1. Consider the complex number $s_1 = -1 + j$ and its geometrical representation on the complex $s$–plane shown below. *Do not use Matlab until you reach question (d) of this problem.*

![Complex Plane Diagram](image)

a) Using geometrical arguments and calculations on the $s$–plane, compute the phase of the complex number $(s_1 + 2)(s_1 + 0)$. Use complex number algebra to verify your geometrical computation.

b) Using geometrical arguments and calculations on the $s$–plane, compute the value of the real number $K$ such that

$$K |s_1 + 2| |s_1 + 0| = 1.$$ 

Use complex number algebra to verify your geometrical computation.

c) Based on the answers to the previous two questions, do you expect $s_1$ to be a closed–loop pole of a feedback system which has two open–loop poles located at 0, −2 and no open–loop zeros? Justify your answer. If yes, what is the value of the feedback gain that would yield a closed–loop pole at location $s_1$?

d) Verify numerically, using MATLAB, your answers to all the above questions. Include corroborating plots in your argument.
2. Consider a feedback system with open–loop poles at 0, −1, −2 and no open–loop zeros. The geometrical representation of this system’s open–loop poles on the complex s–plane is shown below. Do not use Matlab until you reach question (f) of this problem.

![Diagram of s-plane with poles at 0, -1, -2 and -\sqrt{2}, \sqrt{2}]

a) Using geometrical arguments and calculations on the s–plane, show that ±j√2 belongs to the root locus of this system.

b) Using geometrical arguments and calculations on the s–plane, compute the feedback gain K that would be required to drive two closed–loop poles of this system to the locations ±j√2.

c) Verify algebraically the results that you obtained geometrically in questions (a–b).

d) What will happen to this system if K exceeds the value that you computed in question (b)?

e) Sketch the complete root locus for this system. In your plot, indicate numerical values for the asymptote angles and real–axis intercepts, as well as the break–in/away points, if any.

f) Verify numerically, using MATLAB, your answers to all the above questions. Include corroborating plots in your argument.

3. Consider a system with open–loop poles at −1, −2. Initially, this system is connected in proportional control feedback configuration, with gain K. The application where this system is to be used requires that the overshoot not exceed 16.3%. Do not use Matlab until you reach question (h) of this problem.

a) Sketch the root locus for this system.

b) Using geometrical arguments and calculations on the s–plane, find the closed–loop pole location that will yield the desired overshoot. Do you expect your answer to be exact or approximate?
c) What is the settling time at the closed–loop pole chosen from the previous question?

d) Using geometrical arguments and calculations on the s–plane, compute the value of the gain $K$ that will drive the closed–loop pole to the location used in the previous two questions.

e) We now wish to reduce the settling time to 75% of the value obtained in question (c) while maintaining the same overshoot. Therefore, we propose to modify the feedback loop from its present proportional–control configuration to a proportional–derivative (PD) control configuration. Using geometrical arguments and calculations on the s–plane, design the PD controller that meets the new specifications (i.e., indicate where the open–loop zero should be placed on the negative real axis.) **Hint:** Study and understand the PD compensator design procedure described in Lecture 23 before you attempt this question. The PD controller’s open–loop zero should be placed on the real axis to the left of the existing open–loop pole at −2.

f) Using geometrical arguments and calculations on the s–plane, compute the PD controller’s gain that will result in the desired transient performance. Do you expect that the settling time and overshoot requirements will be met exactly or approximately in the new PD controller configuration?

g) Sketch the root locus of the PD–compensated system.

h) Verify numerically, using MATLAB, your answers to all the above questions. Include corroborating plots in your argument.

4. Given the matrices

$$
A = \begin{pmatrix} 3 & 1 \\ -1 & 3 \end{pmatrix}, \quad B = \begin{pmatrix} 2 & -1 \\ 3 & 5 \end{pmatrix}, \quad I = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}
$$

and the vectors

$$
p = \begin{pmatrix} -1 \\ 1 \end{pmatrix}, \quad q = \begin{pmatrix} e^{-3t}\cos t \\ e^{-3t}\sin t \end{pmatrix},
$$

compute the matrices $sI - A$, $AB$, $B^{-1}A$, and the vectors $Bp$, $Aq$. You should study the auxiliary material on matrices that we have posted in the Stellar website before you attempt this problem.

5. In this problem, we will generate a state–space representation for the compensated 2.004 Tower system. (Recall that in Lecture 24 we developed a simplified model for the uncompensated tower; you should thoroughly familiarize yourself with the Lecture 24 notes and the auxiliary notes on matrices before you attempt this problem.) The model is shown in the figure on next page. The wind force (disturbance) is denoted as $w$, and the actuator force is denoted as $a$, as in the
notes. Note that the actuator exerts equal but opposite forces on the tower and slider.

a) Which forces are acting on the tower? Be particularly careful when you include the force due to spring $k_2$, since the spring extension is the relative displacement of the tower with respect to the slider. Similarly, be particularly careful when you include the force due to damper $b_2$, since damping is due to the relative velocity of the tower with respect to the slider. By applying force balance, obtain an equation of motion for the tower.

b) Which forces are acting on the slider? Be careful with the spring and damper forces for the same reasons quoted in the previous question. By applying force balance, obtain an equation of motion for the slider.

c) Now define the tower displacement and velocity $x_1, v_1$, respectively, and slider displacement and velocity $x_2, v_2$, respectively, as the state variables, and the state vector

$$ q = \begin{pmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \end{pmatrix} \equiv \begin{pmatrix} x_1 \\ v_1 \\ x_2 \\ v_2 \end{pmatrix}. $$

Rewrite the tower’s and slider’s equations of motion in terms of the state variables $q_1, q_2, q_3, q_4$.

d) Solve the tower’s equation of motion for $\dot{q}_2$ and the slider’s equation of motion for $\dot{q}_4$.

e) To the two equations that you obtained in the previous question append the definitions $q_2 = \dot{q}_1$, $q_4 = \dot{q}_3$. Rewrite the resulting four equations in matrix form, i.e. find the matrix $A$ and vectors $B, G$ such that

$$ \dot{q}(t) = Aq(t) + Ba(t) + Gw(t). $$
We will refer to $\mathbf{B}$, $\mathbf{G}$ as \textbf{actuation} and \textbf{disturbance} vectors, respectively. (Note that in multi-input systems $\mathbf{B}$ and $\mathbf{G}$ would actually be matrices; hence, the uppercase letter notation.)

Do not substitute numbers in your final matrix expression; you will do that as part of your Lab 7 assignment. Using the state-space representation that we obtained here to minimize the tower’s displacement in response to an impulse disturbance is the subject of the next few lectures and the rest of the Lab assignments.