	588.9	589.6
Run 9	644.4	647
Run 10	700	704



# Example 3: Water Dissociation at 3000 K

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- 1 mole of water dissociated at 3000 K, 1 atm

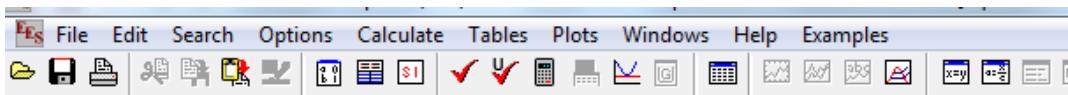


- The conditions for equilibrium is:

$$\sum_N \mu_i dn_i = 0$$

$$\mu_{H_2} \cdot n_{H_2} + \mu_{O_2} \cdot n_{O_2} = \mu_{H_2O} \cdot n_{H_2O}$$

# Equations



"Determine the equilibrium concentrations of different species for the dissociation of water  $H_2O \rightleftharpoons H_2 + 1/2 O_2$  at 3000 K."

"At 3000K, EES has already subtracted data at the reference state:"

T = 3000  
P = 101.5

- Conditions

$h_{H_2O} = \text{ENTHALPY}(H_2O, T=T)$   
 $h_{H_2} = \text{ENTHALPY}(H_2, T=T)$   
 $h_{O_2} = \text{ENTHALPY}(O_2, T=T)$

$s_{H_2O} = \text{ENTROPY}(H_2O, T=T, P=P*X_{H_2O})$   
 $s_{H_2} = \text{ENTROPY}(H_2, T=T, P=P*X_{H_2})$   
 $s_{O_2} = \text{ENTROPY}(O_2, T=T, P=P*X_{O_2})$

$g_{H_2O} = h_{H_2O} - T * s_{H_2O}$   
 $g_{H_2} = h_{H_2} - T * s_{H_2}$   
 $g_{O_2} = h_{O_2} - T * s_{O_2}$

$0 = n_{H_2} * g_{H_2} + n_{O_2} * g_{O_2} - (1-n_{H_2O}) * g_{H_2O}$

$1 - n_{H_2O} = n_{H_2}$   
 $1 - n_{H_2O} = 2 * n_{O_2}$

$X_{H_2O} = n_{H_2O} / (n_{H_2} + n_{O_2} + n_{H_2O})$   
 $X_{H_2} = (n_{H_2}) / (n_{H_2} + n_{O_2} + n_{H_2O})$   
 $X_{O_2} = (n_{O_2}) / (n_{H_2} + n_{O_2} + n_{H_2O})$

$$X_{H_2O} = 0.7963$$

$$X_{H_2} = 0.1358$$

$$X_{O_2} = 0.0679$$

- Properties
  - Entropies using Partial pressure

- Equilibrium

- Mass balance

# Example 3: Code

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T=3000 [K]

P = 101.5 [kPa]

h\_H2O = **enthalpy(H2O, T=T)**

h\_H2 = **enthalpy(H2, T=T)**

h\_O2 = **enthalpy(O2, T=T)**

s\_H2O = **entropy(H2O, T=T, P=P\*X\_H2O)**

s\_H2 = **entropy(H2, T=T, P=P\*X\_H2)**

s\_O2 = **entropy(O2, T=T, P=P\*X\_O2)**

g\_H2O = h\_H2O - T\*s\_H2O

g\_H2 = h\_H2 - T\*s\_H2

g\_O2 = h\_O2 - T\*s\_O2

0 = n\_H2\*g\_H2 + n\_O2\*g\_O2 - (1-n\_H2O)\*g\_H2O

1 - n\_H2O = n\_H2

1 - n\_H2O = 2\*n\_O2

X\_H2O = n\_H2O/(n\_H2+n\_O2+n\_H2O)

X\_H2 = n\_H2/(n\_H2+n\_O2+n\_H2O)

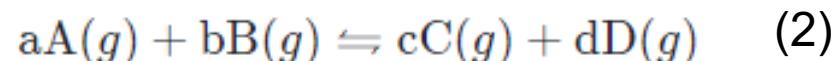
X\_O2 = n\_O2/(n\_H2+n\_O2+n\_H2O)

# Another approach – Equilibrium Constant

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1. Definition of equilibrium constant in terms of change in Gibbs Free energy.
2. A sample reaction
3. Definition of equilibrium constant in terms of partial pressures of reactants and products

$$K_p(T) = \exp\left(-\frac{\Delta G_{rxn}^o(T)}{RT}\right) \quad (1)$$



$$K_p = \frac{(P_C)^c(P_D)^d}{(P_A)^a(P_B)^b} \quad (3)$$

# Calculating K<sub>p</sub>

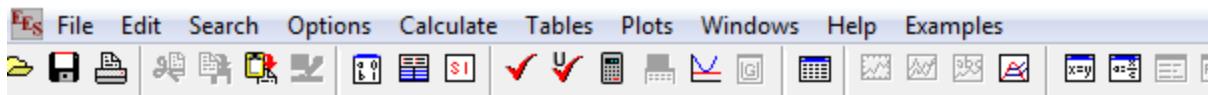
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- Standard Gibbs free energy of the reaction at  $T$ 
  - Evaluated the stoichiometric reaction
  - Standard  $G$  at  $T$  and  $P_0$



$$\Delta G_{rxn}^o(T) = v_{H_2} \cdot g_{H_2}^o(T) + v_{O_2} \cdot g_{O_2}^o(T) - v_{H_2O} \cdot g_{H_2O}^o(T)$$

# Equations



"Determine the equilibrium concentrations of different species for the dissociation of water  $H_2O \rightleftharpoons H_2 + 1/2 O_2$  at 3000 K."

$$a = 0.1457$$

"At 3000K, EES has already subtracted data at the reference state:"

$$T = 3000$$

$$P = 101.5$$

$$R = 8.314$$

$$h_{H2O} = ENTHALPY(H2O, T=T)$$

$$h_{H2} = ENTHALPY(H2, T=T)$$

$$h_{O2} = ENTHALPY(O2, T=T)$$

$$s_{H2O\_0} = ENTROPY(H2O, T=T, P=P)$$

$$s_{H2\_0} = ENTROPY(H2, T=T, P=P)$$

$$s_{O2\_0} = ENTROPY(O2, T=T, P=P)$$

$$G_p = 1 * h_{H2} + 0.5 * h_{O2} - T * (1 * s_{H2\_0} + 0.5 * s_{O2\_0})$$

$$G_r = 1 * h_{H2O} - T * s_{H2O\_0}$$

$$\Delta G = G_p - G_r$$

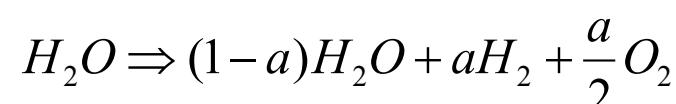
$$K_P = \exp(\Delta G / R/T)$$

$$a / (1 + 0.5 * a) * (0.5 * a / (1 + 0.5 * a))^{0.5} / ((1 - a) / (1 + 0.5 * a)) = K_P$$

- Properties
  - Entropies using standard pressure

- Standard Gibbs Free Energy

- Equilibrium constant



# Example 3: Code (Approach II)

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T=3000 [K]

P = 101.5 [kPa]

R = 8.314

`h_H2O = enthalpy(H2O, T=T)`

`h_H2 = enthalpy(H2, T=T)`

`h_O2 = enthalpy(O2, T=T)`

`s_H2O_0 = entropy(H2O, T=T, P=P)`

`s_H2_0 = entropy(H2, T=T, P=P)`

`s_O2_0 = entropy(O2, T=T, P=P)`

`G_p = h_H2 + 0.5*h_O2 - T*(s_H2_0 + 0.5*s_O2_0)`

`G_r = h_H2O - T*s_H2O_0`

`Delta_G = G_p-G_r`

`K_P = exp(-Delta_G/R/T)`

`a/(1+0.5*a)*(0.5*a/(1+0.5*a))^0.5/((1-a)/(1+0.5*a)) = K_P`

## Example 4: Methane reforming

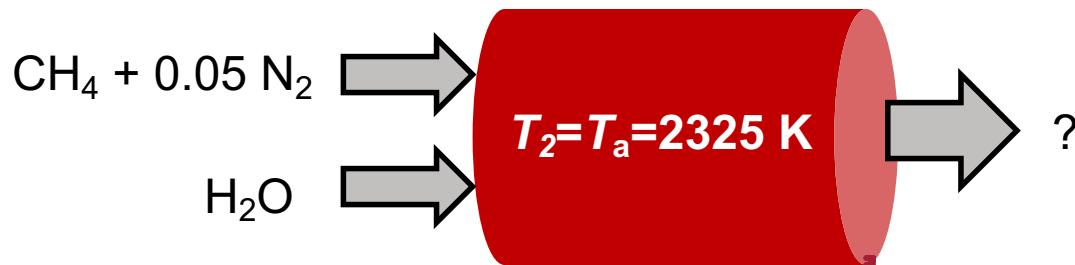
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- What's the equilibrium products of a methane reformer?
  - Natural gas contains 4 – 6% N<sub>2</sub> when it is sold to the pipeline



**P = 1 bar**

**T = 950 – 1350 K**



# CHEM\_EQUIL libraries

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- CHEM\_EQUIL calculates the equilibrium composition for an ideal gas mixture containing elements C, H, O, N, and A (A = Argon).

- **INPUTS:**

- P: pressure [kPa]
- T: temperature [K] (600 K < T < 5000 K)
- AO: ratio of molecules of the inert species to atomic oxygen
- CO: ratio of atomic carbon to atomic oxygen
- HO: ratio of atomic hydrogen to atomic oxygen
- NO: ratio of atomic nitrogen to atomic oxygen

Note: AO can be set to zero. However, the minimum value for any of the other ratios is 1E-5.

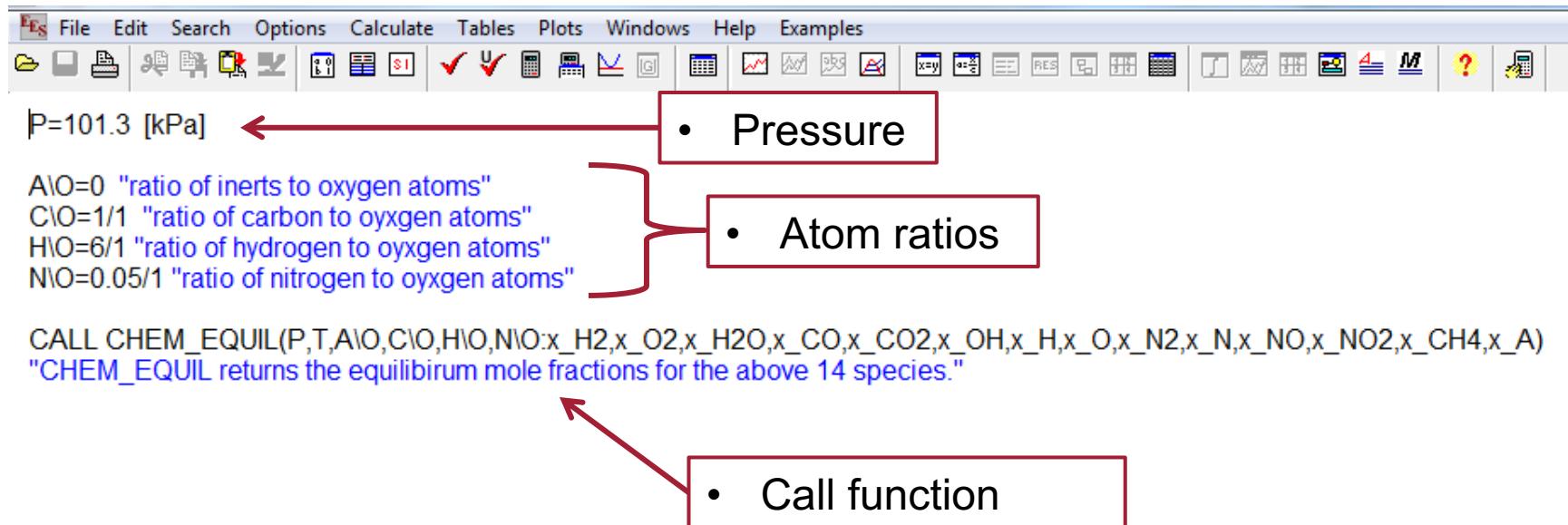
- Call function:

- CALL

```
CHEM_EQUIL(P,T,AO,CO,HO,NO:x_H2,x_O2,x_H2O,x_CO,x_CO2,x_OH,x_H,x_O,x_N2,x_N,x_NO,x_NO2,x_CH4,x_A)
```

# Equations

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\*\*You need to have CHEM\_EQUIL library installed (available on EES website).

## Example 4 - Code

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P = 101.3 [kPa]

{T = 950}

AO = 0

CO = 1/1

HO = 6/1

NO = 0.05/1

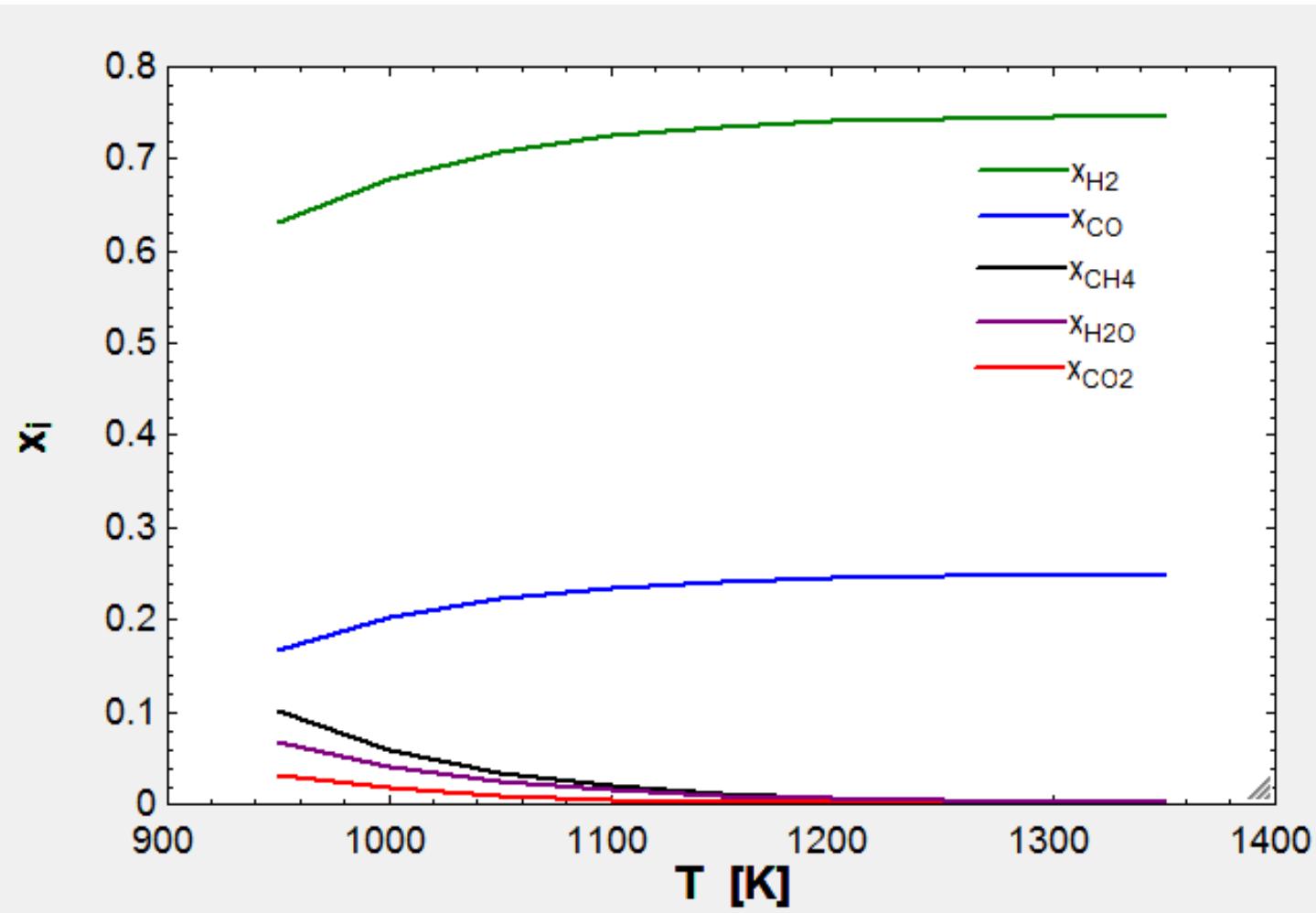
Call

```
chem_equil(P,T,AO,CO,HO,NO:x_H2,x_O2,x_H2O,x_CO,x_CO2,x_OH  
,x_H,x_O,x_N2,x_N,x_NO,x_NO2,x_CH4,x_A)
```

# Parametric Table and Plot

- Tables → New Parametric Table
- Plot → New Plot Windows → X-Y Plot

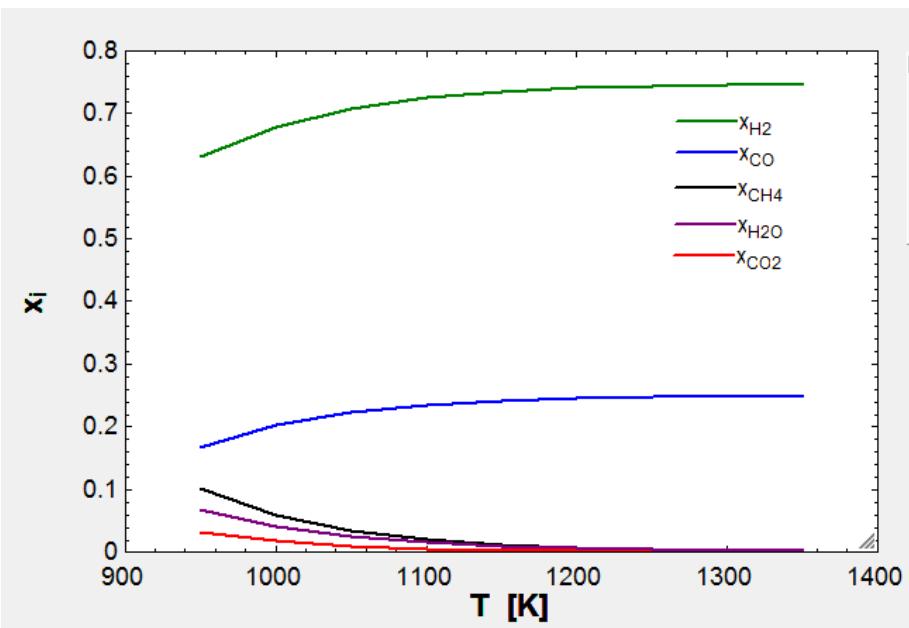
	1 1.9	2 T [K]	3 x <sub>CH4</sub>	4 x <sub>CO</sub>	5 x <sub>CO2</sub>	6 x <sub>H2</sub>	x <sub>H2O</sub>
Run 1		950	0.1005	0.1673	0.03248	0.6317	0.06803
Run 2		1000	0.05945	0.2024	0.01788	0.6787	0.04157
Run 3		1050	0.03414	0.2236	0.009305	0.7081	0.02484
Run 4		1100	0.01975	0.2353	0.004813	0.7252	0.01494
Run 5		1150	0.01171	0.2416	0.002551	0.735	0.009157
Run 6		1200	0.00717	0.245	0.001399	0.7406	0.005771
Run 7		1250	0.004542	0.2469	0.0007997	0.744	0.003742
Run 8		1300	0.002972	0.248	0.0004745	0.746	0.002497
Run 9		1350	0.002003	0.2487	0.0002922	0.7473	0.001711



Plot of data from the previous slide. Steam reforming of Methane with N<sub>2</sub> impurity.

# Throwback to the notes

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Plot of data from the previous slide. Steam reforming of Methane with  $\text{N}_2$  impurity.

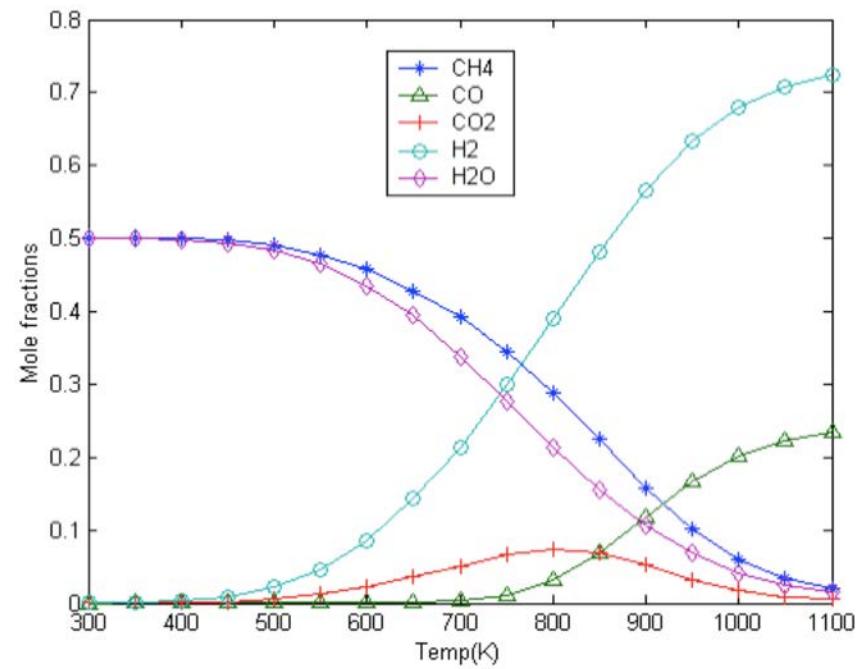


Figure from Lecture 6, 2.60 Spring 2020

# Examples for Today

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1. Adiabatic Flame Temperature
2. Throttling, Joule-Thomson effect
3. Chemical Equilibrium

# Summary

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## 1. Thermodynamics property libraries

- Ideal gas and Real fluids

## 2. Thermodynamic equilibrium

- Gibbs free energy
- Equilibrium constant
- Equilibrium Libraries

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2.60J Fundamentals of Advanced Energy Conversion  
Spring 2020

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